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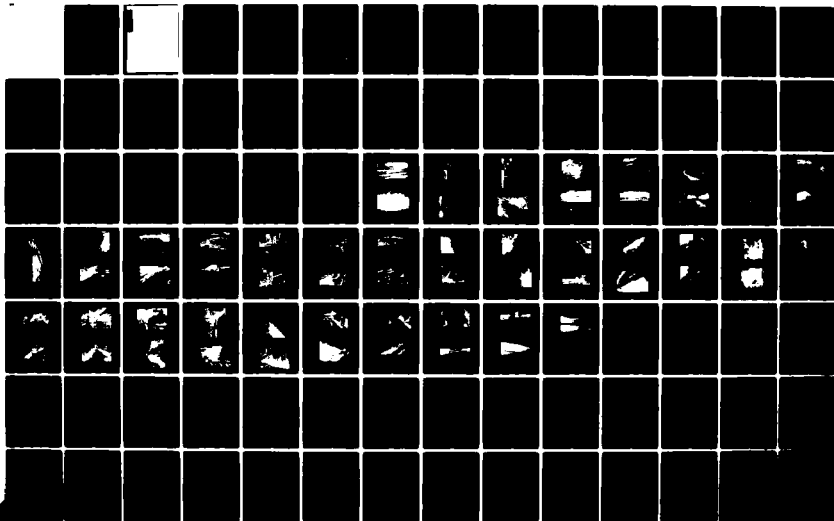
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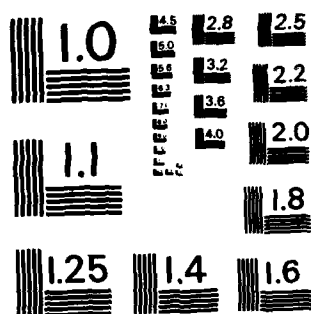
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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This report describes the foundation conditions encountered during the construction of a water supply dam for the city of Conway, Arkansas; such to replace a previous water supply that was adversely affected by the construction of the McClellan-Kerr Arkansas River Navigation System. The dam was founded on a thick shale layer of the Atoka Formation. Locally, the shale was gray to black, hard to moderately hard, sandy, and well compacted. Excavation of a 10-foot wide centerline cutoff core trench in the shale posed		

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no problems with standard earth-moving equipment. Pre-split blasting was required in excavating the outlet works structures and emergency spillway.

Due to the susceptibility of shale to slake and deteriorate when exposed, a 6" to 1' protective layer above final grades in the rock were left until just prior to final foundation preparation, and placement of embankment material and/or concrete for outlet works.

The report gives the results of a well-point dewatering system installed in the valley section that did not function adequately, and methods to overcome ground-water flow at the rock/overburden contact.

Foundation preparation and treatment consisted of wash/air jetting, mortared open joints, concrete fillets, and rock anchoring. The report details the installation of a grout curtain utilizing the stop-grouting, split spacing method.

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DEPARTMENT OF THE ARMY  
LITTLE ROCK DISTRICT, CORPS OF ENGINEERS  
LITTLE ROCK, ARKANSAS

FOUNDATION REPORT

Conway Water Supply Project  
Dam and Dike

June 1983



## TABLE OF CONTENTS

	<u>Page</u>
<b>PART I: INTRODUCTION</b>	
1-01. Location and Description of Project	1
1-02. Construction Authority	1
1-03. Purpose of Report	1
1-04. Contractor and Contract Supervision	1
<b>PART II: FOUNDATION EXPLORATIONS</b>	
2-01. Investigations Prior to Construction	3
2-02. Investigations During Construction	4
<b>PART III: GEOLOGY</b>	
3-01. Regional Geology	5
3-02. Site Geology	5
a. Physiography	5
b. Overburden	5
c. Bedrock Formation	6
d. Bedrock Structure	6
e. Bedrock Weathering	6
f. Ground Water	7
g. Seismicity	7
h. Engineering Characteristics of Overburden	7
i. Engineering Characteristics of Bedrock	8
<b>PART IV: SPECIAL DESIGN CONSIDERATIONS</b>	
4-01. Construction Method	9
4-02. Embankment Stability	9
4-03. Structure Uplift	9
4-04. Earthfill Pressure	9
4-05. Ultimate Strength Design	9
4-06. Wave Forces	9
<b>PART V: EXCAVATION PROCEDURES</b>	
5-01. General	10
5-02. Excavation Equipment	10
5-03. Dewatering System	10
5-04. Excavation Blasting	11
5-05. Foundation Preparaton	11
5-06. Left Abutment Excavation	11
5-07. Valley Excavaton	12
5-08. Right Abutment Excavation	12
5-09. Core Trench Excavation	12

## TABLE OF CONTENTS (con.)

	<u>Page</u>
5-10. Outlet Works Excavation	13
a. Intake Structure	13
b. Outlet Conduit	13
c. Stilling Basin	13
d. Outlet Channel	14
5-11. Spillway Excavation	14
5-12. Dike Excavation	14
 PART VI: CHARACTER OF FOUNDATION	
6-01. General	15
6-02. Left Abutment Foundation	15
6-03. Valley Foundation	15
6-04. Right Abutment Foundation	16
6-05. Outlet Works Foundation	16
a. Intake Structure	16
b. Outlet Conduit	16
c. Stilling Basin	17
6-06. Spillway Foundation	17
6-07. Dike Foundation	17
 PART VII: FOUNDATION TREATMENT	
7-01. General	18
7-02. Curtain Grouting	18
a. Grout Hole Inclinations	18
b. Split Spacing	19
c. Stop Grouting	19
d. Grouting Procedure	19
e. Grout Injections and Mixes	19
f. Grout Conditions	20
7-03. Drainage Provisions	21
7-04. Foundation Anchors	21
7-05. Treatment of Slide Scar	22
 PART VIII: CONSTRUCTION MATERIALS	23
 PART IX: FOUNDATION PROBLEM AREAS	24
 PART X: RECORD OF FOUNDATION APPROVAL	25
 APPENDIX A: Photographs	
 APPENDIX B: Boring Logs	
 APPENDIX C: Plates	



## PART I - INTRODUCTION

1-01. Location and Description of Project. The Conway Water Supply Dam is located in the southeast quarter of Section 21, Township 7 North, Range 15 West. It crosses Cypress Creek at mile 6.7 which is about 5 miles north of Plumerville, Arkansas, in eastern Conway County.

The dam is an earth embankment which rises 83 feet above the streambed to elevation 358.0 (m.s.l.). It has an impervious core, an impervious cut-off, and an outer shell of random fill material. The crest is 20 feet wide, and the length of embankment is 1,374 feet. The reservoir will cover about 1,165 acres and impound 23,500 acre-feet of water at the service spillway crest. The service spillway is at elevation 326 with a two-way drop inlet. There is an emergency saddle spillway on the right abutment with a crest elevation of 339.5. The outlet works has an uncontrolled inlet structure with a 4.0-foot diameter concrete outlet conduit in the right abutment. A pumping station, located on the intake structure, feeds a 36-inch diameter pipeline, which extends 11.4 miles southeast to a treatment plant near Gleason, Arkansas.

There is an earthfill dike located in the northwest quarter of Section 22, Township 7 North, Range 15 West on the east side of the reservoir. The dike is 28 feet high by 1,810 feet long, and has a crest width of 10 feet.

1-02. Construction Authority. The project was authorized under Section 10 of Public Law 93-251 dated 7 March 1974, to replace the existing raw water supply of Conway, Arkansas. The city of Conway previously obtained its water from a pool on Cadron Creek about 2.5 miles upstream from its confluence with the Arkansas River. These facilities were adversely affected by the construction of the Toad Suck Ferry Lock and Dam on the McClellan-Kerr Arkansas River Navigation System.

1-03. Purpose of Report. The objective of this report is to describe the foundation conditions encountered during the construction of the subject dam and its related features, and is a consolidated record of the foundation related construction operations, and an information source for future reference. It is intended also to provide information for evaluating any future structural problems, planning possible foundation studies, and be a part of the permanent project engineering and construction record.

1-04. Contractor and Contract Supervision. The project contract was a joint venture undertaken by McGeorge Contracting Company, Inc., and Valco, Inc. The McGeorge Company was based in Pine Bluff, Arkansas, and Valco was based in North Little Rock, Arkansas. McGeorge was the principal contractor for the earth work, and Valco was responsible for the concrete work. John Bricker of McGeorge, Inc., was the Project Manager over the joint venture. The blasting required in excavation was supervised by Arkansas Explosives, Inc. of Little Rock, Arkansas, and grouting was conducted by Judy Company of Kansas City, Missouri.

The contractor was required to establish and maintain an effective quality control system consisting of plans, procedures, and organization to insure the contract requirements in materials, equipment, workmanship, fabrication, and construction operations. A quality control system manager from within the contractor's organization was required to be at the work site, with responsibility for regulating all quality control matters. A fully qualified staff was required under the system manager with necessary experience and technical training to perform all quality control activities. Records and tests of the contractor's quality control throughout the construction operations were furnished to the Government, as directed by the Contracting Officer. The entire work was subject to inspection and testing by the Government prior to acceptance.

Don Cahoon, Project Superintendent (Civil) of McGeorge, Inc., was the designated Quality Control Officer with responsibility and authority to correct any deficiencies. David Moore, Project Superintendent (Structural) of Valco, Inc., was the designated Assistant Quality Control Officer. Quality Control testing was subcontracted to Anderson Engineering and Testing Company of Little Rock, Arkansas. The Quality Assurance for the project was provided by the Corps of Engineers and supervised by W. H. Hashbarger, Dardanelle Resident Engineer, and Jack Wilson, Project Engineer.

## PART II

### FOUNDATION EXPLORATIONS

2-01. Investigations Prior to Construction. The primary subsurface investigations were conducted in Fiscal Year 1978 and involved 265 exploratory drill holes. The following list shows the quantities and types of these investigations. Some drill holes are listed twice since they contained both soil and rock borings. This gives the list a total of 321 borings which represents the various boring methods rather than the actual number of drill holes. The logs of borings for the main embankment, dike, and outlet works are included in the appendix.

Location	Number of Borings	Linear Feet	Soil Samples		
			Undisturbed	Jar	Bag
Dam Site					
Core Boring, NX Vertical	33	2244.3	---	---	---
Core Boring, 4" Vertical	1	47.3	---	---	---
Standard Penetration	20	200.5	---	119	---
Piston Sampler	22	350.5	118	179	13
Auger Borings	10	43.6	---	14	---
4" Splitspoon	4	14.8	---	5	6
Spillway Site, Right Abutment					
Core Boring, NX Vertical	2	127.5	---	---	---
Auger Borings	15	52.3	---	28	18
Left Abutment Ridge					
Core Boring, NX Vertical	1	46.4	---	---	---
Auger Boring	2	35.0	---	3	---
Dike					
Core Boring, NX Vertical	10	482.1	---	---	---
Standard Penetration	9	98.5	---	46	---
Piston Sampler	5	37.3	9	20	---
Auger Borings	1	7.8	---	4	---
Borrow Area "A"					
Auger Borings	154		---	489	180
Borrow Area "B"					
	32		---	74	24
TOTALS	321	3787.9	127	981	241

Between October 1978 and August 1979, there were 37 additional holes drilled to determine the subsurface conditions for the spillway, outlet works, and embankment. All of the holes were combinations of soil and core borings. Samples of the rock core obtained from the outlet works foundation were tested for bearing strength and shear strength.

All of the exploratory borings were drilled by the Little Rock District, Corps of Engineers, using a Failing 1500 truck mounted rig. Overburden samples of the main embankment and dike foundations were obtained using a thin walled tube with piston, and split spoon samplers. The borrow materials were investigated by drilling a grid of auger holes spaced on 400-foot centers. All soils were classified according to the Unified Soils Classification System. The core holes were logged to give geologic descriptions and show the results of water pressure tests. Selected soil samples were tested to define the shear strength parameters. The borrow material and some of the foundation overburden were tested for natural water content in percent dry weight, plasticity index, and liquid limit.

2-02. Investigations During Construction. There was no exploratory drilling or other foundation investigations during construction. However, holes were drilled during construction for presplitting of rock faces, setting steel anchors, drain holes, and foundation grouting. This drilling is described where applicable in the following sections of this report.

## PART III

### GEOLOGY

3-01. Regional Geology. The Conway Water Supply Project is located in the north-central Arkansas Valley. Topographically, this is the low rolling flood plain of the Arkansas River which is bounded to the north and south by ridges and mountains reaching heights above 2,800 feet. The valley is a structural basin, or synclinorium, which is bounded to the north by the Boston Mountains of the Ozark Dome and to the south by the Ouachita Mountains, an anticlinorium. The valley extends eastward to the Mississippi Embayment and westward to the Interior Lowlands of Oklahoma. Structurally, the Arkansas Valley is a transitional province between the adjoining provinces to the north and south. Folds in the valley are more closed toward the intensely folded Ouachitas to the south, but become progressively more open toward the less intricately folded Ozark Dome to the north. Thrust faults which are typical of the Ouachita Mountains are common in the valley south of the Arkansas River. Normal faults which are downthrown to the south are typical of the Boston Mountains and are common in the valley north of the Arkansas River. Formations throughout the valley consist mostly of shale and sandstone of the Pennsylvanian Period with a few igneous intrusions thought to be of the Cretaceous Period. These formations are mostly unfossiliferous, seldom calcareous, often carbonaceous, and sometimes contain coal.

3-02. Site Geology. The local geology was similar throughout the project. The foundation consisted of the same rock formation over the entire area, however, there were a few variations in specific rock characteristics and conditions, which will be discussed in Part VI of this report.

a. Physiography. The project site is located where the northern Arkansas Valley rises to meet the southward sloping Ozark Highland Physiographic Province. Differential erosion of gently dipping sandstone and shale has formed this into an area of narrow ridges and broad valleys. The landforms trend east-west with the local and regional structure in most cases. Ridges, such as the one forming the dam abutments, are normally capped with the harder, erosion resistant sandstone or the more sandy shale. Valleys are usually eroded in the less resistant shale or in the weakened rock along fault traces. The dam valley, however, is formed by a 550-foot-wide gap incised through a typical east-west trending ridge. The dam abutments rise about 85 feet above the flood plain, but topographic relief in the area reaches about 150 feet.

b. Overburden. The dam abutments were covered with residual soils and colluvium consisting of sandy clay, clayey sand, and silt. Detrital fragments and float rock of the sandstone caprock were scattered along portions of the upper abutment slopes. Overburden thickness ranged from about 5 to 14 feet on the left abutment and from about 1.5 to 11 feet on the right abutment. The alluvial deposits of the valley average about 20 feet in depth and consisted mainly of sandy clays and clayey sands with occasional silt and silty sand. At the dike, overburden consisted of about 8 to 16 feet of residual sandy clay which graded into the weathered parent rock, sandy shale. It often contained detrital fragments and some float.

c. bedrock Formation. The entire project area is underlain by the Atoka Formation of the Pennsylvanian Period. The Atoka is reported to be over 9,480 feet thick near Perryville, Arkansas, but about 5,000 feet thick at the dam site. It is a formation of interbedded sandstone and shale with the shale usually predominating. Other than the sandstone in the spillway foundation and capping the dam abutments, the project structures are completely underlain by shale.

The Atoka shale is typically a gray to black carbonaceous shale which weathers to a dull gray or buff and is sometimes micaceous or silty. Locally, the shale was hard to moderately hard, sandy, well compacted and cemented, and usually micaceous. It was often splintery and would readily air slake in places. Sand composition varied throughout the site, and in some cases it approached shaley sandstone. Although most of the shale in the foundation is sandy to some degree, it becomes pure shale at about 40 to 45 feet below the main embankment.

The sandstone beds throughout the Atoka Formation range in thickness from a few inches to more than 100 feet. It is usually dark to light brown or gray, medium to fine grained, commonly micaceous, and often ripple marked or crossbedded. The sandstone in the spillway foundation and capping the dam abutments was hard, fine to medium grained, micaceous, and gray, except where it is weathered and iron stained to reddish brown. The base of the Atoka can sometimes be recognized by a strata called the "Millstone Grit," a thick bedded sandstone containing light colored, water-worn pebbles.

d. Bedrock Structure. The project is located on a broad, gently sloping homocline formed by the southward dipping limbs of the Arkansas Valley Basin and the Ozark Dome. Local structure trends east-west as does the Solgohachia Anticline and the Greenbriar Syncline, which flank the project to the north and south, respectively. The limbs of these folds dip from 2 degrees to 15 degrees but the formation dip at the project site ranges from 2 degrees to 7 degrees southward. Normal faults are common in the area and are often downthrown to the south augmenting the regional basin structure. Although no major faults were encountered in the dam foundation, there were minor displacements along bedding planes in the left abutment. The U.S.G.S. Geologic Map of the Menifee Quadrangle shows a fault trending east-west across the dike foundation, but there were no indications of this fault other than a small distorted fold in the weathered shale above firm rock. There is a major set of nearly vertical joints throughout the project with strikes which average from 12 degrees to 16 degrees northeast. The joints usually dip toward the northwest at 82 degrees to 90 degrees. Otherwise, joints occur occasionally at various attitudes, but for the most part they trend to the northeast.

e. Bedrock Weathering. Weathering throughout the project was aided by open fractures and joints which were conducive to groundwater movement, slope saturation, and freeze-thaw processes. Some of the shale was susceptible to slaking and would deteriorate into small chips when exposed to air. Therefore, care was taken during construction to protect foundation rock from unnecessary exposure at final grade.

Significant bedrock weathering was minimal in the dam valley but more pronounced in the abutments and the dike foundation. The shale in the dam valley was weathered less than a foot in depth, and firm rock was often encountered almost directly beneath the alluvium. However, it was sometimes more than 14 feet to firm shale in the dam abutments, and the shale foundation at the dike was weathered as deep as 8 to 10 feet in places. The sandstone in the spillway foundation and abutment caprock was rather resistant, with little deterioration from weathering.

f. Ground Water. Hydraulic pressure tests in project bore holes indicated that the foundation rock was generally impermeable as expected for shale, but that permeable zones existing in the formation due to open joints, fractures, and bedding planes. The water table was at an average of 5 feet below the valley surface and from there it rose about 15 feet in the lower abutments, according to water level readings in exploratory bore holes. Artesian water was encountered in some of the grout holes drilled in the valley, and occasional springs seeped water into the valley excavations. There were two springs in the stilling basin excavation, one with a flow rate of 5 gallons per minute and another which flowed at one-half gallon per minute.

g. Seismicity. The project is in a Seismic Risk Zone I which indicates that only minor damage would be expected from earthquakes. Therefore, a seismic coefficient of 0.05G was used in the structure design. Only earthquakes of minor intensity have occurred in the project area, and local activity usually amounts to only infrequent tremors. In early 1982, however, numerous tremors occurred in the project area. Most of these tremors were very minor and almost imperceptible, but a few were in the range of 3 to 5 on the Richter Scale. One of the quakes had an epicenter near Naylor, Arkansas, which is about 23 miles southeast of the dam; it occurred on 20 January 1982 and registered 4.5 on the Richter Scale. Although this earthquake was noticeable, it was considered minor and caused no apparent damage.

The most noted earthquake area in the region is about 140 miles northeast of the project near New Madrid, Missouri. In 1811 and 1812, earthquakes in this vicinity reached the top of the Modified Mercalli Scale with an intensity of XII. The New Madrid area is now classified as a Seismic Risk Zone III, in which major earthquake damage could be expected. A Seismic Risk Zone II of expected moderate damage is roughly concentric about the Zone III and includes most of northeast Arkansas.

h. Engineering Characteristics of Overburden. Overburden throughout the project foundation consisted mostly of sandy to silty clay and clayey sands. This is an impervious material with fair to good shear strength and medium to low compressibility when compacted and saturated. It has fair to good workability as a construction material and is considered suitable for foundation material when seepage control is important. There was also occasional silt and silty sand in the overburden, particularly in the dam's valley section. Silt and silty sand are semipervious to impervious with fair to good shear strength and low to medium compressibility when compacted and saturated. Overburden samples taken in the valley along the dam's centerline had a water content ranging from 6 to 30 with an average of 22, a liquid limit ranging from 20 to 44 with an average of 29, and a plasticity index ranging from 4 to 23 with an average of 11.

i. Engineering Characteristics of Bedrock. The foundation bedrock is shale of the Atoka Formation in every structure except for sandstone in portions of the spillway. The sandstone is a hard, resistant material favorable for the spillway foundation, but formed a relatively small amount of the total bedrock. The shale is hard to moderately hard, massive, well compacted, and provided good core recovery which indicated competent foundation rock. The shale is inherently impervious, but hydraulic pressure tests revealed pervious zones created by open fractures, joints, and bedding planes. For design purposes, the shale was considered to have a cohesion of 6.12 t.s.f. (tons/sq.ft.) and an angle of internal friction of 31 degrees ( $\tan=0.6$ ). Based on these properties, the allowable pressure on firm rock was 12 k.s.f. (kips/sq.ft.). An increase of 33-1/2 percent was allowed for earthquake and wave forces, and as stated previously, seismic forces were based on an acceleration of 0.05 G.



## PART IV

### SPECIAL DESIGN CONSIDERATIONS

4-01. Construction Method. Several approaches to the dam design were initially considered after the project requirements were developed. A stage construction method was studied, which would have allowed time for the alluvial foundation to gain strength. Also, a very flat sloped embankment was considered, which would have been constructed without removal of the alluvial foundation. However, it was decided that the foundation alluvium should be removed to the top of rock, and excavation would extend to the top of firm rock in the core trench. This design was favored because it eliminated several problems such as stage construction in relatively small quantities, potential liquifaction of the sands, costly seismic design analysis, possible seepage control needed along the downstream toe of the dam, and post-construction embankment settlement due to soft foundation.

4-02. Embankment Stability. The stability of the embankment was analyzed using conditions for the downstream slope at the end of construction, for partial pool, for sudden drawdown (between maximum pool and bottom of water supply pool), and for steady seepage. The computed critical safety factors for each of these conditions were respectively 1.9, 2.0, 1.4, and 1.7. The factors of safety required by EM 1110-2-1902 for these same respective conditions were 1.3, 1.5, 1.0, and 1.5.

4-03. Structure Uplift. All structures were designed for 100 percent uplift except for the stilling basin which was assumed to be relieved 50 percent by drains.

4-04. Earthfill Pressure. The earthfill was assumed to exert an at-rest pressure with  $K=0.8$  and  $K=0.7$  for the stilling basin backfill. The resultant was applied at  $0.38H$  above the base. The  $K$  for active earth pressure was taken as 0.5.

4-05. Ultimate Strength Design. For ultimate strength design, a load factor of 1.8 was used. The capacity reduction factor was 0.9 for flexural members, and 0.7 for flexural members with significant axial loading. The capacity reduction factor for shear was 0.85.

4-06. Wave Forces. The significant wave height and length was based on an effective fetch of 1.097 miles, a wind velocity of 54 m.p.h., and a minimum wind duration of 18.0 seconds.

## PART V

### EXCAVATION PROCEDURES

5-01. General. Most of the excavation closely followed the lines and grades indicated in the plans and specifications. All permanent construction areas were stripped to an average depth of about one foot to remove unsuitable material such as topsoil, roots, stumps, and other organic matter. Excavation was classified for payment purposes as either rock or common, according to the determination of the contracting officer. Rock excavation was considered as the removal and disposal of shale and sandstone from their natural positions, including all boulders measuring more than one cubic yard. Common excavation was considered that which was not otherwise classified as rock. The contractor was responsible for maintaining the finished grade at all times; however, some deviation tolerances were allowed. The general tolerance for rock excavation was plus or minus 6 inches. The tolerance on close line drilled and presplit faces was a plus 3 inches with no minus allowances.

5-02. Excavation Equipment. The major excavation machinery was Caterpillar 631 and Terex TS18 scrapers. The scrapers were assisted by dozers and rippers where needed. Excavation of the overburden in the valley began with scrapers, but when the material became too soft and loose, Bucyrus Erie 65-D and 35-B draglines were used. Bulldozers on the job ranged from D-5 to D-9 Caterpillars and a TD-25 International. There were also Euclid end dump trucks, 950 loaders, backhoes, a wheel-type farm tractor, and a 12F motor patrol grader.

5-03. Dewatering System. A well point system was initially rented from Stang Hydronics to provide a dewatering system for the dam construction. The wellpoint pumps were Stang Model 708-1, size 8x6, and driven by 2-53 or 2-71 Detroit diesel engines. Standard non-self-jetting 1-1/2-inch wellpoints were used with 1-1/2-inch risers. The header pipe was 8-inch PVC pipe modified for wellpoint attachment on 5-foot centers. The wellpoints were installed by water jetting an 8-inch jet casing to the top of rock where the wellpoints were set within a surrounding sand filter. A 6-inch flowmeter was installed in the discharge line to record the volume of discharge. The system was installed about 5 feet outside of the crest line for excavated slopes with wellpoints spaced on 5-foot centers. However, the system did not work for this jobsite due to impermeable soils and excavations which bottomed on solid rock. Groundwater in the foundation was often at the overburden-rock contact or below and, therefore, difficult to pick up with wellpoints.

The contractor devised a plan to use shallow ditches, clay dikes, sandbag dikes, and appropriately located sump pumps for dewatering rather than wellpoints. Water was channeled to sumps by use of shallow ditches or dikes as applicable and then pumped over the cofferdams to the downstream runoff area. Pumping to the sumps from low areas in the rock surface was accomplished with small pumps such as 2- or 3-inch trash pumps. The water was then removed with a 6-inch sump pump capable of pumping 1,000 gallons per minute with a 100-foot head.

5-04. Excavation Blasting. Blasting was performed with Tovex T-1, a tubular water gel explosive manufactured by Du Pont, and with ANFO, ammonium nitrate fuel oil. Most of the blasting was done with Tovex T-1 which has a density of 0.25 lb./ft. (net explosive), a velocity of 6,800 M/Sec., and is packaged in one inch O.D. x 50 ft. coiled tubes. Originally, the specifications would not permit the use of ammonium nitrate as an explosive, but due to a value engineering change, it was allowed with Tovex in blasting the spillway excavation. However, the use of ANFO explosive was restricted to beyond 75 feet from the spillway crest and 5 feet from presplit faces.

Blasting with any explosive was not permitted within 100 feet of the intake structure or the outlet conduit while or after the concrete was placed. No blasting was allowed within 100 feet of foundation grouting, during or after grouting operations.

The blast holes were drilled according to specifications and patterned under supervision of the blasting contractor, Arkansas Explosives, Inc. For general rock excavation, blast holes were not allowed to be drilled deeper than two-thirds of the remaining depth to final grade, and in no case was the bottom of holes allowed closer than 6 inches from the final grade. The blast holes in the spillway excavation ranged from 3 to 4 inches in diameter and were usually spaced in 8'x12' or 10'x14' patterns. However, other patterns were also used, such as 4'x4', 6'x9', 7'x8', 7'x9', 7'x11', and 9'x12'. The wider patterns were used for the greater hole depths and the more narrow patterns for shallow holes. In presplitting excavations, 3- to 3-1/2-inch-diameter holes were drilled at 2-foot intervals along the desired break line and to the full depth of the cut; Tovex (0.25 lb./ft.) was loaded in every other hole.

5-05. Foundation Preparation. Horizontal surfaces of the rock foundation were protected by a 6- to 12-inch layer of unexcavated rock which was not removed to grade until the contractor was ready for placement of embankment material, reinforcement steel, or concrete. The drilling and grouting operations were performed on this protective layer to prevent damage and deterioration of the final foundation surface. The protective layer was easily and quickly removed for final cleaning just before placement of the construction material. At this time the rock surface, joints, and fractures were cleaned of dirt and loose drummy material by barring, picking, wedging, sweeping, and finally by washing or air jetting.

Open joints and fractures were cleaned of loose and weathered material and then filled and sealed with concrete or cement mortar. Areas with vertical faces and overhangs were either sloped off or a concrete fillet was placed in the recesses to allow proper compaction of the impervious fill. Rock surfaces upon which concrete was to be placed was required to be kept continuously wet for 24 hours immediately prior to the concrete placement.

5-06. Left Abutment Excavation. Excavation on the left abutment followed the lines and grades of the contract drawings with no problems. The upper abutment slopes above elevation 305 were stripped to a depth of about one foot within the embankment area. Below elevation 305, the overburden was sloped at 1 vertical on 2 horizontal to the top of rock, which was at about elevation 289. The rock abutment extended from elevation 289 to elevation 264

at the top of rock in the valley floor. The surface in this area was scaled to remove loose and drummy rock prior to placement of embankment material. Care was taken that the rock slope would be no steeper than 4 vertical on 1 horizontal. The core trench in the left abutment was excavated to firm rock and extended from centerline station 16+20 to 22+43.

5-07. Valley Excavation. Excavation in the valley section removed a thickness of about 22 feet of overburden from approximate elevations 286 to 264. The top part of bedrock in the valley was weathered less than a foot in depth. This weathered zone was removed with the overburden and as a result, no further excavation was required in order to extend a core trench to firm rock, since the entire embankment foundation was excavated to firm rock. Therefore, the valley excavation was roughly on one horizon with no core trench along the axis as originally illustrated in the contract drawings. The excavation extended to the embankment toe limits which was 253 feet upstream of the dam axis at elevation 283 and downstream 232 feet from the axis at elevation 284.

Excavation slopes along the embankment toe were 1 vertical on 2 horizontal, and there were no problems in attaining the specified lines and grades. Small but persistent seeps of groundwater occurred intermittently throughout the valley excavation, and these areas were dewatered ahead of the embankment placement. Open joints and fractures were cleaned and filled with concrete or mortar as required. The rock surface was cleaned and prepared for embankment placement as described in paragraph 5-05.

5-08. Right Abutment Excavation. Excavation on the right abutment was somewhat different from that for the left abutment, due to a bench and adjoining rock face required for the outlet works foundation. The upper abutment slopes above elevation 335 were stripped to a depth of about 1 foot within the embankment area. Below elevation 335, the abutment was sloped in overburden at 1 vertical on 3 horizontal for the most part. However, it was transitioned to 1 vertical on 1 horizontal upstream of the intake structure and to 1 vertical on 2.5 horizontal along the lower outlet channel. At the top of rock, approximate elevation 325, the slope was changed to 4 vertical on 3 horizontal to form the rock face adjacent to the outlet works. The foundation bench for the outlet conduit was at the base of this rock face and extended in width from Station 11+02 to Station 11+75 on the dam axis. It was excavated to the elevation for the bottom of the outlet conduit which varied from elevation 284 upstream to elevation 281 downstream. The rock abutment sloped downward from the bench to near elevation 266 at the top of rock in the valley floor. The slope surface was no steeper than 4 vertical on 1 horizontal and was scaled to remove loose and drummy rock prior to placement of embankment materials. The core trench in the right abutment extended from Station 8+71 to 10+70 on the dam axis and was excavated to firm rock.

5-09. Core Trench Excavation. A core trench was excavated to firm rock along the dam axis from Station 8+71 to Station 22+43.44. The actual trench construction occurred only in both abutments, since the entire valley floor and the outlet conduit bench were excavated to firm rock. The trench was actually cut from Station 8+71 to 10+70 in the right abutment and from Station 16+20 to 22+43.44 in the left abutment. However, a 25-foot-wide strip along the centerline between Stations 10+70 and 16+20 was treated, inspected, and mapped as part of the core trench, although no actual trench was cut.

The trench was 10 feet wide from Station 8+71 to 9+70 where the walls tapered outward until the trench was 25 feet wide at Station 10+20. The trench foundation remained 25 feet wide to Station 19+50 where the walls tapered inward to a width of 10 feet again at Station 20+00. In the abutments, the trench walls were sloped at 1 vertical on 2 horizontal from the ground surface to the top of rock and at 1 vertical on 1 horizontal from the top of rock to the bottom of the trench in firm rock. There were no problems in the core trench excavation; lines and grades followed the contract drawings except for the absence of trench walls in the valley section. The geologic mapping of the core trends foundation is shown on sheets 13 through 17 of the plans.

5-10. Outlet Works Excavation. The outlet works excavation included the intake structure, the outlet conduit, the stilling basin, and the outlet channel. There were a few minor deviations from the specified lines and grades, but none of any major significance.

a. Intake Structure. The intake structure foundation extends along the outlet works centerline from Station 7+45.75 to Station 7+96.75. The excavation area for the wet well section was a 35-foot x 32-foot rectangle which extended from Station 7+45.75 to Station 7+80.75. The adjoining area for the drop inlet section was a 16-foot x 8-foot rectangle which extended from Station 7+80.75 to Station 7+96.75. The geologic map of the intake structure foundation is shown on sheet 19 of plans.

Contract drawings indicated that the excavation should be 4 feet in depth proceeding from elevation 284.14 (the outlet conduit elevation) to elevation 280.14. The excavation was constructed to this elevation and depth except where several joints intersected near the center of the foundation. This area was excavated to a depth of 4-1/2 to 5-1/2 feet in order to remove broken rock.

b. Outlet Conduit. The foundation excavation for the outlet conduit had a minimum width of 6 feet 4 inches and extended 420.66 feet along the outlet works centerline from Station 7+96.75 to Station 12+17.41. The elevation dropped along the invert from 284.14 at the intake structure to 281.00 at the stilling basin. The adjacent right abutment was sloped at 4 vertical on 3 horizontal to the top of the conduit excavation, and at that point it was excavated to a 6-foot-9-inch vertical cut against which the conduit concrete was poured. The conduit sidewall was presplit with a small amount of overexcavation, due mostly to overbreakage in the rock formation. The geologic maps of the outlet conduit are shown on sheets 20 through 22 of plans.

c. Stilling Basin. The stilling basin excavation extended along the outlet works centerline from Station 12+17.41 to Station 12+86.91, 69.5 feet beyond the end of the outlet conduit. At the end of the conduit, the foundation began to widen progressively and slope downward from elevation 281 at Station 12+17.41 to elevation 272.9 at about Station 12+56. Beyond this point, the foundation was about 18 feet wide and horizontal. The west side of the excavation had a 10-foot-wide berm at about elevation 286, above which the abutment was sloped at 1 vertical on 3 horizontal. The east side of the excavation had a 3-foot-wide berm at elevation 274, above which the slope was

1 vertical on 1 horizontal. The excavation was presplit with a minor amount of overexcavation, due to overbreakage in the rock formation. The geologic map of the stilling basin excavation is shown on sheet 19 of plans.

d. Outlet Channel. The excavation for the outlet channel closely followed the contract specifications. It extended along the existing creek channel from Station 12+86.91 to about Station 16+08. The channel was curved by cutting an inside radius of 300 feet on the east bank and an outside radius of 350 feet on the west bank. The channel floor was at elevation 274 with side slopes of 4 vertical on 1 horizontal in rock and 1 vertical on 2.5 to 3 horizontal in overburden. A 10-foot-wide berm on the west side of the stilling basin also extended along the outlet channel to Station 13+60.

5-11. Spillway Excavation. The spillway was excavated according to contract drawings in a saddle of the right abutment. The excavation was 235 feet wide with sides sloped at 4 vertical on 1 horizontal in presplit rock and 1 vertical on 2 horizontal in overburden. The approach channel was given an adverse slope of 0.010. The exit channel was given a supercritical slope of .025 for 200 feet and then sloped at 0.0034 to where the channel daylighted in a natural ravine about 1,600 feet below the spillway crest.

5-12. Dike Excavation. An inspection-core trench was excavated along the dike alignment. The trench was 10 feet wide with 1 vertical on 1 horizontal side slopes. The core trench was excavated to firm rock between dike Stations 19+60 and 25+00 with the remaining inspection trench in overburden. The excavation followed contract specifications with no problems. Geologic mapping of the dike core trend is shown on sheet 18 of plans.

## PART VI

### CHARACTER OF FOUNDATION

6-01. General. The foundation proved to be very stable throughout the project. The Atoka was the only rock formation encountered and was relatively hard, massive shale for the most part. The strata dipped only slightly, and contained no major structural complexities. Joints and fractures which formed occasional permeable zones were sealed in the grout curtain with little difficulty, although some artesian groundwater was encountered.

6-02. Left Abutment Foundation. The foundation rock in the left abutment was predominantly massive, moderately hard to hard, gray to dark gray, sandy shale. The rock surface was relatively smooth overall; however, in places it was rough and somewhat broken due to air-slaking and fractures. Occasionally, small steps were formed by excavation along intersecting joints and bedding planes, most of which were only a few tenths of a foot in height. Most of the joints were in the nearly vertical, NE trending set common to the project area. These joints varied in strike from N5°E to N29°E and in dip from 90 degrees to 82 degrees NW. There were a few joints which trended from N68°E to N86°E and from N31°W to N79°W. There were some parted bedding planes, but otherwise low angle fractures were sparse. A few small joint displacements indicated minor faulting in the left abutment. From Stations 17+26 to 17+31, three joints were displaced about 0.2 foot along the formation bedding plane which had an apparent dip of 3°SE. A more prominent displacement was visible in the north wall of the core trench at about elevation 307. Several nearly vertical joints were displaced about 1.1 feet along the formation bedding plane, which had an apparent dip of 2 degrees SE. However, there were no slickensides, gouge, or other indications of faulting along the foundation floor on this horizon. The left abutment had no groundwater problems and was mostly dry except for occasional runoff dampness along bedding planes.

6-03. Valley Foundation. The surface of the valley foundation was relatively smooth, massive, sound rock consisting of moderately hard to hard, dark gray to black, sandy shale. The formation was nearly horizontal, but dips varied from 2 degrees to 6 degrees southward. Excavation along intersecting joints and bedding planes created occasional thin steps which were only tenths of a foot in height. Most of the joints typically trended NE and were nearly vertical; their average strike was about N14°E. Usually, joints and fractures appeared relatively tight on the foundation surface, and there were no displacements or other indications of faulting. An old stream channel formed a depression in the top of rock which ran diagonally from NW to SE in the NW quadrant of the valley foundation. There was some groundwater seepage into this depression which was removed by sump pumps, buckets, and sweeping. Bedrock in the old channel was nevertheless firm, hard shale which presented no foundation problems. Small, intermittent groundwater seepage occurred throughout the valley foundation, and there were artesian flows in some of the grout holes. However, the dewatering procedures and grouting operations successfully controlled these problems.

6-04. Right Abutment Foundation. The rock foundation in the right abutment was mostly moderately hard to hard, massive, gray to black, sandy shale. The rock surface varied from relatively smooth to somewhat broken in places where air-slaking and fractures were prevalent. Excavation along intersecting joints and bedding planes formed occasional small steps which were usually a few tenths of a foot in height; none were allowed to be over 2 feet high. The nearly vertical, NE trending set of joints were also prominent in the right abutment. These joints varied in strike from N6°E to N31°E and in dip from 90° to 76°NW. There were a few high angle joints striking NW from 12° to as much as 80°, but these were somewhat random rather than characteristic. In the rock slope between axis Stations 10+70 and 11+02, there were several joints dipping at 4° to 5°SE and striking N62°E. There were no indications of faulting, and no groundwater problems above the outlet works.

6-05. Outlet Works Foundation. The geologic mapping, photography, and inspection of the outlet works included the foundations for the intake structure, the outlet conduit, and the stilling basin. Foundation characteristics were generally similar for each of these features, but specific conditions varied from place to place.

a. Intake Structure. The foundation rock was moderately hard to hard, dark gray, sandy shale. The rock surface was relatively smooth for the most part, but broken in places. A set of five nearly vertical joints trended N25°E across the foundation. These joints were intersected in the downstream half of the foundation by three curved joints which trended roughly NW-SE and dipped about 60°NE. There were also a couple of similar curved joints in the NE corner of the foundation and a few random, irregular fractures. The joints and fractures were somewhat weathered in places with occasional iron staining. There were no faults or groundwater problems.

b. Outlet Conduit. The foundation surface was smooth, massive, sound rock consisting of hard to moderately hard, dark gray to black, sandy shale. Although jointing occurred intermittently throughout the conduit foundation, it was most pronounced in the upstream 110 feet of the alignment. Most of the joints trended NE and were nearly vertical with dips of 90° to 83°NW, and strikes ranged from N73°E to N4°E and averaged N14°E. However, occasional joints trended in other directions than NE, and there were some random, irregular fractures. There were no indications of faulting along any joint or fracture plane. An irregular clay seam of 1 to 2 inches in width occurred between conduit Stations 8+54 and 8+61. It appeared that this clay seam could be projected to connect with a clay-filled, NE trending joint in the right abutment near conduit Station 8+83. A rock slide occurred along this joint plane between Stations 8+54 and 8+83 when material was removed from the base of the abutment slope during early conduit excavation. When the slide debris was removed, it left a sloping and somewhat irregular abutment surface adjacent to the conduit alignment (see paragraph 7-05). Otherwise, the foundation was markedly smooth and hard with little jointing or fracturing from conduit Station 11+15 to Station 12+30 in the stilling basin. It was also very smooth and hard with only one tight fracture in the area where the conduit alignment crossed the dam axis. (Conduit Station 10+00 = dam axis Station 11+05).



c. Stilling Basin. Similar to the outlet conduit, the foundation rock in the stilling basin consisted of moderately hard to hard, dark gray to black, sandy shale with a typically smooth, massive surface appearance. Fracturing and jointing were relatively moderate. Joints had dips of 90° to 86°NW and strikes of N5°W to N11°E. Joints and fractures appeared tight with little weathering, and there were no indications of faulting. Sump pumps were required to remove water from the excavation due to a couple of springs in the west stilling basin wall. A spring occurred at outlet works Station 12+20 which flowed at 1/2 gallon per minute, and another was at Station 12+51 which flowed at 5 gallons per minute.

6-06. Spillway Foundation. The spillway foundation surface was smooth to somewhat rough, massive, sound rock. The rock consisted mainly of moderately hard to hard, dark gray to black, sandy shale, but downstream of spillway Station 11+50, it was hard, gray, fine to medium grained sandstone. Most of the joints trended NE and were nearly vertical. There were no indications of faults and no groundwater problems.

6-07. Dike Foundation. The dike foundation was smooth, massive, sound shale which was moderately hard to hard, dark gray to black, and sandy to very sandy in places. For a few feet at each end of the core trench, the shale was weathered, moderately soft to moderately hard, and brown to buff before grading into the overburden of the inspection trench. The jointing was nearly vertical and mostly trended NE with an average strike of N12°E. The firm foundation rock had no indications of faults; however, there was a small distorted fold in the weathered shale of the west core trench wall at Station 20+52. The dike foundation was well above the water table, and there were no groundwater problems.

## PART VII

### FOUNDATION TREATMENT

7-01. General. Foundation treatment included a grout curtain, drainage provisions, foundation anchors, and repair of a rock slide scar. However, the major foundation treatment consisted of the grout curtain to control leakage through the foundation rock and drainage curtain to relieve uplift pressure beneath the stilling basin. The foundation rock was relatively impermeable shale except for zones of permeability along open fractures, joints, and bedding planes. These permeable zones were detected prior to construction by exploratory drilling and water pressure tests. The investigations revealed that although much of the foundation would probably take little or no grout, there were a number of areas which would require grouting to seal potential seepage zones. Although the grout curtain was intended to reduce the flow of water through the rock strata beneath the dam, the stilling basin was designed with drainage holes to relieve uplift pressures by at least 50 percent.

7-02. Curtain Grouting. The grout curtain was constructed along the axis of the dam foundation between 8+50 and 22+40. The grout holes, which were EX size having a 1.485 inch O.D., were drilled with standard percussion drilling equipment using a track-mounted Chicago pneumatic drill. The holes were grouted by zones using the split spacing-stop grouting method. The entire grout placement required 408 grouting connections, 2,080.7 bags of cement, and a grouting time of 132 hours 20 minutes. Foundations grouting is shown on sheets 23 and 24 of the plans.

a. Grout Hole Inclinations. Most of the joints at the dam site ranged from high angled to vertical, and therefore, it was determined that the maximum interception of joints would be accomplished by drilling the grout holes at 30° from vertical. The holes drilled in the valley bottom and the left abutment were inclined 30° from vertical toward the left abutment. The holes drilled in the right abutment were inclined 30° from vertical toward the right abutment.

At two areas along the axis the grout holes were drilled in a fan pattern where four holes were drilled at 2.5-foot intervals on each side of a vertical hole with respective inclinations of 7.5°, 15°, 22.5°, and 30°. This formed a fan arrangement of 9 grout holes along 20 feet of the dam axis. The hole at 90°, two holes at 15°, and two holes at 30° were primaries, and the remaining four holes were secondaries. One fan was located at the base of the right abutment to form a transition between the grout holes inclined toward the left abutment and those inclined toward the right abutment. The central vertical hole of this fan was located at Station 12+22. The other fan pattern was located with the central vertical hole at Station 10+64, and was devised to grout the 4 vertical on 3 horizontal slope above the outlet conduit. An extra secondary hole was drilled at Station 11+02 near the base of the slope to intersect the bottom of the fan holes which were drilled from above the slope; this hole was drilled 70 feet into the right abutment at an angle of 45°.

b. Split Spacing. Split spacing was the procedure of locating additional grout holes midway between two previously grouted holes. The primary holes were drilled and grouted at 20-foot intervals to a depth of 70 feet. The secondary holes were then split spaced midway between the primary holes giving a final spacing on 10-foot intervals for most of the grout curtain. However, there were areas of significant grout consumption which were supplemented with split spaced tertiary and quaternary holes. If these holes proved tight during water pressure tests, it indicated that the previous grouting was effective, and the holes were backfilled rather than grouted. The secondary holes extended to a depth of 60 feet in the left abutment but averaged 45 feet depth elsewhere. The tertiary and quaternary holes were drilled to depths varying from 20 to 45 feet depending on the zones they were intended to check.

c. Stop-Grouting. Stop-grouting was the method used whereby each hole was drilled to its final depth and grouted by zones through a packer set at successively shallower stops. The areas beneath the packer settings which were to receive grout were termed zones, and the predetermined packer setting depths were termed stops.

d. Grouting Procedure. The grouting procedure involved five basic steps for each hole. First, after being drilled to its full depth, the hole was cleaned by applying water to the bottom and letting it overflow at the surface until the return water became clear. This removed any drill cuttings, slurry, or debris left in the hole after drilling. Second, the holes were water pressure tested and washed. All holes were tested and washed with clean water under continuous pressure at the required grouting stops and pressures. This washed open the permeable fractures in the grouting zone and gave a preliminary indication of grouting conditions. Third, the packer was placed in the hole at the lowest stop or grouting position predetermined for the hole. Fourth, grout was pumped into the zone at the pressure and mixes required. Finally, after the grout pressure dropped sufficiently, the packer was moved to the next higher stop, and grout was placed at the lower pressure required for that zone. This procedure continued until the grouting was completed throughout the hole. No grouting was allowed within a 100-foot section of any drilling in progress. Before grouting could begin in any hole, at least the nearest two holes in advance of that hole had to be drilled to final depth. Also, the adjacent hole had to be pressure washed to clean out any intervening seams and fractures.

e. Grout Injections and Mixes. The grout injections and mixes were controlled to suit the conditions encountered in each grouting zone. Neat cement grout was mixed in a water-cement ratio by volume and varied according to hole characteristics from 3.0 to 0.6. The procedure usually started with a 3.0 grout, the thinnest mix allowed by the contract specifications. Most of the holes were tight, or relatively tight, and in many cases no thicker grout was needed. At 3.0 or 1.0 grout was usually the final mixture for the more permeable zones. However, in a few cases where open joints and artesian flows were encountered, it was necessary to use an 0.75 or 0.60 mixture. Each zone was considered completely grouted when the rate of grout consumption using

the maximum required pressure was less than 1 cubic foot of mixture in 10 minutes. Grouting pressures varied according to the depth of packer stops beneath the top of the rock foundation. The pressures used were normally 1 p.s.i. for each foot of rock depth with allowances for the hydrostatic weight of the grout column. A 1.0 grout mix was used to backfill holes.

f. Grouting Conditions. Judy Company began grouting in Hole No. 14+20 on 12 September 1980. The operations proceeded well with no serious difficulties although occasional open joints were encountered and there were some artesian groundwater flows. The greatest grout consumption and the artesian flows occurred in the same general area indicating a more open joint system than in other parts of the foundation. The artesian flows were in the western valley section, and some large grout takes also occurred in that section, as well as in the lower right abutment. Artesian groundwater flows occurred in numerous holes between Stations 12+28 and 15+20, and there was often venting in adjacent holes during the grouting in this area. There were several holes between Stations 11+02 and 15+00 which had grouting zones that required bags of cement in the double digit amounts, but there were four holes which required over 100 bags of cement. The grouting conditions in these four holes were as follows:

Hole No. 11+48. Drilling was stopped when drill water was lost at the 48-foot depth. The packer was set at the 40-foot depth to grout the open zone. The grouting finally required an 0.75 mixture and took a total of 126.4 bags of cement in 1 hour and 50 minutes.

Hole No. 12+38. This was an old exploratory core hole which was found with an existing artesian flow. The hole was grouted below the 40-foot depth. This zone required a final grout mixture of 0.60 and took a total of 207.7 bags of cement in 2 hours and 19 minutes.

Hole No. 12+81. This was a grout hole which encountered an artesian flow below the 40-foot depth. When the zone below that depth was grouted, it required a 1.0 mixture and took a total of 139.7 bags of cement in 2 hours and 25 minutes.

Hole No. 13+74. This was a grout hole which was tight below the 40-foot depth but required final grout mixtures of 0.75 at both the 20-foot and 2-foot stops. The zone below the 20-foot stop took 124.3 bags of cement in 2 hours and 31 minutes, and the zone below the 2-foot stop took another 26.8 bags in 1 hour and 17 minutes.

Otherwise, the east valley section and both abutments were relatively tight. Most of the grout consumption at these locations was a 3.0 mixture requiring only tenths of a bag of cement. The largest grout consumption in the east valley section was 7.1 bags of cement below the 2-foot stop in Hole No. 15+30. This hole had some leaking through joints to the foundation surface. The largest grout take in the left abutment was 17.4 bags of cement below the 20-foot stop in Hole No. 18+40. The largest consumption in the right abutment was 17.5 bags of cement below the 2-foot stop in Hole No. 10+61.5. The final grouting operation was completed in Hole No. 12+84 on 19 March 1981.

7-03. Drainage Provisions. Drainage holes were drilled into the stilling basin foundation to relieve uplift pressures. The holes were percussion drilled with a minimum diameter of 3 inches at the final depth. They extended to a depth of 10 feet into rock and were slanted upstream 75° from the surface of the concrete slab. There were three holes drilled on the outlet works centerline at Stations 12+29.91, 12+39.91, and 12+49.91. At Stations 12+59.91, 12+69.91, and 12+80.91 a hole was drilled 2 feet 7 inches to each side of the centerline giving six additional holes. Therefore, there was a total of nine drainage holes throughout the stilling basin. These holes were drilled, as required by the contract specifications, after the dam's grouting operation was finished. All of the holes were cleaned by flushing with water and compressed air before final acceptance.

A vertical and horizontal filter drainage blanket was constructed in connection with the toe drain on the downstream side of the select impervious embankment. The filter material was a clean, free draining, well graded sand and gravel. The vertical filter blanket was 3 feet wide and extended along the downstream edge of the select impervious core from the top of this core at elevation 339.5 to the bottom of the horizontal filter blanket at elevation 286.0. The horizontal filter blanket was 2 feet thick and joined the vertical filter blanket at its base. The horizontal filter blanket extended laterally up the abutment slopes to elevation 339.5. It extended from the edge of the select impervious core, which was 35 feet downstream from the dam axis, to the toe drain, which was 216 feet downstream from the dam axis. The toe drain was a 12-inch, bituminous-coated, perforated, corrugated metal pipe wrapped in type "B" filter cloth. It was laid in a 3-foot-wide trench connected with filter material to the base of the horizontal filter blanket. The toe drain extended parallel to the dam axis and drained from east to west with respective invert elevations of 283.0 at the left abutment and 280.25 at the right abutment.

7-04. Foundation Anchors. Steel anchors were set in the foundation beneath both the spillway concrete control section and the stilling basin slab. No. 9 steel anchors were spaced along the spillway control section on 10-foot centers and were grouted into 3-inch-diameter, percussion-drilled holes which extended vertically 6 feet below the concrete. There were a series of nine anchors placed beneath each of the two stilling basin wingwalls. These were No. 11 steel anchors and were grouted into 3-inch-diameter, percussion-drilled holes that extended vertically 10 feet into the rock beneath the stilling basin slab.

The anchors were installed at least 6 days before concrete was placed over the foundation to allow proper setting time for the mortar. The mortar was a cement, sand, and water mixture proportioned into one part cement to two parts sand by dry weight with enough water for proper consistency. Each anchor hole was partially filled with mortar, and the anchor bar was vibrated to the bottom of the hole. Then, more mortar was added if needed to finish filling the hole. The bars were completely surrounded by mortar and not allowed to rest against the side of the hole.

7-05. Treatment of Slide Scar. Concrete fill was required along the scar of a rock slide which occurred on the right abutment slope above the conduit alignment. The slide left a relatively smooth scar on the upper abutment slope, but it was quite irregular and fractured adjacent to the conduit foundation. Therefore, it was decided to pour concrete fill against the slide scar where it adjoined the outlet foundation near elevation 281 (between Stations 8+54 and 8+83), in order to stabilize the fractured rock next to the relatively thin conduit wall. The concrete fill was placed to the top of the outlet conduit which was about elevation 288.

## PART VIII

### CONSTRUCTION MATERIALS

The earth materials used in the project construction consisted of riprap, bedding material, concrete aggregate, and sand. The riprap was syenite rock from the Granite Mountain Quarries in southeast Little Rock, Arkansas. Syenite consists mostly of feldspar minerals, and with an increase in its normally low amount of quartz, it would grade into granite. The bedding material was sandstone of the Atoka Formation from the M & M Rock Company quarry near Greenbriar, Arkansas. The concrete aggregate was a fluvial gravel obtained from an M & M Rock Company quarry located about 3 miles west of Toad Suck Ferry Lock and Dam. The sand supply was obtained from Jeffries Sand Plant near Cedar Park, about 2 miles north of Toad Suck Ferry Lock and Dam. Samples of these materials were tested by the Southwestern Division Laboratory in Dallas, Texas, and were approved for construction use.

## PART IX

### FOUNDATION PROBLEM AREAS

The foundation rock was sound and competent throughout the project, and no foundation problems are anticipated in the future. The rock was entirely Atoka Formation and consisted of hard to moderately hard, gray to black, usually sandy shale with some fine to medium grained, hard, gray sandstone. There were no major structural problems, and open joints and fractures were successfully sealed in the grout curtain. The small, low-angle faults in the left abutment showed no signs of intense movement such as gouge, breccia, or slickensides, but rather, appeared to be inactive, minor slippage along the shale bedding planes. There were some artesian groundwater flows in the valley foundation, but these were also sealed in the grout curtain. The grouting operations proceeded well with no significant difficulties and should provide an effective curtain beneath the embankment. The rock slide in the right abutment did no major damage and caused no construction problems other than extra concrete to smooth the scar adjacent to the outlet conduit. Therefore, the foundation appears quite good and should have no future problems.



## PART X

## RECORD OF FOUNDATION APPROVAL

The rock foundation was inspected, mapped, and photographed by a geologist after it was cleaned and prepared as described in paragraph 5-05. No drummy or loose material was allowed on the rock surface, and overhangs were removed or backfilled with concrete. Open joints and fractures were filled with mortar. Occasional, thin clay seams were cleaned to a depth of several inches and filled with mortar. The foundation was generally hard, massive rock which cleaned well and was usually approved with little difficulty. The following is a list of mapping and approval dates for various sections of the foundation:

<u>Structure</u>	<u>Date</u>	<u>Stations Mapped &amp; Approved</u>	<u>Geologist</u>
DIKE (core trench)	5 Sep 80	24+00 to 22+50	R. Crutchfield
	6 Sep 80	22+50 to 19+60	R. Crutchfield
	16 Sep 80	24+00 to 25+00	B. Jabarro
INTAKE STRUCTURE	13 Nov 80	7+45.75 to 7+97	J. Irwin
OUTLET CONDUIT	20 Nov 80	7+97 to 8+37	J. Browko
	11 Dec 80	8+37 to 8+57	R. Crutchfield
	31 Dec 80	8+57 to 8+97	R. Crutchfield
	26 Jan 81	12+16.75 to 11+16.75	R. Crutchfield
	27 Feb 81	11+16.75 to 10+76.75	R. Crutchfield
	9 Mar 81	10+76.75 to 10+36.75	R. Crutchfield
	10 Mar 81	10+36.75 to 9+96.75	R. Crutchfield
	10 Mar 81	8+97 to 9+76.75	R. Crutchfield
	11 Mar 81	9+76.75 to 9+96.75	R. Crutchfield
STILLING BASIN	24 Jun 81	12+16.75 to 12+38.91	R. Crutchfield
	30 Jun 81	12+38.91 to 12+62.91	R. Crutchfield
	16 Jul 81	12+62.91 to 12+86.9	J. Browko
DAM (core trench)	6 Oct 80	14+00 to 15+30	R. Crutchfield
	7 Oct 80	15+30 to 16+70	R. Crutchfield
	24 Mar 81	11+75 to 12+40	R. Crutchfield
	27 Mar 81	12+40 to 14+00	J. Browko
	11 Jun 81	11+02 to 11+75	J. Browko
	24 Jun 81	10+70 to 11+02	R. Crutchfield
	16 Apr 82	16+70 to 17+15	S. Hartung
	22 Apr 82	10+35 to 10+70	R. Crutchfield
	23 Apr 82	17+15 to 17+40	R. Crutchfield
	3 May 82	17+57 to 18+18	R. Crutchfield
	4 May 82	9+80 to 10+35	R. Crutchfield
	10 May 82	17+40 to 17+57	R. Crutchfield
	12 May 82	18+18 to 18+75	R. Crutchfield
	8 Jun 82	19+20 to 19+75	R. Crutchfield
	9 Jun 82	18+75 to 19+20	R. Crutchfield
	16 Jun 82	19+75 to 20+63	R. Crutchfield
	22 Jun 82	9+80 to 9+10	R. Crutchfield

APPENDIX A

PHOTOGRAPHS

Pages 000 thru 031



View east showing Phase I excavation and left  
effluent core trench in background.

21 Aug 60 Conway Water Supply Photo No. 1



View west showing Phase I excavation and right  
effluent in background.

4 Sep 60 Conway Water Supply Photo No. 2



View northeast along dam axis with foundation rock exposed in core trench from Stations 9+40 to 9+75 --- Atoka Shale.

22 Jun 62 Conway Water Supply Photo No. 3



View southwest along dam axis with foundation rock exposed in core trench from Stations 9+75 to 9+10 --- Atoka Shale.

22 Jun 62 Conway Water Supply Photo No. 4



View northeast at foundation rock exposed in  
core trench from Stations 9+75 to 10+20 ---  
Atoka Shale.

4 May 82 Conway Water Supply Photo No. 5



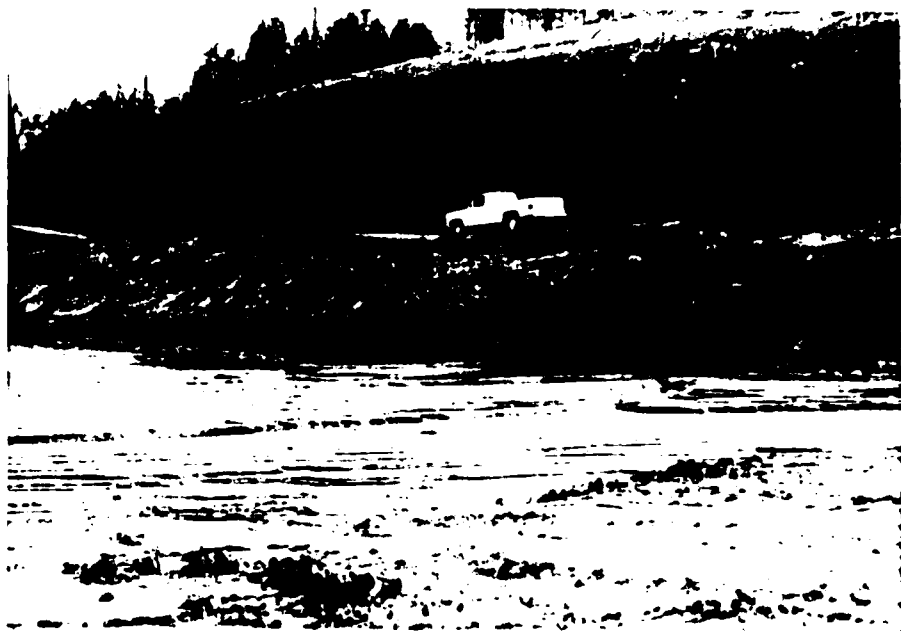
View southwest along dam axis with foundation  
rock exposed from Stations 11+74 to 11+10.  
Outlet conduit is in background with 4 vertical  
on 3 horizontal rock slope above it. Rock is  
Atoka Shale.

11 Jun 81 Conway Water Supply Photo No. 6



View south showing foundation rock: exposed in slope along dam axis between Stations 11+75 and 11+95 --- Atoka Shale.

24 Mar 81. Conway Water Supply Photo No. 7



View southwest showing foundation rock: exposed along dam axis from Stations 12+40 to 11+75, left to right. Note joints in right abutment in background. Rock is Atoka Shale.

24 Mar 81 Conway Water Supply Photo No. 8



View southwest toward Station 12+00 on dam axis  
in upper center photo. Note exposed Atoka Form-  
ation bedding planes.

26 Apr 81 Conway Water Supply Photo No. 9



View southwest toward Station 15+20 near pump  
in center-right of photo. Note foundation  
preparation of Atoka Formation.

7 Nov 80 Conway Water Supply Photo No. 10



View northeast along dam axis from Station 14+30. Note foundation preparation crew and left abutment core trench in background.

6 Nov 80 Conway Water Supply Photo No. 11



View east toward left abutment core trench showing exposed foundation rock along dam axis between Stations 16+20 to 16+58. Note concrete fill along rock ledges of Ato'a Shale.

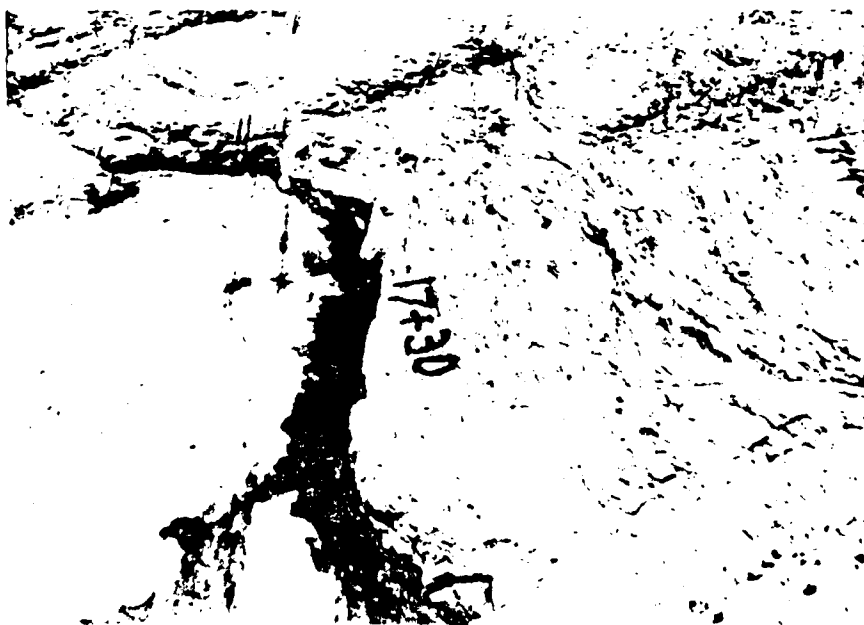
7 Nov. 80 Conway Water Supply Photo No. 12





View north showing exposed foundation rock a-  
long dam axis between Stations 17+20 and  
17+40 --- Atoka Shale.

23 Apr 82 Conway Water Supply Photo No. 13



View north on dam axis at Station 17+30. Note  
minor joint displacement in upper left photo.

23 Apr 82 Conway Water Supply Photo No. 14



View northeast showing exposed foundation rock  
along dam axis between Stations 17+40 and 17+  
70 --- Atoka Shale.

10 May 82 Conway Water Supply Photo No. 15



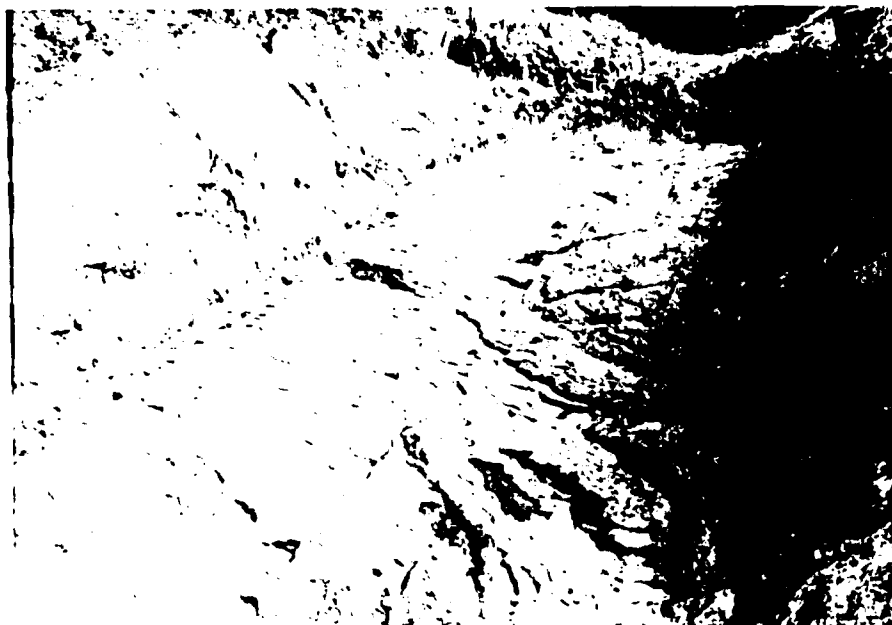
View northeast showing exposed foundation rock  
along dam axis between Stations 17+57 and 18+18.  
Note curve in core trench along dam axis. Rock  
is Atoka Shale.

3 May 82 Conway Water Supply Photo No. 16



View north at Station 13+10 in left abutment core trench. Note the 1.1 ft. displacement of nearly vertical joints along a bedding plane in center photo.

12 May 32 Conway Water Supply Photo No. 17



View northeast showing foundation rock exposed along dam axis from Stations 13+75 to 19+75 --- Atoka Shale.

9 Jun 82 Conway Water Supply Photo No. 18



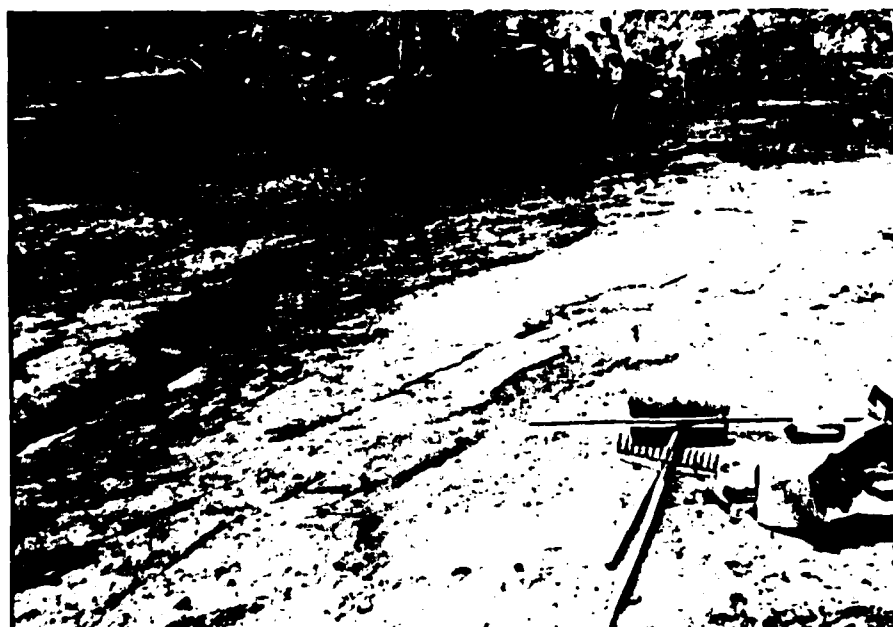
View north showing foundation rock exposed from Stations 20+45 to 20+63 in left abutment core trench. Note the blocky sandstone layer overlying the shale --- Atoka Formation

10 Jun 82 Conway Water Supply Photo No. 19



View southeast showing foundation preparation downstream of dam axis in Phase II excavation.

24 Mar 81 Conway Water Supply Photo No. 20



View southwest showing foundation preparation downstream of dam axis in Phase II excavation.

3 Apr 81 Conway Water Supply Photo No. 21



View west showing foundation preparation upstream of dam axis in Phase I excavation. Right abutment in background.

9 Oct 80 Conway Water Supply Photo No. 22



View east showing foundation preparation upstream of dam axis in Phase II excavation.

26 Mar 81 Conway Water Supply Photo No. 23



View north showing foundation preparation upstream of dam axis in Phase I excavation.

8 Nov 80 Conway Water Supply Photo No. 24



View north showing foundation preparation upstream of dam axis in Phase I excavation.

8 Nov 80 Conway Water Supply Photo No. 25



View northeast showing grout fill of open joint  
in Phase I excavation downstream of dam axis.

3 Nov 80 Conway Water Supply Photo No. 26



View northeast toward left abutment in upper  
photo. Note excavated rock and concrete  
fill along open joint in downstream Phase I  
excavation.

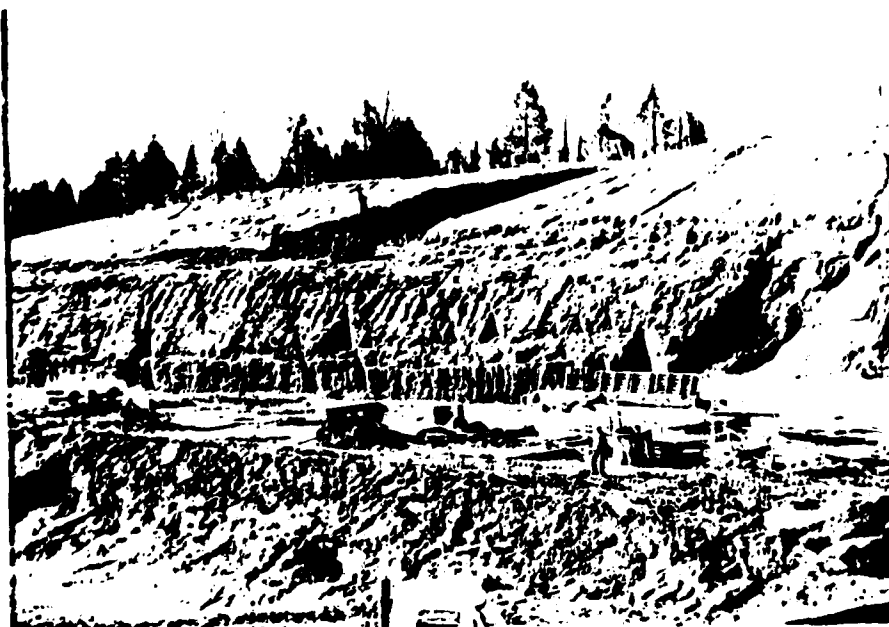
3 Nov 80 Conway Water Supply Photo No. 27





View west toward right dam abutment. Note intake structure and outlet conduit construction in center-right photo, grout hole drilling in core trench in center-left photo, and joints along rock face.

20 Sep 81 Conway Water Supply Photo No. 23



View southwest showing grout hole drilling in right abutment core trench at upper-center photo. Note joints and landslide scar in center-right photo.

20 Sep 81 Conway Water Supply Photo No. 29



View southwest showing grouting operation in left abutment core trench. Phase I excavation in background after a heavy rain.

30 Sep 80 Conway Water Supply Photo No. 30



View north showing grout hole drilling rig at about Station 12+00 on the dam axis.

10 Mar 81 Conway Water Supply Photo No. 31



View southwest along dike axis showing exposed  
foundation rock between Stations 24+00 and  
25+00 ---- Atoka Shale.

16 Sep 80 Conway Water Supply Photo No. 32



View northeast along dike axis showing exposed  
foundation rock between Stations 24+90 and  
24+00 ---- Atoka Shale.

16 Sep 80 Conway Water Supply Photo No. 33



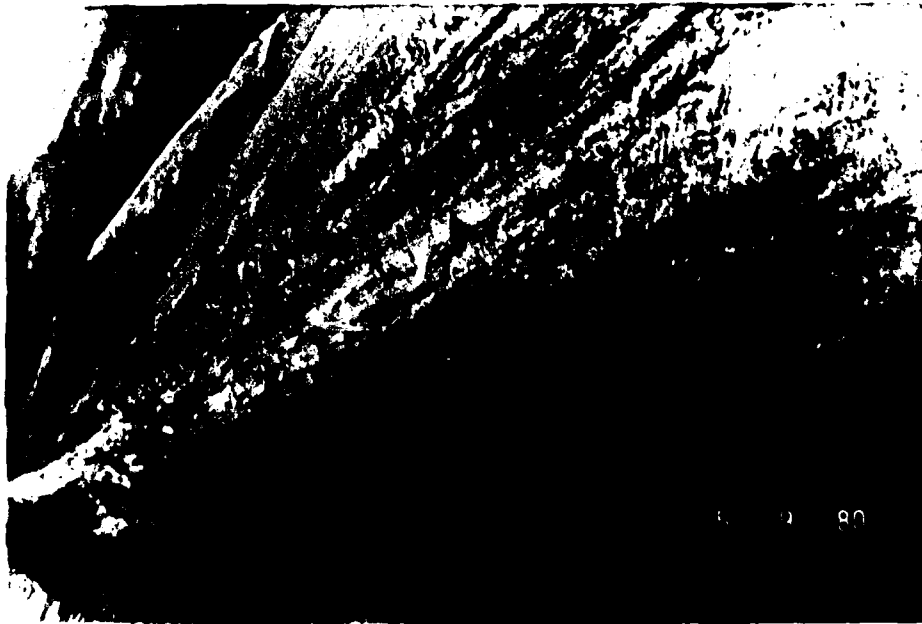
View northeast showing foundation preparation  
in dike core trench between Stations 24+70  
and 24+00. Work crew is at about Station  
24+00.

16 Sep 80 Conway Water Supply Photo No. 34



View northwest at distorted fold of weathered  
shale in core trench wall of dike at Station  
19+85.

6 Sep 80 Conway Water Supply Photo No. 35



View northeast from Station 24+00 in dike core trench showing exposed foundation rock --- Atoka Shale.

3 Sep 80 Conway Water Supply Photo No. 36



View southwest from Station 19+70 in dike core trench showing foundation preparation of exposed Atoka Shale.

6 Sep 80 Conway Water Supply Photo No. 37



View northwest showing foundation rock exposed  
in intake structure excavation --- Atoka  
Shale.

13 Nov 80 Conway Water Supply Photo No. 38



View northwest showing foundation rock ex-  
posed in intake structure excavation --- Atoka  
Shale.

13 Nov Conway Water Supply Photo No. 39



View west at rock slide scar in right abutment along outlet conduit Stations 3+63 to 3+83.

11 Dec 80 Conway Water Supply Photo No. 40



STA 8+37

View northwest along outlet conduit alignment from Station 8+37.

20 Nov 80 Conway Water Supply Photo No. 42



View southwest at rock slide scar in right abutment near outlet conduit Station 8+83.

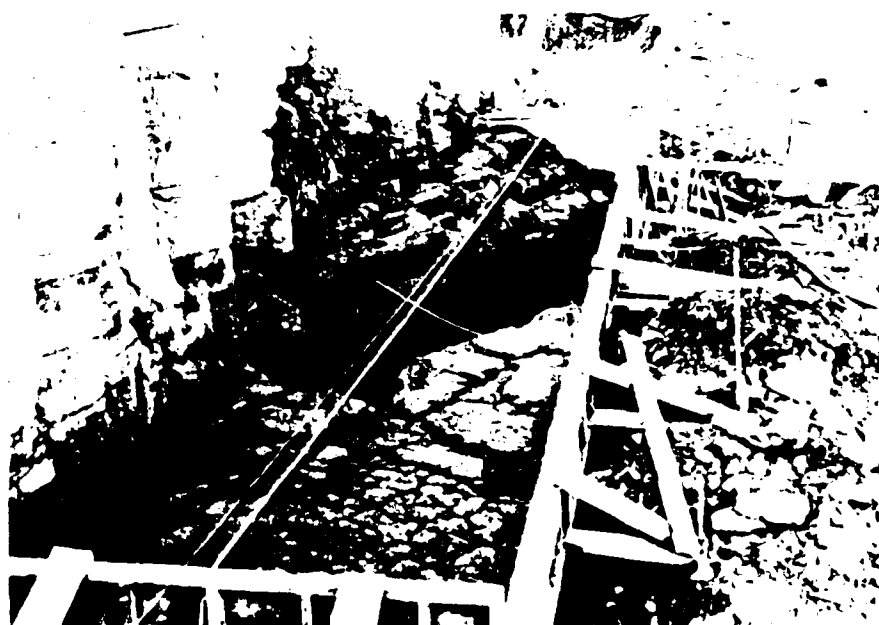
20 Nov 80 Conway Water Supply Photo No. 41





View southeast along outlet conduit alignment  
showing exposed foundation rock from Station  
8+57 --- Atoka Shale.

31 Dec 80 Conway Water Supply Photo No. 43



View northwest along outlet conduit alignment  
showing exposed foundation rock from Station  
8+97 --- Atoka Shale.

31 Dec 80 Conway Water Supply Photo No. 44



View southeast along outlet conduit alignment  
showing exposed foundation rock from Station  
3+41 --- Atoka Shale.

11 Dec 80 Conway Water Supply Photo No. 45



View northwest along outlet conduit alignment  
showing exposed foundation rock from Station  
9+60 --- Atoka Shale.

10 Mar 81 Conway Water Supply Photo No. 46



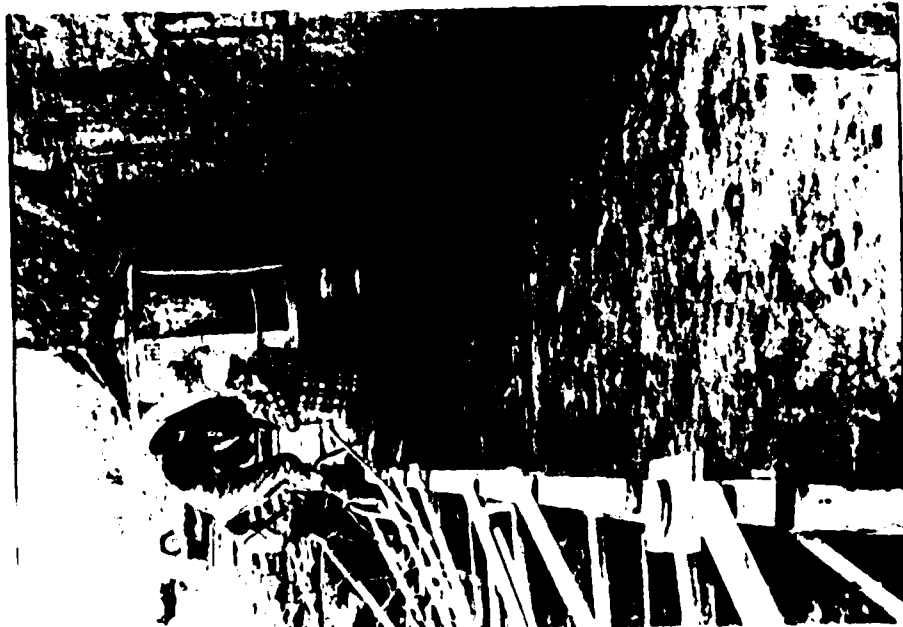
View northwest along outlet conduit alignment showing exposed foundation rock from Station 9+83 --- Atoka Shale.

11 Mar 81 Conway Water Supply Photo No. 47



View southeast along outlet conduit alignment showing exposed foundation rock from Station 9+97 --- Atoka Shale.

10 Mar 81 Conway Water Supply Photo No. 48



View southeast along outlet conduit alignment from Station 9+97, showing concrete pour.

11 Mar 81 Conway Water Supply Photo No. 49



View southeast along outlet conduit alignment from Station 10+70, showing exposed foundation rock --- Atoka Shale.

27 Feb 81 Conway Water Supply Photo No. 50



View northwest along outlet conduit alignment  
from Station 10+72, showing exposed foundation  
rock --- Atoka Shale.

9 Mar 81 Conway Water Supply Photo No. 51



View northwest along outlet conduit alignment  
from Station 10+96, showing exposed foundation  
rock --- Atoka Shale.

27 Feb 81 Conway Water Supply Photo No. 52



View southeast along outlet conduit alignment  
showing exposed foundation rock from Station  
11+17 — Atoka Shale.

25 Jan 81 Conway Water Supply Photo No. 53



View northwest showing outlet works align-  
ment from the stilling basin in left fore-  
ground to the intake structure in center-  
right of photo.

11 Feb 81 Conway Water Supply Photo No. 54



View northwest at upstream stilling basin foundation with outlet conduit construction in background.

13 Feb 81 Conway Water Supply Photo No. 55



View northwest at upstream stilling basin foundation from Stations 12+16.75 to 12+42.75 --- Atoka Shale.

13 Feb 81 Conway Water Supply Photo No. 56



View northwest at stilling basin foundation from  
Station 12+86.9 to 12+62.9 — Atoka Shale.

16 Jul 81 Conway Water Supply Photo No. 57



View north at blasting in spillway exca-  
vation.

29 Apr 81 Conway Water Supply Photo No. 58





View north at blasting in spillway excavation.

29 Apr 81 Conway Water Supply Photo No. 59



SPILLWAY RIGHT CUT SLOPE LOOKING  
UPSTREAM OVER CONCRETE CONTROL  
STRUCTURE PHOTO #60

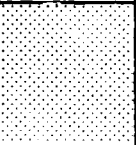
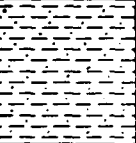
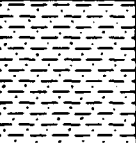
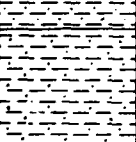
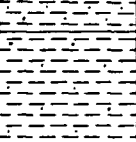
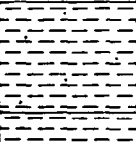
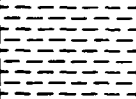
7 DEC 82 CONWAY WATER SUPPLY



SPILLWAY CUT LOOKING UPSTREAM  
OVER CONCRETE CONTROL STRUCTURE  
PHOTO #61  
7 DEC 82 CONWAY WATER SUPPLY

APPENDIX B

BORING LOGS  
Pages 032 thru 087

GENERALIZED GEOLOGIC COLUMN					
SYSTEM	FORMATION	SECTION	THICKNESS IN FEET	UNIT	DESCRIPTION
PENNSYLVANIAN	ATOKA		+ 7	10	<u>SANDSTONE</u> , HARD, FINE TO MEDIUM GRAINED, MEDIUM GRAY, MICACEOUS, FOUND ONLY IN THE HIGHER ELEVATIONS OF BOTH ABUTTMENTS AS A CAPPING STRATA, USUALLY SLIGHTLY WEATHERED.
			14 to 27	11	<u>SHALE, SANDY</u> , MODERATELY HARD TO HARD, CEMENTED, FINE GRAINED, BLACK TO MEDIUM GRAY, MICACEOUS, NUMEROUS SANDSTONE LAMINATIONS & INCLUSIONS, SOME LENSES OF SHALY SANDSTONE.
			13 to 48	12	<u>SHALE, SANDY</u> , HARD TO MODERATELY HARD, FINE GRAINED, CEMENTED, BLACK TO MEDIUM GRAY, MICACEOUS, NUMEROUS THICK TO THIN OFTEN IRREGULAR SANDSTONE LAMINATIONS & INCLUSIONS ZONES OF WHICH OCCASSIONALLY GRADE INTO SHALY SANDSTONE.
			11 to 27	13	<u>SHALE, SANDY</u> , HARD TO MODERATELY HARD, FINE GRAINED, CEMENTED, BLACK TO MEDIUM GRAY, MICACEOUS, NUMEROUS SANDSTONE LAMINATIONS & INCLUSIONS, OCCASSIONAL SHALY SANDSTONE LENSES.
			5 to 20	14	<u>SHALE, SANDY</u> , HARD TO MODERATELY HARD, FINE GRAINED, CEMENTED, BLACK TO MEDIUM GRAY, MICACEOUS, SCATTERED SANDSTONE LAMINATIONS & INCLUSIONS.
			7 to 24	15	<u>SHALE, SANDY</u> , HARD TO MODERATELY HARD, FINE GRAINED, CEMENTED, BLACK TO MEDIUM GRAY, WIDELY SCATTERED SANDSTONE LAMINATIONS & INCLUSIONS.
			+ 37	16	<u>SHALE</u> , MODERATELY HARD TO HARD, FINE GRAINED TO SILTY, BLACK, MICACEOUS, SCATTERED HARD SILTSTONE NODULES & LENSES ARE ENCOUNTERED IN THIS UNIT STARTING FROM ABOUT 10 TO 15' BELOW ITS TOP SURFACE.

Hole No. 6

DRILLING LOG		DIVISION SOUTHWESTERN		INSTALLATION LITTLE ROCK DISTRICT		SHEET 1 OF 2 SHEETS	
1. PROJECT CONWAY WATER SUPPLY				10. SIZE AND TYPE OF BIT NXL			
2. LOCATION (Coordinates or Station) N 0+06 E 11+30				11. DATUM FOR ELEVATION SHOWN (TBM or MSL) MSL			
3. DRILLING AGENCY U. S. CORPS OF ENGINEERS				12. MANUFACTURER'S DESIGNATION OF DRILL FAILING 1500			
4. HOLE NO. (As shown on drawing title and file number) 6				13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN		DISTURBED UNDISTURBED	
5. NAME OF DRILLER WOOD				14. TOTAL NUMBER CORE BOXES 6		15. ELEVATION GROUND WATER 289.8	
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG FROM VERT				16. DATE HOLE STARTED 1-20-78 COMPLETED 1-24-78			
7. THICKNESS OF OVERBURDEN 5.0				17. ELEVATION TOP OF HOLE 305.			
8. DEPTH DRILLED INTO ROCK 80.9				18. TOTAL CORE RECOVERY FOR BORING 98.9 %			
9. TOTAL DEPTH OF HOLE 85.9				19. SIGNATURE OF INSPECTOR R. PERRY			

ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOV. e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g
300.1			O.B.			BEGIN CORING
296.1			TOP OF ROCK			
			UNIT 12	91		1.2 CFM @ 4.5 PSI
	10		SHALE, SDY HD TO MOD HD WHERE UNWEATHERED	100	1	W.T. $\nabla$ 1-24-78
	20			75		0.0 CFM @ 12 PSI
				100	2	1.2 CFM @ 17 PSI
	30					0.0 CFM @ 20 PSI
						0.0 CFM @ 26 PSI
			UNIT 13	100		
	40		SHALE, SDY HD TO MOD HD	100	3	0.0 CFM @ 30 PSI
	50					0.0 CFM @ 30 PSI
			UNIT 14	100	4	
	60		SHALE, SDY HD TO MOD HD	100		0.0 CFM @ 30 PSI
					5	

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PROJECT

032

HOLE NO.

6

Hole No. 6

DRILLING LOG		DIVISION	INSTALLATION		SHEET 2 OF 2 SHEETS	
		SOUTHWESTERN	LITTLE ROCK DISTRICT			
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g
	70		UNIT 15 SHALE, SDY MOD HD TO HD	100		0.0 CFM @ 30 PSI
	80		UNIT 16 SHALE, MOD HD	100	6	0.0 CFM @ 30 PSI
200.0						BOTTOM OF HOLE 85.9'
			NOTE: FOR DETAILED DESCRIPTION OF UNITS - SEE GENERALIZED GEOLOGIC COLUMN			

033

Hole No. 13

DRILLING LOG		DIVISION SOUTHWESTERN		INSTALLATION LITTLE ROCK DISTRICT		SHEET 1 OF 2 SHEETS	
1. PROJECT CONWAY WATER SUPPLY				10. SIZE AND TYPE OF BIT NXL			
2. LOCATION (Coordinates or Station) 0+00 E 18+00				11. DATUM FOR ELEVATION SHOWN (TBM or MSL) MSL			
3. DRILLING AGENCY U. S. CORPS OF ENGINEERS				12. MANUFACTURER'S DESIGNATION OF DRILL FAILING 1500			
4. HOLE NO. (As shown on drawing title and file number) 13				13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN		DISTURBED 5 UNDISTURBED -	
5. NAME OF DRILLER NASH				14. TOTAL NUMBER CORE BOXES 5		15. ELEVATION GROUND WATER -	
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG. FROM VERT.				16. DATE HOLE		STARTED 2-21-78 COMPLETED 2-24-78	
7. THICKNESS OF OVERBURDEN 7.5				17. ELEVATION TOP OF HOLE 325.2			
8. DEPTH DRILLED INTO ROCK 80.0				18. TOTAL CORE RECOVERY FOR BORING 86 %			
9. TOTAL DEPTH OF HOLE 87.5				19. SIGNATURE OF INSPECTOR N. BOSTON			

ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g
317.7			O.B.			
			TOP OF ROCK			BEGIN CORING
	10	BADLY WEA C.L.	UNIT 12	38		
		BADLY WEA C.L.		25	1	
300.8	20	WEA Fe STAINS	SHALE, SDY MOD HD TO HD WHERE UNWEATHERED	93		0.0 CFM @ 15 PSI
FIRM ROCK	30			100		0.0 CFM @ 25 PSI
	40	SOFT JT			2	
		JTS		100		1.6 CFM @ 30 PSI
	50	JTS				
				97	3	1.0 CFM @ 30 PSI
	60		UNIT 13 SHALE, SDY HD TO MOD HD	100	4	0.3 CFM @ 30 PSI

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PROJECT

HOLE NO

13

034

Hole No. 13

DRILLING LOG			DIVISION	INSTALLATION		SHEET 2 OF 2 SHEETS	
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d		% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g
	70		UNIT 13 (cont)				
		JT	UNIT 14				0.0 CFM @ 30 PSI
		JT.	SHALE, SDY HD TO MOD HD				
		NUM FRAC					
	80	JT					0.0 CFM @ 30 PSI
237.6			SHALE, SDY UNIT 15 HD TO MOD HD				
	90		NOTE: FOR DETAILED DESCRIPTION OF UNITS - SEE GENERALIZED GEOLOGIC COLUMN				BOTTOM OF HOLE 87.6'

035



Hole No. 22

DRILLING LOG		DIVISION SOUTHWESTERN		INSTALLATION LITTLE ROCK DISTRICT		SHEET 1 OF 2 SHEETS	
1. PROJECT CONWAY WATER SUPPLY				10. SIZE AND TYPE OF BIT NXL			
2. LOCATION (Coordinates or Station) N 1+50 E 9+70				11. DATUM FOR ELEVATION SHOWN (TBM or MSL) MSL			
3. DRILLING AGENCY U. S. CORPS OF ENGINEERS				12. MANUFACTURER'S DESIGNATION OF DRILL FAILING 1500			
4. HOLE NO. (As shown on drawing title and file number) 22				13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN		DISTURBED 3 UNDISTURBED 5	
5. NAME OF DRILLER WOOD				14. TOTAL NUMBER CORE BOXES 9		15. ELEVATION GROUND WATER 303.9	
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG. FROM VERT.				16. DATE HOLE 3-3-78		17. ELEVATION TOP OF HOLE 347.0	
7. THICKNESS OF OVERBURDEN 5.3				18. TOTAL CORE RECOVERY FOR BORING 99.4		19. SIGNATURE OF INSPECTOR PERRY	
8. DEPTH DRILLED INTO ROCK 126.9							
9. TOTAL DEPTH OF HOLE 132.2							
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g	
341.6			O.B. TOP OF ROCK			BEGIN CORING	
	10		BADLY WEA SHALE, SDY MOD HD WHERE UNWEATHERED	100	1		
			C.L.	100			
328.6			SL WEA	84.9			
FIRM ROCK	20		Fe STAINS				
			UNIT 12	100	2	0.4 CFM @ 15 PSI	
	30		JT, Fe SHALE, SDY MOD HD TO HD	100		1.1 CFM @ 25 PSI	
	40		SOFT			0.8 CFM @ 30 PSI	
	50		JT BROKEN JTS	100	3	▽ W.L. 3-10-78 0.0 CFM @ 30 PSI	
	60		JT BROKEN JTS SOFT	100	4	2.2 CFM @ 30 PSI	

036

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PROJECT

HOLE NO. 22

Hole No. 22

DRILLING LOG		DIVISION SOUTHWESTERN		INSTALLATION LITTLE ROCK DISTRICT		SHEET 2 OF 2 SHEETS	
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g	
	70		UNIT 13 SHALE, SDY HD TO MOD HD	100	5	0.9 CFM @ 30 PSI	
	80			100		0.0 CFM @ 30 PSI	
	90		UNIT 14 SHALE, SDY HD TO MOD HD	100	6	0.0 CFM @ 30 PSI	
	100			100	7	0.0 CFM @ 30 PSI	
	110		UNIT 15 SHALE, SDY HD TO MOD HD	100	8	0.0 CFM @ 30 PSI	
	120		UNIT 16 SHALE MOD HD TO HD	100		0.0 CFM @ 30 PSI	
214.8	130	SILTSTS		100	9	0.0 CFM @ 30 PSI	
	140					BOTTOM OF HOLE 132.2'	
NOTE: FOR DETAILED DESCRIPTION OF UNITS - SEE GENERALIZED GEOLOGIC COLUMN							

037

Hole No. 32

DRILLING LOG		DIVISION	INSTALLATION		SHEET 1 OF 2 SHEETS	
1. PROJECT CONWAY WATER SUPPLY			10. SIZE AND TYPE OF BIT NXL			
2. LOCATION (Coordinates or Station) N 0+75 E 14+50			11. DAYUM FOR ELEVATION SHOWN (TBM or MSL) MSL			
3. DRILLING AGENCY US Corps of Engineers			12. MANUFACTURER'S DESIGNATION OF DRILL FAILING 1500			
4. HOLE NO. (As shown on drawing title and file number) 32			13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN		DISTURBED 9	UNDISTURBED 13
5. NAME OF DRILLER Nash			14. TOTAL NUMBER CORE BOXES 4		15. ELEVATION GROUND WATER --	
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG. FROM VERT.			16. DATE HOLE 3/3/78		COMPLETED 3/6/78	
7. THICKNESS OF OVERBURDEN 20.1			17. ELEVATION TOP OF HOLE 286.0			
8. DEPTH DRILLED INTO ROCK 51.3			18. TOTAL CORE RECOVERY FOR BORING 98 %			
9. TOTAL DEPTH OF HOLE 71.4			19. SIGNATURE OF INSPECTOR N. Boston			
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g
			OVERBURDEN			
265.9						
264.4	20		TOP OF ROCK			ROCK BIT
Firm Rock			UNIT 13	85 (0)		BEGIN CORING
	30		SHALE, SDY HD to MOD HD	100 (0)	1	0.7 CFM @10 PSI
	40		UNIT 14	100 (100)		0.0 CFM @20 PSI
	50		SHALE, SDY HD to MOD HD	100	2	1.44 CFM @30 PSI
	60		UNIT 15	100	3	2.0 CFM @30 PSI
			SHALE HD to MOD HD			0.0 CFM @30 PSI
			UNIT 16			

ENG FORM 1836  
MAR 71

PREVIOUS EDITIONS ARE OBSOLETE

(TRANSLUCENT)


PROJECT

HOLE NO

038

32

Hole No. 32

DRILLING LOG			DIVISION	INSTALLATION		SHEET 2 OF 2 SHEETS	
			SOUTHWESTERN	LITTLE ROCK DISTRICT			
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g	
214.6	70		UNIT 16 (Cont)	100	4		
			NOTE: FOR DETAILED DESCRIPTION OF UNITS - SEE GENERALIZED GEOLOGIC COLUMN			Bottom of Hole 71.4'	

039

Hole No. 33

DRILLING LOG		DIVISION Southwestern		INSTALLATION Little Rock District		SHEET 1 OF 2 SHEETS	
1. PROJECT Conway Water Supply				10. SIZE AND TYPE OF BIT NXL			
2. LOCATION (Coordinates or Station) N 0+00 E 16+15				11. DATUM FOR ELEVATION SHOWN (TBM or MSL) MSL			
3. DRILLING AGENCY U. S. Corps of Engineers				12. MANUFACTURER'S DESIGNATION OF DRILL Failing 1500			
4. HOLE NO. (As shown on drawing title and file number) 33				13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN		DISTURBED 12 UNDISTURBED 7	
5. NAME OF DRILLER Nash				14. TOTAL NUMBER CORE BOXES 4		15. ELEVATION GROUND WATER -	
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG. FROM VERT.				16. DATE HOLE 3-15-78		STARTED 3-16-78 COMPLETED	
7. THICKNESS OF OVERBURDEN 18.7				17. ELEVATION TOP OF HOLE 286.2		18. TOTAL CORE RECOVERY FOR BORING 100 %	
8. DEPTH DRILLED INTO ROCK 52.7				19. SIGNATURE OF INSPECTOR N. Boston			
9. TOTAL DEPTH OF HOLE 71.4							

ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g
			OVERBURDEN			
267.5			Top of Rock			Begin Coring
267.1	20	WEA, BROKEN	Unit 13	100		0.0 CFM @ 9 PSI
		Shale, SDY HD to MOD HD		100	1	
	30	IT				0.0 CFM @ 23 PSI
			UNIT 14	100	2	
	40		Shale, SDY HD to MOD HD	100		0.0 CFM @ 30 PSI
			UNIT 15		3	
	50		Shale, SDY HD to MOD HD	100		0.0 CFM @ 30 PSI
	60		UNIT 16	100	4	0.0 CFM @ 30 PSI

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
(TRANSLUCENT)

PROJECT

HOLE NO

33

040

DRILLING LOG			DIVISION	INSTALLATION		Hole No. 33	
			Southwestern	Little Rock District		SHEET 2 OF 2 SHEETS	
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOV- ERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g	
214.8	70		Shale MOD HD to HD Unit 16 (cont)				
	80					Bottom of Hole 71.4'	
			NOTE: FOR DETAILED DESCRIPTION OF UNITS - SEE GENERALIZED GEOLOGIC COLUMN				

ENG FORM 18 36 MAR 71 PREVIOUS EDITIONS ARE OBSOLETE

(TRANSLUCENT)

PROJECT

HOLE NO 33

041

Hole No. 40

DRILLING LOG		DIVISION SOUTHWESTERN		INSTALLATION LITTLE ROCK DISTRICT		SHEET 1 OF 2 SHEETS	
1. PROJECT conway water supply				10. SIZE AND TYPE OF BIT NXL			
2. LOCATION (Coordinates or Station) N 3+85 E 10+80				11. DATUM FOR ELEVATION SHOWN (TBM or MSL) MSL			
3. DRILLING AGENCY U. S. CORPS OF ENGINEERS				12. MANUFACTURER'S DESIGNATION OF DRILL FAILING 1500			
4. HOLE NO. (As shown on drawing title and file number) 40				13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN 3		DISTURBED UNDISTURBED -	
5. NAME OF DRILLER NASH				14. TOTAL NUMBER CORE BOXES 6			
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG. FROM VERT.				15. ELEVATION GROUND WATER 284.1			
7. THICKNESS OF OVERBURDEN 5.0				16. DATE HOLE STARTED 5/17/78 COMPLETED 5/19/78			
8. DEPTH DRILLED INTO ROCK 86.9				17. ELEVATION TOP OF HOLE 305.8			
9. TOTAL DEPTH OF HOLE 91.9				18. TOTAL CORE RECOVERY FOR BORING 99 %			
				19. SIGNATURE OF INSPECTOR R. PERRY			
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g	
300.8			O.B. TOP OF ROCK			BEGIN CORING	
293.4 FIRM ROCK	10	C.L. WEA BROKEN SOFT Fe STAINS	UNIT 12 SHALE, SDY HD TO MOD HD	80 100 100	1	1.0 CFM @ 10 PSI	
	20	SOFT				LOST WATER W.T. ▽ 5-19-78	
	30	JT, Fe SOFT, Fe JT, Fe	UNIT 13 SHALE, SDY HD TO MOD HD	100	2	0.0 CFM @ 19 PSI	
	40	JTS		100		0.0 CFM @ 29 PSI	
	50		UNIT 14 SHALE, SDY HD TO MOD HD	100	3	0.0 CFM @ 30 PSI	
	60		UNIT 15 SHALE, SDY HD TO MOD HD	100	4	0.0 CFM @ 30 PSI	
				100			

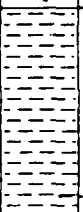
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PROJECT

HOLE NO  
CWS 40

042

Hole No. 40

DRILLING LOG		DIVISION		INSTALLATION		SHEET	
		SOUTHWESTERN		LITTLE ROCK DISTRICT		2	
						OF 2 SHEETS	
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g	
213.9	70	 SILTST	UNIT 16 SHALE MOD HD TO HD			0.0 CFM @ 30 PSI	
				98	5	0.0 CFM @ 30 PSI	
	80			100	6	0.0 CFM @ 30 PSI	
	90					0.0 CFM @ 30 PSI	
						BOTTOM OF HOLE 91.9'	
			NOTE: FOR DETAILED DESCRIPTION OF UNITS SEE GENERALIZED GEOLOGIC COLUMN				

043



Hole No. 41

DRILLING LOG		DIVISION SOUTHWESTERN		INSTALLATION LITTLE ROCK DISTRICT		SHEET 1 OF 2 SHEETS	
1. PROJECT CONWAY WATER SUPPLY				10. SIZE AND TYPE OF BIT NXL			
2. LOCATION (Coordinates or Station) S 1+40 E 11+35				11. DATUM FOR ELEVATION SHOWN (TBM or MSL) MSL			
3. DRILLING AGENCY U.S. Corps of Engineers				12. MANUFACTURER'S DESIGNATION OF DRILL FAILING 1500			
4. HOLE NO. (As shown on drawing title and title number) 41				13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN		DISTURBED 3 UNDISTURBED -	
5. NAME OF DRILLER NASH				14. TOTAL NUMBER CORE BOXES 5		15. ELEVATION GROUND WATER -	
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG. FROM VERT.				16. DATE HOLE STARTED 5/23/78 COMPLETED 5/25/78			
7. THICKNESS OF OVERBURDEN 5.0				17. ELEVATION TOP OF HOLE 296.1			
8. DEPTH DRILLED INTO ROCK 76.2				18. TOTAL CORE RECOVERY FOR BORING 99			
9. TOTAL DEPTH OF HOLE 81.2				19. SIGNATURE OF INSPECTOR R. PERRY			

ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g
291.1			O.B.			
290.4			TOP OF ROCK			BEGIN CORING
	10	C.L. SL WEA Fe STAINS	UNIT 12 SHALE, SDY HD TO MOD HD	89 100 89	1	
	20	C.L. JT. Fe "		100		0.0 CFM @ 8 PSI
	30			100	2	0.0 CFM @ 13 PSI
	40		UNIT 13 SHALE, SDY HD TO MOD HD	100		0.0 CFM @ 27 PSI
	50	JT		100	3	0.0 CFM @ 30 PSI
	60	VERT JTS	UNIT 14 SHALE, SDY HD TO MOD HD	100		0.3 CFM @ 30 PSI
				100	4	0.0 CFM @ 30 PSI

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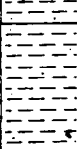
PROJECT

HOLE NO

41

044

Hole No. 41

DRILLING LOG		DIVISION SOUTHWESTERN		INSTALLATION LITTLE ROCK DISTRICT		SHEET 2 OF 2 SHEETS	
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g	
214.9	70	 FRAC	UNIT 15 SHALE, SDY HD TO MOD HD		5	0.0 CFM @ 30 PSI	
	80		UNIT 16 SHALE MOD HD TO HD	100			
			NOTE: FOR DETAILED DESCRIPTION OF UNITS - SEE GENERALIZED GEOLOGIC COLUMN			BOTTOM OF HOLE 81.2'	

045

Hole No. 42

DRILLING LOG		DIVISION SOUTHWESTERN		INSTALLATION LITTLE ROCK DISTRICT		SHEET OF 1 SHEETS	
1. PROJECT CONWAY WATER SUPPLY				10. SIZE AND TYPE OF BIT NXL			
2. LOCATION (Coordinates or Station) S 1+40 E 11+15				11. DATUM FOR ELEVATION SHOWN (TBM or MSL) MSL			
3. DRILLING AGENCY U. S. Corps of Engineers				12. MANUFACTURER'S DESIGNATION OF DRILL FAILING 1500			
4. HOLE NO. (As shown on drawing title and file number) 42				13. TOTAL NO. OF OVER- BURDEN SAMPLES TAKEN: <span style="float:right">DISTURBED UNDISTURBED</span> 1 <span style="float:right">-</span>			
5. NAME OF DRILLER NASH				14. TOTAL NUMBER CORE BOXES 3			
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG FROM VERT				15. ELEVATION GROUND WATER -			
7. THICKNESS OF OVERBURDEN 4.6				16. DATE HOLE <span style="float:right">STARTED COMPLETED</span> 5/30/78 5/31/78			
8. DEPTH DRILLED INTO ROCK 45.1				17. ELEVATION TOP OF HOLE 305.3			
9. TOTAL DEPTH OF HOLE 49.7				18. TOTAL CORE RECOVERY FOR BORING 96 %			
				19. SIGNATURE OF INSPECTOR E. MARTIN			
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	1. CORE RECOV- ERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g	
302.3			O.B. TOP OF ROCK			BEGIN CORING	
300.7							
295.5	10	C.L. -WEA C.L. -Fe STAINS	UNIT 12 SHALE, SDY HD TO MOD HD	28 100 92	1	0.0 CFM @ 7 PSI	
FIRM ROCK	20	-Fe		100	2	0.0 CFM @ 17 PSI	
	30					0.4 CFM @ 27 PSI	
	40		UNIT 13 SHALE, SDY HD TO MOD HD	100	3	0.0 CFM @ 30 PSI	
255.6	50					BOTTOM OF HOLE 49.7'	
	60						
NOTE FOR DETAILED DESCRIPTION OF UNITS, SEE GENERAL GEOLOGIC COLUMN							

046

Hole No. 43

DRILLING LOG		DIVISION SOUTHWESTERN		INSTALLATION LITTLE ROCK DISTRICT		SHEET 1 OF 1 SHEETS	
1. PROJECT CONWAY WATER SUPPLY				10. SIZE AND TYPE OF BIT NYL			
2. LOCATION (Coordinates or Station) S 2+12 E 11+52				11. DATUM FOR ELEVATION SHOWN (TBM or MSL) MSL			
3. DRILLING AGENCY U. S. Corps of Engineers				12. MANUFACTURER'S DESIGNATION OF DRILL FAILING 1500			
4. HOLE NO. (As shown on drawing title and title number) 43				13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN		DISTURBED 7 UNDISTURBED -	
5. NAME OF DRILLER NASH				14. TOTAL NUMBER CORE BOXES 2		15. ELEVATION GROUND WATER -	
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG. FROM VERT.				16. DATE HOLE STARTED 6/1/78 COMPLETED 6/1/78			
7. THICKNESS OF OVERBURDEN 10.4				17. ELEVATION TOP OF HOLE 287.6			
8. DEPTH DRILLED INTO ROCK 27.1				18. TOTAL CORE RECOVERY FOR BORING 99 %			
9. TOTAL DEPTH OF HOLE 37.5				19. SIGNATURE OF INSPECTOR E. MARTIN			
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g	
277.2	10		O.B.  TOP OF ROCK			BEGIN CORING	
270.6	20	WEA Fe STAINS	UNIT 12 SHALES, SDY BD TO MOD BD	100 98 100 100	1	0.0 CFM @ 6 PSI	
250.1	30			98	2	0.0 CFM @ 16 PSI	
	40			100		BOTTOM OF HOLE 37.5'	
	50		NOTE FOR DETAILED DESCRIPTION OF UNITS, SEE GENERALIZED GEOLOGIC COLUMN				
	60						

047

Hole No. 45

DRILLING LOG		DIVISION SOUTHWESTERN		INSTALLATION LITTLE ROCK DISTRICT		SHEET 1 OF 1 SHEETS	
1. PROJECT CONWAY WATER SUPPLY				10. SIZE AND TYPE OF BIT NXL			
2. LOCATION (Coordinates or Station) S 2+12 E 11+33				11. DATUM FOR ELEVATION SHOWN (TBM or MSL) MSL			
3. DRILLING AGENCY U. S. Corps of Engineers				12. MANUFACTURER'S DESIGNATION OF DRILL FAILING 1500			
4. HOLE NO. (As shown on drawing title and file number) 45				13. TOTAL NO. OF OVERBURDEN SAMPLES TAKEN		DISTURBED 2 UNDISTURBED -	
5. NAME OF DRILLER NASH				14. TOTAL NUMBER CORE BOXES 3		15. ELEVATION GROUND WATER --	
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG FROM VERT.				16. DATE HOLE STARTED 6/5/78 COMPLETED 6/6/78			
7. THICKNESS OF OVERBURDEN 5.2				17. ELEVATION TOP OF HOLE 296.8			
8. DEPTH DRILLED INTO ROCK 36.5				18. TOTAL CORE RECOVERY FOR BORING 94 %			
9. TOTAL DEPTH OF HOLE 41.7				19. SIGNATURE OF INSPECTOR E. MARTIN			
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g	
291.6			O.B.				
288.4			TOP OF ROCK			BEGIN CORING	
FIRM ROCK	10	C.L. BADLY WEA	UNIT 12	25 (O)			
		SL WEA		85 (O)			
		C.L.	SHALE, SDY	100 (O)			
		Fe STAINS	HD TO MOD HD	97 (69)	1	0.0 CFM @ 8 PSI	
	20	JT. OPEN					
		VERT JT					
	30	VERT JT		100 (81)	2	0.9 CFM @ 18 PSI	
		BROKEN JT					
255.1	40			100	3	LOST WATER 2.4 CFM @ 24 PSI 75% WATER	
						BOTTOM OF HOLE 41.7'	
	50						
	60						
NOTE: FOR DETAILED DESCRIPTION OF UNITS - SEE GENERALIZED GEOLOGIC COLUMN							

048

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PROJECT

HOLE NO 45

TRANSLUCENT

Hole No. 46

DRILLING LOG		DIVISION SOUTHWESTERN		INSTALLATION LITTLE ROCK DISTRICT		SHEET 1 OF 2 SHEETS	
1. PROJECT CONWAY WATER SUPPLY				10. SIZE AND TYPE OF BIT NXL			
2. LOCATION (Coordinates or Station) N 7+35 E 10+95				11. DATUM FOR ELEVATION SHOWN (TBM or MSL) MSL			
3. DRILLING AGENCY U. S. Corps of Engineers				12. MANUFACTURER'S DESIGNATION OF DRILL FAILING 1500			
4. HOLE NO. (As shown on drawing title and file number) 46				13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN		DISTURBED 2 UNDISTURBED -	
5. NAME OF DRILLER NASH				14. TOTAL NUMBER CORE BOXES 7		15. ELEVATION GROUND WATER 288.6	
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG. FROM VERT.				16. DATE HOLE STARTED 6/7/78 COMPLETED 6/12/78			
7. THICKNESS OF OVERBURDEN 4.0				17. ELEVATION TOP OF HOLE 317.5			
8. DEPTH DRILLED INTO ROCK 104.8				18. TOTAL CORE RECOVERY FOR BORING 99 %			
9. TOTAL DEPTH OF HOLE 108.8				19. SIGNATURE OF INSPECTOR E. MARTIN			

ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g
313.5			O.B. TOP OF ROCK			BEGIN CORING
312.5						
307.8	10	C.L. BADLY WEA, C.L. WEA	UNIT 12	47 (0)		
FIRM ROCK			SHALE, SDY HD TO MOD HD	90 (0)		
				100 (30)	1	1.2 CFM @ 7 PSI
	20	Fe STAINS		100 (71)		
				100		0.0 CFM @ 18 PSI
	30	Fe, SOFT		(86)	2	W.T. ▽
		Fe "				6/9/78
	40	"		100		0.0 CFM @ 28 PSI
		IT				
	50	ITS	UNIT 13	100	3	0.0 CFM @ 30 PSI
		IT, CALCITE	SHALE, SDY HD TO MOD HD			
	60			100	4	0.0 CFM @ 30 PSI
		IT, CALCITE	UNIT 14			
			SHALE, SDY HD TO MOD HD	100		0.3 CFM @ 30 PSI

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PROJECT

HOLE NO

46

049

Hole No. 46


DRILLING LOG		DIVISION		INSTALLATION		SHEET 2 OF 2 SHEETS	
		SOUTHWESTERN		LITTLE ROCK DISTRICT			
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g	
	70	JT	UNIT 14 (Contd) SHALE, SDY HD TO MOD HD		5		
				100		0.6 CFM @ 30 PSI	
	80	C.L.	UNIT 15 SHALE, SDY HD TO MOD HD			25% WATER	
				100		2.1 CFM @ 30 PSI	
	90	JTS	UNIT 16 SHALE MOD HD TO HD		6		
				100		75% WATER	
	100	SILTSTS			7	0.0 CFM @ 30 PSI	
208.7				100			
						BOTTOM OF HOLE 108.8'	
			NOTE: FOR DETAILED DESCRIPTION OF UNITS - SEE GENERALIZED GEOLOGIC COLUMN				

050

Hole No. 47

DRILLING LOG		DIVISION SOUTHWESTERN		INSTALLATION LITTLE ROCK DISTRICT		SHEET OF 1 SHEETS	
1. PROJECT CONWAY WATER SUPPLY				10. SIZE AND TYPE OF BIT NXI			
2. LOCATION (Coordinates or Station) N 7+32 E 77+15				11. DATUM FOR ELEVATION SHOWN (TBM or MSL) MSL			
3. DRILLING AGENCY U. S. Corps of Engineers				12. MANUFACTURER'S DESIGNATION OF DRILL FAILING 1500			
4. HOLE NO. (As shown on drawing title and file number) 47				13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN		DISTURBED 2 UNDISTURBED -	
5. NAME OF DRILLER NASH				14. TOTAL NUMBER CORE BOXES 3		15. ELEVATION GROUND WATER 290.7	
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG FROM VERT.				16. DATE HOLE		STARTED 6/13/78 COMPLETED 6/14/78	
7. THICKNESS OF OVERBURDEN 4.5				17. ELEVATION TOP OF HOLE 308.4		18. TOTAL CORE RECOVERY FOR BORING 99 %	
8. DEPTH DRILLED INTO ROCK 42.0				19. SIGNATURE OF INSPECTOR E. MARTIN			
9. TOTAL DEPTH OF HOLE 46.5							

ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g
304.4			0.B. TOP OF ROCK			BEGIN CORING
303.7						
299.8						
FIRM ROCK	10	C.L. Fe STAINS C.L. Fe STAINS FRAC FRAC Fe Fe Fe	UNIT 12 SHALE, SDY HD TO MOD HD	36 (0) 93 (69) 100 (60) 100	1	1.2 CFM @ 6 PSI  W.T.  6-14-78
	20				2	0.0 CFM @ 16 PSI
	30					
	40		UNIT 13 SHALE, SDY HD TO MOD HD	100 100	3	0.3 CFM @ 26 PSI
261.9						
	50					BOTTOM OF HOLE 46.5
NOTE FOR DETAILED DESCRIPTION OF UNITS, SEE GENERALIZED GEOLOGIC COLUMN						

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MAR 71

(TRANSLUCENT)

PROJECT

HOLE NO

47

051



Hole No. 48

DRILLING LOG		DIVISION		INSTALLATION		SHEET	
		SOUTHWESTERN		LITTLE ROCK DISTRICT		OF 1 SHEETS	
1. PROJECT CONWAY WATER SUPPLY				10. SIZE AND TYPE OF BIT NXI			
2. LOCATION (Coordinates or Station) N 3+85 E 10+60				11. DATUM FOR ELEVATION SHOWN (TBM or MSL) MSL			
3. DRILLING AGENCY U. S. Corps of Engineers				12. MANUFACTURER'S DESIGNATION OF DRILL FAILING 1500			
4. HOLE NO. (As shown on drawing title and file number) 48				13. TOTAL NO. OF OVER- BURDEN SAMPLES TAKEN: DISTURBED 2 UNDISTURBED -			
5. NAME OF DRILLER NASH				14. TOTAL NUMBER CORE BOXES 3			
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG. FROM VERT.				15. ELEVATION GROUND WATER 285.6			
7. THICKNESS OF OVERBURDEN 5.9				16. DATE HOLE: STARTED 6/14/78 COMPLETED 6/16/78			
8. DEPTH DRILLED INTO ROCK 44.7				17. ELEVATION TOP OF HOLE 313.0			
9. TOTAL DEPTH OF HOLE 50.6				18. TOTAL CORE RECOVERY FOR BORING 94 %			
				19. SIGNATURE OF INSPECTOR E. MARTIN			
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOV- ERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g	
307.1			O.B.				
306.7			TOP OF ROCK	91		BEGIN CORING	
305.7	10	C.L. WEA SL WEA	UNIT 12 SHALE, SDY HD TO MOD HD	(0) 90 (21)	1	0.7 CFM @ 7 PSI	
FIRM ROCK	20	C.L. WEA SL WEA		54 (0)		2.0 CFM @ 17 PSI	
	30		UNIT 13 SHALE, SDY HD TO MOD HD	97 (52)	2	LOST WATER	
	40			100 (91)		W.T. ▽ 6-16-78	
	50			100 (100)	3	2.3 CFM @ 25 PSI	
262.4						0.0 CFM @ 30 PSI	
				BOTTOM OF HOLE 50.6'			
NOTE: FOR DETAILED DESCRIPTION OF UNITS - SEE GENERALIZED GEOLOGIC COLUMN							

052

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(TRANSLUCENT)

PROJECT

HOLE NO.

48

Hole No. 49

DRILLING LOG		DIVISION SOUTHWESTERN		INSTALLATION LITTLE ROCK DISTRICT		SHEET OF 1 SHEETS	
1. PROJECT CONWAY WATER SUPPLY				10. SIZE AND TYPE OF BIT NXL			
2. LOCATION (Coordinates or Station) N 1+25 E 11+55				11. DATUM FOR ELEVATION SHOWN (TBM or MSL) MSL			
3. DRILLING AGENCY U. S. CORPS OF ENGINEERS				12. MANUFACTURER'S DESIGNATION OF DRILL FALLING 1500			
4. HOLE NO (As shown on drawing title and file number) 49				13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN 2		DISTURBED UNDISTURBED -	
5. NAME OF DRILLER NASH				14. TOTAL NUMBER CORE BOXES 2			
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG. FROM VERT.				15. ELEVATION GROUND WATER 280.8			
7. THICKNESS OF OVERBURDEN 5.0				16. DATE HOLE STARTED 6-21-78 COMPLETED 6-22-78			
8. DEPTH DRILLED INTO ROCK 26.7				17. ELEVATION TOP OF HOLE 294.8			
9. TOTAL DEPTH OF HOLE 31.7				18. TOTAL CORE RECOVERY FOR BORING 90 %			
				19. SIGNATURE OF INSPECTOR E. MARTIN			
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g	
289.8			O.B.				
289.3			TOP OF ROCK			BEGIN CORING	
287.3			UNIT 12	100			
		WEA		100			
	10	SL WEA	SHALE, SDY HD TO MOD HD	91	1	5% WATER	
		Fe STAINS C.L.		56		W.T. ▽	
				100		6-22-75	
	20	C.L.		67		FREE FLOW @ 0.0 PSI	
				86		25% WATER	
			UNIT 13	100		50% WATER	
			SHALE, SDY HD TO MOD HD	100	2	0.0 CFM @ 29 PSI	
263.1	30					BOTTOM OF HOLE 31.7'	
NOTE: FOR DETAILED DESCRIPTION OF UNITS - SEE GENERALIZED GEOLOGIC COLUMN							

053

Hole No. 50

DRILLING LOG		DIVISION SOUTHWESTERN		INSTALLATION LITTLE ROCK DISTRICT		SHEET 1 OF 1 SHEETS	
1. PROJECT CONWAY WATER SUPPLY				10. SIZE AND TYPE OF BIT 4" x 5-1/2"			
2. LOCATION (Coordinates or Station) N 3+65 E 10+82				11. DATUM FOR ELEVATION SHOWN (TBM or MSL) MSL			
3. DRILLING AGENCY U. S. CORPS OF ENGINEERS				12. MANUFACTURER'S DESIGNATION OF DRILL FAILING 1500			
4. HOLE NO. (As shown on drawing title and file number) 50				13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN DISTURBED - UNDISTURBED -			
5. NAME OF DRILLER NASH				14. TOTAL NUMBER CORE BOXES 15			
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG. FROM VERT.				15. ELEVATION GROUND WATER 281.1			
7. THICKNESS OF OVERBURDEN 6.0				16. DATE HOLE STARTED 6-26-78 COMPLETED 6-29-78			
8. DEPTH DRILLED INTO ROCK 47.3				17. ELEVATION TOP OF HOLE 306.4			
9. TOTAL DEPTH OF HOLE 53.3				18. TOTAL CORE RECOVERY FOR BORING 93 %			
				19. SIGNATURE OF INSPECTOR E. MARTIN			
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOV- ERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g	
300.4			OVERBURDEN				
			TOP OF ROCK			BEGIN CORING	
	10	C.L. WEA C.L. SL WEA Fe STAINS JT JTS JT	UNIT 12 SHALE, SDY HD TO MOD HD	53	1	50% WATER	
291.4				90	2		
FIRM ROCK	20			98	3		
				100	4	25% WATER	
				96	5	W.T. ▽	
	30		UNIT 13 SHALE, SDY HD TO MOD HD	100	6	6-29-78 5% WATER	
				100	7		
	40			100	8	NOTE: Specimens of core tested by Southwest Division Laboratory	
				100	9		
				100	10		
				100	11		
				100	12		
	50		UNIT 14 SHALE, SDY HD TO MOD HD	100	13		
253.1				100	14		
				100	15		
	60					BOTTOM OF HOLE 53.3'	
NOTE: FOR DETAILED DESCRIPTION OF UNITS - SEE GENERALIZED GEOLOGIC COLUMN				054			

Hole No. 51

<b>DRILLING LOG</b>		<b>DIVISION</b> SOUTHWESTERN	<b>INSTALLATION</b> LITTLE ROCK DISTRICT	<b>SHEET</b> OF 2 SHEETS
1. PROJECT CONWAY WATER SUPPLY			10. SIZE AND TYPE OF BIT NXI	
2. LOCATION (Coordinates or Station) N 1+70 E 8+70			11. DATUM FOR ELEVATION SHOWN (TBM or MSL) MSL	
3. DRILLING AGENCY U. S. Corps of Engineers			12. MANUFACTURER'S DESIGNATION OF DRILL FAILING 1500	
4. HOLE NO. (As shown on drawing title and file number) 51			13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN DISTURBED 2    UNDISTURBED	
5. NAME OF DRILLER WOOD			14. TOTAL NUMBER CORE BOXES 7	
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG. FROM VERT.			15. ELEVATION GROUND WATER 315.4	
7. THICKNESS OF OVERBURDEN 5.0			16. DATE HOLE STARTED 11/8/78    COMPLETED 11/13/78	
8. DEPTH DRILLED INTO ROCK 105.0			17. ELEVATION TOP OF HOLE 358.5	
9. TOTAL DEPTH OF HOLE 110.0			18. TOTAL CORE RECOVERY FOR BORING 97 %	
			19. SIGNATURE OF INSPECTOR R. PERRY	

ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g
353.5			OVERBURDEN	(RQD)		
353.0			TOP OF ROCK			BEGIN CORING
	10	2 C.L. WEA BROKEN C.L. BROKEN -IT	SANDSTONE, HD UNIT 10 UNIT 11	92 (36) 98 (0) 83 (20) 100	1	
340.2	20		SHALE, SDY MOD HD TO HD			0.0 CFM @ 16 PSI
FIRM ROCK	30	FRAC	UNIT 12	(67)		
	40	VERT FRACS BROKEN C.L. VERT FRACS, BROKEN C.L. VERT FRACS, BROKEN FRACS, BROKEN		100 (40) 62 (0) 98	2 3	2.24 CFM @ 16 PSI LOST WATER RETURN 1.4 CFM @ 30 PSI
	50		SHALE, SLY HD TO MOD HD	(62) 100		W.T. 43.7 11-13-78
	60	-FRAC		(96) 100	4	0.0 CFM @ 30 PSI 0.64 CFM @ 30 PSI


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PROJECT

HOLE NO  
51

055

Hole No. 51

DRILLING LOG		DIVISION		INSTALLATION		SHEET 2 OF 2 SHEETS		
		SOUTHWESTERN		LITTLE ROCK DISTRICT				
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g		
	70		UNIT 12 (Contd)	(96)				
				100				
	80		UNIT 13	(100)	5	0.0 CFM @ 30 PSI		
				100		0.0 CFM @ 30 PSI		
	90		SHALE, SDY HD TO MOD HD	(100)	6			
			FRAC. CALCITE	100		0.0 CFM @ 30 PSI		
	100		UNIT 14	(98)		0.0 CFM @ 30 PSI		
				100	7			
248.5	110			SHALE, SDY HD TO MOD HD	(100)		0.0 CFM @ 30 PSI	
	120			NOTE: FOR DETAILED DESCRIPTION OF UNITS - SEE GENERALIZED GEOLOGIC COLUMN			BOTTOM OF HOLE 110.0'	

056

Hole No. 52

DRILLING LOG		DIVISION SOUTHWESTERN		INSTALLATION LITTLE ROCK DISTRICT		SHEET 1 OF 2 SHEETS	
1. PROJECT CONWAY WATER SUPPLY				10. SIZE AND TYPE OF BIT NXL			
2. LOCATION (Coordinates or Station) N 1+25 E 11+35				11. DATUM FOR ELEVATION SHOWN (TBM or MSL) MSL			
3. DRILLING AGENCY CORPS OF ENGINEERS				12. MANUFACTURER'S DESIGNATION OF DRILL 1500			
4. HOLE NO. (As shown on drawing title and file number) 52				13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN		DISTURBED 2	
5. NAME OF DRILLER NASH				14. TOTAL NUMBER CORE BOXES 7		UNDISTURBED -	
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG. FROM VERT.				15. ELEVATION GROUND WATER 285.1		16. DATE HOLE STARTED 11-8-78 COMPLETED 11-14-78	
7. THICKNESS OF OVERBURDEN 4.0				17. ELEVATION TOP OF HOLE 305.3		18. TOTAL CORE RECOVERY FOR BORING 99	
8. DEPTH DRILLED INTO ROCK 96.8				19. SIGNATURE OF INSPECTOR E. MARTIN			
9. TOTAL DEPTH OF HOLE 100.8							
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g	
301.3			O.B. = BADLY WEA. SHALE TOP OF ROCK	(ROD)		BEGIN CORING	
300.9				100		0.56 CFM @ 2 PSI	
298.3				(0)			
	10	BROKEN CL BROKEN BROKEN Fe STAINS	UNIT 12	97	1		
				(23)			
	20		SHALE, SDY HD TO MOD HD	100		1.12 CFM @ 17 PSI	
				(79)			
	30			(90)	2		
				100			
	40		UNIT 13	(94)		0.0 CFM @ 26 PSI	
			SHALE, SDY HD TO MOD HD	100	3	0.0 CFM @ 30 PSI	
	50			(100)			
			UNIT 14	100		2.34 CFM @ 30 PSI	
	60		SHALE, SDY HD TO MOD HD	(90)	4		
				99			

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PROJECT

HOLE NO.

52

057

Hole No. 52

DRILLING LOG		DIVISION SOUTHWESTERN		INSTALLATION LITTLE ROCK DISTRICT		SHEET 2 OF 2 SHEETS	
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVER- ERY e	BOX OR SAMPLE NO f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g	
228.3	70	FRAC	UNIT 15	(97)	5	2.42 CFM @ 30 PSI	
			SHALE, SDY HD TO MOD HD	100		NO WATER RETURN	
204.5	80	C.L. SOFT	UNIT 16	(100)	6	0.0 CFM @ 30 PSI	
			SHALE, MOD HD TO HD	98		1.38 CFM @ 30 PSI	
	90	SILTSTS		(57)			
				100		0.78 CFM @ 30 PSI	
	100			(59)	7		
						BOTTOM OF HOLE 100.3	
	110						
	120						
			NOTE: FOR DETAILED DESCRIPTION OF UNITS - SEE GENERALIZED GEOLOGIC COLUMN				

058

ENG FORM 1836  
MAR 71

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PROJECT

HOLE NO  
52

Hole No. 53

DRILLING LOG		DIVISION SOUTHWESTERN		INSTALLATION LITTLE ROCK DISTRICT		SHEET OF 2 SHEETS	
1. PROJECT CONWAY WATER SUPPLY				10. SIZE AND TYPE OF BIT NXL			
2. LOCATION (Coordinates or Station) N 1+10 E 12+30				11. DATUM FOR ELEVATION SHOWN (TBM or MSL) MSL			
3. DRILLING AGENCY U. S. Corps of Engineers				12. MANUFACTURER'S DESIGNATION OF DRILL FALLING 1500			
4. HOLE NO. (As shown on drawing title and file number) 53				13. TOTAL NO. OF OVER- BURDEN SAMPLES TAKEN		DISTURBED 6 UNDISTURBED -	
5. NAME OF DRILLER NASH				14. TOTAL NUMBER CORE BOXES 6		15. ELEVATION GROUND WATER 279.5	
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG FROM VERT				16. DATE HOLE STARTED 11/1/78 COMPLETED 11/6/78		17. ELEVATION TOP OF HOLE 282.5	
7. THICKNESS OF OVERBURDEN 17.5				18. TOTAL CORE RECOVERY FOR BORING 99 %		19. SIGNATURE OF INSPECTOR E. MARTIN	
8. DEPTH DRILLED INTO ROCK 73.8							
9. TOTAL DEPTH OF HOLE 91.3							
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOV- ERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g	
			OVERBURDEN	(RQD)		W.L. 11-6-78	
265.0	10						
264.7			TOP OF ROCK			BEGIN CORING	
264.6	20	-CL. -FRAC. -IT	UNIT 13 SHALE, SDY HD TO MOD HD	97 (36) 100	1	0.0 CFM @ 10 PSI	
	30	-ITS, CALCITE		(83)			
	40		UNIT 14 SHALE, SDY HD TO MOD HD	100 (98)	2	0.74 CFM @ 19 PSI	
	50		UNIT 15 SHALE, SDY HD TO MOD HD	(96)		0.48 CFM @ 30 PSI	
	60	-IT -IT -IT SILTST	UNIT 16 SHALE, MOD HD TO HD	100 (93) 100	3	1.46 CFM @ 30 PSI	
					4		

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PROJECT

HOLE NO. 53

059



Hole No. 53

DRILLING LOG		DIVISION		INSTALLATION		SHEET 2 OF 2 SHEETS	
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVER- ERY e	BOX OR SAMPLE NO. f	REMARKS g (Drilling time, water loss, depth of weathering, etc., if significant)	
191.2	70	-FRAC -SILTST -IT	UNIT 16 (contd)	(79)	4	1.54 CFM @ 30 PSI	
		-SILTSTS		100 (85)			
		-BROKEN		100			
	80	-SILTSTS		(72)	5		
		-SILTST		100			
	90	"		(94)	6		
						BOTTOM OF HOLE 91.3'	
	100		NOTE: FOR DETAILED DESCRIPTION OF UNITS - SEE GENERALIZED GEOLOGIC COLUMN				
	110						
	120						

060

Hole No. 54

DIVISION		SOUTHWESTERN		LITTLE ROCK DISTRICT		SHEET 1 OF 2 SHEETS	
1. PROJECT CONWAY WATER SUPPLY				10. SIZE AND TYPE OF BIT NXL			
2. LOCATION (Coordinates or Station) N 1+00 E 12+95				11. DATUM FOR ELEVATION SHOWN (TBM or MSL) MSL			
3. DRILLING AGENCY CORPS OF ENGINEERS				12. MANUFACTURER'S DESIGNATION OF DRILL FAILING 1500			
4. HOLE NO. (As shown on drawing title and file number) 54				13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN 7		DISTURBED 7	
5. NAME OF DRILLER WOOD				14. TOTAL NUMBER CORE BOXES 4		UNDISTURBED -	
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG. FROM VERT				15. ELEVATION GROUND WATER 279.3		16. DATE HOLE STARTED 10-26-78 COMPLETED 10-31-78	
7. THICKNESS OF OVERBURDEN 20.3				17. ELEVATION TOP OF HOLE 285.5			
8. DEPTH DRILLED INTO ROCK 55.9				18. TOTAL CORE RECOVERY FOR BORING 99			
9. TOTAL DEPTH OF HOLE 76.7				19. SIGNATURE OF INSPECTOR E. MARTIN			

ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g
			OVERBURDEN	3		
	10			(RQD)		
264.7	20		TOP OF ROCK			▽W.L. 6.2' 10-30-78
264.3						BEGIN CORING
FIRM ROCK		FRAC	UNIT 13 100			0.86 CFM @ 11 PSI
	30		SHALE, SDY HD TO MOD HD	(67)	1	
		FRAC	UNIT 14			0.90 CFM @ 15 PSI
	40		SHALE, SDY HD TO MOD HD	(32)		
				100		39.9'
	50		UNIT 15	(26)	2	1.5 CFM @ 25 PSI
				100		2.14 CFM @ 25 PSI
227.5	60		SHALE, SDY HD TO MOD HD	(97)		
		COL	UNIT 16		3	
		BROKEN	SHALE, MOD HD TO HD	100		

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PROJECT

AD-A130 646

ARKANSAS RIVER AND TRIBUTARIES ARKANSAS AND OKLAHOMA  
TOAD SUCK FERRY LOCK..(U) ARMY ENGINEER DISTRICT LITTLE  
ROCK ARK R L CRUTCHFIELD JUN 83

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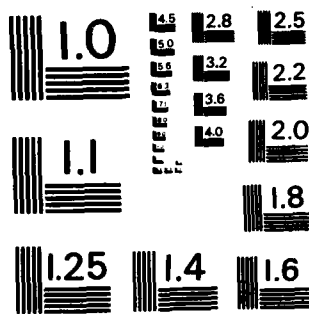
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MICROCOPY RESOLUTION TEST CHART  
NATIONAL BUREAU OF STANDARDS-1963-A

Hole No. 54

DRILLING LOG			DIVISION SOUTHWESTERN	INSTALLATION LITTLE ROCK DISTRICT	SHEET 2 OF 2 SHEETS	
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g
208.9	70	 CLAY " " - SILTST "	UNIT 16 (CONT)	(73)	4	-1.94 CFM @ 30 PSI  25% WATER RETURN  BOTTOM OF HOLE 76.7'
				100		
				(95)		
				100		
				100		

NOTE:  
FOR DETAILED DESCRIPTION  
OF UNITS - SEE GENERALIZED  
GEOLOGIC COLUMN

062

Hole No. 55

DRILLING LOG		DIVISION SOUTHWESTERN		INSTALLATION LITTLE ROCK DISTRICT		SHEET OF 2 SHEETS	
1. PROJECT CONWAY WATER SUPPLY				10. SIZE AND TYPE OF BIT NXL			
2. LOCATION (Coordinates or Station) N 0+60 E 15+35				11. DATUM FOR ELEVATION SHOWN (FSM or MSL) MSL			
3. DRILLING AGENCY CORPS OF ENGINEERS				12. MANUFACTURER'S DESIGNATION OF DRILL FAILING 1500			
4. HOLE NO. (As shown on drawing title and file number) 55				13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN 7		DISTURBED UNDISTURBED	
5. NAME OF DRILLER WOOD				14. TOTAL NUMBER CORE BOXES 4			
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG. FROM VERT.				15. ELEVATION GROUND WATER 279.0			
7. THICKNESS OF OVERBURDEN 21.5				16. DATE HOLE STARTED 10-31-78 COMPLETED 11-2-78			
8. DEPTH DRILLED INTO ROCK 57.7				17. ELEVATION TOP OF HOLE 286.3			
9. TOTAL DEPTH OF HOLE 78.6				18. TOTAL CORE RECOVERY FOR BORING 99			
				19. SIGNATURE OF INSPECTOR R. PERRY			
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g	
			OVERBURDEN	% (RQD)		▽W.L. 7.3'	
264.8	20		TOP OF ROCK			BEGIN BORING	
264.3			UNIT 13	99			
FIRM ROCK			SHALE, SDY HD TO MOD HD	(58)	1	0.9 CFM @ 12 PSI	
				100		0.0 CFM @ 20 PSI	
			UNIT 14	(97)			
			SHALE, SDY HD TO MOD HD	100	2	0.0 CFM @ 28 PSI	
				(100)			
			UNIT 15	100		0.0 CFM @ 30 PSI	
			SHALE, SDY HD TO MOD HD	(100)			
				100	3	0.0 CFM @ 30 PSI	
				(91)			
223.9	60		UNIT 16	100	4		

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PROJECT

HOLE NO.  
55

063

Hole No. 55

DRILLING LOG		DIVISION	INSTALLATION		SHEET 2 OF 2 SHEETS	
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g
207.7	70		UNIT 16 (CONT)			0.84 CFM @ 30 PSI
			SHALE, MOD HD TO HD	100		0.0 CFM @ 30 PSI
	80					BOTTOM OF HOLE 78.6'
	90		NOTE: FOR DETAILED DESCRIPTION OF UNITS - SEE GENERALIZED GEOLOGIC COLUMN			
	100					

064

Hole No. 56

DIVISION <b>DRILLING LOG</b>		SOUTHWESTERN		INSTALLATION <b>LITTLE ROCK DISTRICT</b>		SHEET OF 1 SHEETS	
1. PROJECT <b>Conway Water Supply</b>				10. SIZE AND TYPE OF BIT <b>NXL</b>			
2. LOCATION (Coordinates or Station) <b>N 0+35 E 16+80</b>				11. DAYUM FOR ELEVATION SHOWN (FSM or MSL) <b>MSL</b>			
3. DRILLING AGENCY <b>Corps of Engineers</b>				12. MANUFACTURER'S DESIGNATION OF DRILL <b>Failing 1500</b>			
4. HOLE NO. (As shown on drawing title and file number) <b>56</b>				13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN <b>2</b>		UNDISTURBED <b>-</b>	
5. NAME OF DRILLER <b>WOOD</b>				14. TOTAL NUMBER CORE BOXES <b>3</b>			
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG. FROM VERT.				15. ELEVATION GROUND WATER <b>285.9</b>		16. DATE HOLE <b>3-23-79</b>	
7. THICKNESS OF OVERBURDEN <b>3.0</b>				17. ELEVATION TOP OF HOLE <b>298.6</b>		COMPLETED <b>3-26-79</b>	
8. DEPTH DRILLED INTO ROCK <b>34.2</b>				18. TOTAL CORE RECOVERY FOR BORING <b>98</b>			
9. TOTAL DEPTH OF HOLE <b>37.2</b>				19. SIGNATURE OF INSPECTOR <b>R. PERRY</b>			

ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g
295.6			OB			
294.9			TOP OF ROCK (RQD)	97		BEGIN CORING
		CL	UNIT 12			
		BADLY WEA		(0)		
	10		SHALE, SDY HD TO MOD HD	94	1	
285.0				(26)		W.L. 12.7
FIRM ROCK				100		3-26-79
				(0)		
	20			100		
			UNIT 13	(30)	2	0.0 CFM @ 15 PSI
				100		
	30		SHALE, SDY HD TO MOD HD	(100)		
				100	3	0.0 CFM @ 26 PSI
261.4				(100)		
	40					BOTTOM OF HOLE
						37.2'
	50					
	60					

NOTE:  
FOR DETAILED DESCRIPTION OF UNITS - SEE GENERALIZED GEOLOGIC COLUMN

065

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MAR 71

**PROJECT**

HOLE NO.  
56

**(TRANSLUCENT)**



Hole No. 57

DRILLING LOG		DIVISION		INSTALLATION		SHEET	
1. PROJECT CONWAY WATER SUPPLY		SOUTHWESTERN		LITTLE ROCK DISTRICT		OF 2 SHEETS	
2. LOCATION (Coordinates or Station) N 0+28 E 17+45				10. SIZE AND TYPE OF BIT NXL			
3. DRILLING AGENCY U. S. CORPS OF ENGINEERS				11. DATUM FOR ELEVATION SHOWN (BSM or MSL) MSL			
4. HOLE NO. (As shown on drawing title and file number) 57				12. MANUFACTURER'S DESIGNATION OF DRILL FATLING 1500			
5. NAME OF DRILLER WOOD				13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN		DISTURBED 2	
				14. TOTAL NUMBER CORE BOXES 5		UNDISTURBED -	
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG. FROM VERT.				15. ELEVATION GROUND WATER 278.3			
7. THICKNESS OF OVERBURDEN 2.9				16. DATE HOLE STARTED 3-27-79 COMPLETED 3-28-79			
8. DEPTH DRILLED INTO ROCK 74.1				17. ELEVATION TOP OF HOLE 315.6			
9. TOTAL DEPTH OF HOLE 77.0				18. TOTAL CORE RECOVERY FOR BORING 95 %			
				19. SIGNATURE OF INSPECTOR R. PERRY			

ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g
312.7			O.B. TOP OF WEA SH	% (RQD)		BEGIN CORING
311.1				65 (0)		
304.0	10	BADLY WEA	UNIT 12	69 (0)		
TOP OF ROCK		C.L.		88 (0)	1	
297.3	20	C.L.	SHALE, SDY HD TO MOD HD	100		0.0 CFM @ 17 PSI
FIRM ROCK		FRACS		(21)		
	30			100	2	0.0 CFM @ 27 DSI
				(37)		▽W.L. 37.3' 3-28-79
	40		UNIT 13	100		0.0 CFM @ 30 PSI
			SHALE, SDY HD TO MOD HD	(97)	3	0.0 CFM @ 30 PSI
	50			100		0.0 CFM @ 30 PSI
			UNIT 14	(100)		
	60		SHALE, SDY HD TO MOD HD	100	4	0.0 CFM @ 30 PSI

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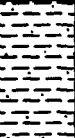
(TRANSLUCENT)

PROJECT

HOLE NO.

57

Hole No. 57

DRILLING LOG			DIVISION	INSTALLATION	SHEET 2 OF 2 SHEETS	
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g
238.5	70		UNIT 14 (cont)		4	0.0 CFM @ 30 PSI
			100	5		
	80		UNIT 15  SHALE, SDY HD TO MOD HD			BOTTOM OF HOLE 77.0
<p>NOTE: FOR DETAILED DESCRIPTION OF UNITS - SEE GENERALIZED GEOLOGIC COLUMN</p>						

067

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PROJECT

HOLE NO.  
57


Hole No. 59

DRILLING LOG		DIVISION		INSTALLATION		SHEET	
		SOUTHWESTERN		LITTLE ROCK DISTRICT		1 OF 2 SHEETS	
1. PROJECT CONWAY WATER SUPPLY				10. SIZE AND TYPE OF BIT NXL & ROCK BIT			
2. LOCATION (Coordinates or Station) N 0+60 E 18+60				11. DAYON FOR ELEVATION SHOWN (FWS or MSL) MSL			
3. DRILLING AGENCY U. S. CORPS OF ENGINEERS				12. MANUFACTURER'S DESIGNATION OF DRILL FAILING 1500			
4. HOLE NO. (As shown on drawing title and file number) 59				13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN		DISTURBED - UNDISTURBED -	
5. NAME OF DRILLER WOOD				14. TOTAL NUMBER CORE BOXES 6		15. ELEVATION GROUND WATER 301.6	
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG. FROM VERT.				16. DATE HOLE STARTED 3-29-79 COMPLETED 4-3-79		17. ELEVATION TOP OF HOLE 338.6	
7. THICKNESS OF OVERBURDEN 1.5				18. TOTAL CORE RECOVERY FOR BORING 95 %		19. SIGNATURE OF INSPECTOR R. PERRY	
8. DEPTH DRILLED INTO ROCK 83.0							
9. TOTAL DEPTH OF HOLE 84.5							

ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g
337.1			O.B. TOP OF ROCK	(ROD)		BEGIN CORING
336.8			SANDSTONE, HD	90 (70)		ROCK BIT
334.5			UNIT 11	82 (0)		
	10	C.L. RES CLAY C.L.		70 (0)	1	
		BADLY WEA C.L.	SHALE, SDY MOD, HD	(0)		
317.2	20	SL WEA		77 (0)		
315.2			UNIT 12	100		0.0 CFM @ 19 PSI
FIRM ROCK	30			(25)	2	
			SHALE, SDY HD TO MOD HD	100 (63)		0.12 CFM @ 27 PSI
	40	C.L.		95 (51)	3	▽ W.L. 37.0' 4-3-79
	50			100 (92)		0.0 CFM @ 30 PSI
			UNIT 13	99		0.0 CFM @ 30 PSI
	60		SHALE, SDY HD TO MOD HD	(19)	4	
		C.L.				

Hole No. 59

DRILLING LOG		DIVISION SOUTHWESTERN		INSTALLATION LITTLE ROCK DISTRICT		SHEET 2 OF 2 SHEETS	
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVER- ERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g	
254.1	70	 VERT FRAC  ST, PYRITE	UNIT 14 (cont)	100 (87)	5	-0.68 CFM @ 30 PSI	
	80		UNIT 15  SHALE, SDY HD TO MOD HD	100 (77)		-0.0 CFM @ 30 PSI	
	90					6	BOTTOM OF HOLE 84.5'
<p>NOTE: FOR DETAILED DESCRIPTION OF UNITS - SEE GENERALIZED GEOLOGIC COLUMN</p>							

069

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PROJECT

HOLE NO.

59

Hole No. 60

DRILLING LOG		DIVISION SOUTHWESTERN		INSTALLATION LITTLE ROCK DISTRICT		SHEET OF 1 SHEETS	
1. PROJECT CONWAY WATER SUPPLY				10. SIZE AND TYPE OF BIT NXL			
2. LOCATION (Coordinate or Station) N 1+00 E 19+00				11. DATUM FOR ELEVATION SHOWN (TBM or MSL) MSL			
3. DRILLING AGENCY U. S. CORPS OF ENGINEERS				12. MANUFACTURER'S DESIGNATION OF DRILL FALLING 1500			
4. HOLE NO. (As shown on drawing title and file number) 60				13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN		DISTURBED 1 UNDISTURBED -	
5. NAME OF DRILLER WOOD				14. TOTAL NUMBER CORE BOXES 3		15. ELEVATION GROUND WATER 342.1	
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG. FROM VERT.				16. DATE HOLE 4-4-79		STARTED COMPLETED 4-5-79	
7. THICKNESS OF OVERBURDEN 4.8				17. ELEVATION TOP OF HOLE 347.5			
8. DEPTH DRILLED INTO ROCK 46.2				18. TOTAL CORE RECOVERY FOR BORING 87 %			
9. TOTAL DEPTH OF HOLE 51.0				19. SIGNATURE OF INSPECTOR S. HARTUNG			
ELEVATION e	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g	
342.7			O.B. TOP OF ROCK	(RQD)		BEGIN CORING	
337.7	10	BADLY WEA CL	UNIT 10 SANDSTONE, HD	50 (0)		▽ W.L. 5.4' 4-5-79	
335.6				80			
		RESID CLAY CL	UNIT 11	(-)	1		
	20	BADLY WEA CL		87 (0)			
				60			
322.6			SHALE, SDY MOD HD TO HD				
FIRM ROCK	30	CL	UNIT 12	(0)			
				94	2	0.0 CFM @ 25 PSI	
	40	CL	SHALE, SDY HD TO MOD HD	(23)			
				99	3	0.75 CFM @ 30 PSI	
296.5	50			(24)			
						BOTTOM OF HOLE 51.0'	
	60						
NOTE: FOR DETAILED DESCRIPTION OF UNITS - SEE GENERALIZED GEOLOGIC COLUMN							

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PROJECT

HOLE NO.

60

070

Hole No. 61

<b>DRILLING LOG</b>		<b>DIVISION</b> SOUTHWESTERN	<b>INSTALLATION</b> LITTLE ROCK DISTRICT	<b>SHEET</b> 1 OF 2 SHEETS
1. PROJECT CONWAY WATER SUPPLY			10. SIZE AND TYPE OF BIT NXL	
2. LOCATION (Coordinates or Station) N 1+50 E 19+50			11. DATUM FOR ELEVATION SHOWN (TBM or MSL) MSL	
3. DRILLING AGENCY U. S. CORPS OF ENGINEERS			12. MANUFACTURER'S DESIGNATION OF DRILL FAILING 1500	
4. HOLE NO. (As shown on drawing title and file number) 61			13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN DISTURBED 2 UNDISTURBED -	
5. NAME OF DRILLER WOOD			14. TOTAL NUMBER CORE BOXES 9	
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG. FROM VERT.			15. ELEVATION GROUND WATER 342.9	
7. THICKNESS OF OVERBURDEN 4.4			16. DATE HOLE STARTED 1-12-79 COMPLETED 1-19-79	
8. DEPTH DRILLED INTO ROCK 137.5			17. ELEVATION TOP OF HOLE 351.5	
9. TOTAL DEPTH OF HOLE 141.9			18. TOTAL CORE RECOVERY FOR BORING 95 %	
			19. SIGNATURE OF INSPECTOR R. PERRY	

ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g
347.1			O.B. TOP OF ROCK	% (RQD)		BEGIN CORING
	10	C.L. BADLY WEA	UNIT 10	61 (0)		
		C.L.	SANDSTONE, HD	59 (30)		W.L. 8.6' 1-16-79
336.3				14	1	
331.8	20	C.L. BADLY WEA	UNIT 11	(7)		
FIRM ROCK			SHALE, SDY HD TO MOD HD	96		0.0 CFM @ 18 PSI
	30	C.L. "		(0)		
			UNIT 12	100	2	0.0 CFM @ 28 PSI
	40			(14)		
				100		0.0 CFM @ 30 PSI
	50		SHALE, SDY HD TO MOD HD	(23)	3	0.0 CFM @ 30 PSI
				100		0.0 CFM @ 30 PSI
	60			(80)		
				100	4	0.0 CFM @ 30 PSI

Hole No. 61

DRILLING LOG			DIVISION	INSTALLATION		SHEET 2 OF 2 SHEETS	
			SOUTHWESTERN	LITTLE ROCK DISTRICT			
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g	
	70		UNIT 13	(65)	4		
			SHALE, SDY HD TO MOD HD	97		0.0 CFM @ 30 PSI	
	80	C.L.		(92)	5		
			UNIT 14	100		1.8 CFM @ 30 PSI	
	90			(100)			
			SHALE, SDY HD TO MOD HD	100	6	0.0 CFM @ 30 PSI	
	100			(100)		0.0 CFM @ 30 PSI	
				100			
	110		UNIT 15	100	7	0.0 CFM @ 30 PSI	
		IT		(100)			
			SHALE, SDY HD TO MOD HD	100		0.0 CFM @ 30 PSI	
	120			(100)	8	0.0 CFM @ 30 PSI	
				100			
222.5	130		UNIT 16	(100)			
			SHALE, MOD HD TO HD	100	9	0.0 CFM @ 30 PSI	
209.6	140	SILTST " "		(99)			
	150		NOTE: FOR DETAILED DESCRIPTION OF UNITS - SEE GENERALIZED GEOLOGIC COLUMN				BOTTOM OF HOLE 141.9'
							072

ENG FORM 1836  
MAR 71

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PROJECT

HOLE NO.  
61

Hole No. 62

DRILLING LOG		DIVISION SOUTHWESTERN		INSTALLATION LITTLE ROCK DISTRICT		SHEET OF 1 SHEETS	
1. PROJECT CONWAY WATER SUPPLY				10. SIZE AND TYPE OF BIT NXL			
2. LOCATION (Coordinates or Station) N 2+00 E 22+00				11. DATUM FOR ELEVATION SHOWN (TBM or MSL) MSL			
3. DRILLING AGENCY U. S. CORPS OF ENGINEERS				12. MANUFACTURER'S DESIGNATION OF DRILL FAILING 1500			
4. HOLE NO. (As shown on drawing title and file number) 62				13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN		DISTURBED 2 UNDISTURBED -	
5. NAME OF DRILLER WOOD				14. TOTAL NUMBER CORE BOXES 2		15. ELEVATION GROUND WATER -	
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG. FROM VERT.				16. DATE HOLE STARTED 4-9-79 COMPLETED 4-10-79		17. ELEVATION TOP OF HOLE 354.14	
7. THICKNESS OF OVERBURDEN 5.5				18. TOTAL CORE RECOVERY FOR BORING 87		19. SIGNATURE OF INSPECTOR R. PERRY	
8. DEPTH DRILLED INTO ROCK 35.5							
9. TOTAL DEPTH OF HOLE 41.0							
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g	
348.6			O.B.	%			
345.9			TOP OF ROCK	(RQD)		BEGIN CORING	
	10	CL	BADLY WEA UNIT 10	63			
		CL	WEA SANDSTONE, HD	(31)			
				90	1		
337.4				(75)			
	20	CL	RESID CLAY UNIT 11	38			
333.8				(0)			
FIRM ROCK			BROKEN	100		0.0 CFM @ 18 PSI	
	30		" SHALE, SDY MOD HD TO HD	(46)			
				100	2	0.0 CFM @ 25 PSI	
	40	JT	UNIT 12	(11)			
			SHALE, SDY HD TO MOD HD				
313.1			BROKEN	100			
				(0)			
						BOTTOM OF HOLE 41.0'	
	50						
	60						
NOTE: FOR DETAILED DESCRIPTION OF UNITS - SEE GENERALIZED GEOLOGIC COLUMN							

073



Hole No. 63

DRILLING LOG		DIVISION SOUTHWESTERN		INSTALLATION LITTLE ROCK DISTRICT		SHEET 1 OF 1 SHEETS	
1. PROJECT CONWAY WATER SUPPLY				10. SIZE AND TYPE OF BIT NXI			
2. LOCATION (Coordinates or Station) N 2+60 E 20+57				11. DATUM FOR ELEVATION SHOWN (TBM or MSL) MSL			
3. DRILLING AGENCY U. S. Corps of Engineers				12. MANUFACTURER'S DESIGNATION OF DRILL FAILING			
4. HOLE NO. (As shown on drawing title and file number) 63				13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN		DISTURBED 2 UNDISTURBED -	
5. NAME OF DRILLER WOOD				14. TOTAL NUMBER CORE BOXES 3		15. ELEVATION GROUND WATER -	
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG. FROM VERT.				16. DATE HOLE STARTED 4/10/79 COMPLETED 4/11/79		17. ELEVATION TOP OF HOLE 356.4	
7. THICKNESS OF OVERBURDEN 5.0				18. TOTAL CORE RECOVERY FOR BORING 92 %		19. SIGNATURE OF INSPECTOR R. PERRY	
8. DEPTH DRILLED INTO ROCK 36.6							
9. TOTAL DEPTH OF HOLE 41.6							

ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g
351.4			OVERBURDEN	%		
348.4			TOP OF ROCK	(RQD)		BEGIN CORING
	10	C.L. BADLY WEA - JT	UNIT 10 SANDSTONE, HD	84 (0)		
340.9		- SL WEA		100 (61)	1	
336.8	20	C.L. "	UNIT 11 SHALE, SDY MOD HD TO HD	58 (9)		
FIRM ROCK		C.L. "		97 (54)		0.0 CFM @ 17 PSI
	30	C.L. "	UNIT 12 SHALE, SDY HD TO MOD HD	98 (36)	2	0.0 CFM @ 22 PSI
314.8	40			100 (35)		0.0 CFM @ 30 PSI
						BOTTOM OF HOLE 41.6'
	50					
	60					

NOTE:  
FOR DETAILED DESCRIPTION  
OF UNITS - SEE GENERALIZED  
GEOLOGIC COLUMN

074

Hole No. 64

DRILLING LOG		DIVISION SOUTHWESTERN		INSTALLATION LITTLE ROCK DISTRICT		SHEET 1 of 1 SHEETS	
1. PROJECT CONWAY WATER SUPPLY				10. SIZE AND TYPE OF BIT NXL			
2. LOCATION (Coordinates or Station) N 3+20 E 21+15				11. DATUM FOR ELEVATION SHOWN (TBM or MSL) MSL			
3. DRILLING AGENCY U. S. Corps of Engineers				12. MANUFACTURER'S DESIGNATION OF DRILL FAILING 1500			
4. HOLE NO. (As shown on drawing title and file number) 64				13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN		DISTURBED 3	
5. NAME OF DRILLER WOOD				14. TOTAL NUMBER CORE BOXES		3	
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG. FROM VERT.				15. ELEVATION GROUND WATER		-	
7. THICKNESS OF OVERBURDEN 4.5				16. DATE HOLE STARTED 4/13/79		COMPLETED 4/13/79	
8. DEPTH DRILLED INTO ROCK 34.3				17. ELEVATION TOP OF HOLE		357.41	
9. TOTAL DEPTH OF HOLE 38.8				18. TOTAL CORE RECOVERY FOR BORING		90 %	
				19. SIGNATURE OF INSPECTOR R. PERRY			
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g	
352.9			OVERBURDEN	%		BEGIN CORING	
			TOP OF ROCK	(RQD)			
	10	WEA BADLY WEA SL WEA	UNIT 10	100 (41)			
343.9		C.L. SL WEA	SANDSTONE, HD	81 (45)	1		
339.3		C.L.	UNIT 11	51 (0)			
FIRM ROCK	20	"	SHALE, SDY MOD HD TO HD	97 (71)		0.0 CFM @ 15 PSI	
	30	C.L.	UNIT 12	94 (69)	2	0.0 CFM @ 23 PSI	
318.6		C.L.	SHALE, SDY HD TO MOD HD	97 (63)	3		
						BOTTOM OF HOLE 38.8'	
NOTE: FOR DETAILED DESCRIPTION OF UNITS - SEE GENERALIZED GEOLOGIC COLUMN							

075

Hole No. 65

DRILLING LOG		DIVISION SOUTHWESTERN		INSTALLATION LITTLE ROCK DISTRICT		SHEET 1 OF 1 SHEETS	
1. PROJECT CONWAY WATER SUPPLY				10. SIZE AND TYPE OF BIT NXL			
2. LOCATION (Coordinates or Station) N 2+52N E 10+85				11. DATUM FOR ELEVATION SHOWN (TBM or MSL) MSL			
3. DRILLING AGENCY U. S. CORPS OF ENGINEERS				12. MANUFACTURER'S DESIGNATION OF DRILL FAILING 1500			
4. HOLE NO. (As shown on drawing title and file number) 65				13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN		DISTURBED - UNDISTURBED -	
5. NAME OF DRILLER WOOD				14. TOTAL NUMBER CORE BOXES 4		15. ELEVATION GROUND WATER 301.2	
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG. FROM VERT.				16. DATE HOLE 11-28-78		STARTED 11-29-78 COMPLETED	
7. THICKNESS OF OVERBURDEN 0.5				17. ELEVATION TOP OF HOLE 318.5			
8. DEPTH DRILLED INTO ROCK 58.6				18. TOTAL CORE RECOVERY FOR BORING 96 %			
9. TOTAL DEPTH OF HOLE 59.1				19. SIGNATURE OF INSPECTOR R. PERRY			
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g	
318.07			O.B.	68		BEGIN CORING	
314.7			UNIT T2	(0)			
TOP/RK 313.3				81			
FIRM ROCK				(14)	1		
	10			100		0.0 CFM @ 10 PSI	
				(29)		W.L. 17.3 ▽	
				100		11/29/78	
	20			(47)	2	0.0 CFM @ 21 PSI	
			SHALE, SDY HD TO MOD HD	100			
	30			(72)			
				100	3	0.18 CFM @ 30 PSI	
	40			(64)			
			UNIT 13	100		1.46 CFM @ 30 PSI	
			SHALE, SDY HD TO MOD HD				
	50			100	4	1.8 CFM @ 30 PSI	
			UNIT 14	(100)			
			SHALE, SDY HD TO MOD 40				
259.4	60					BOTTOM OF HOLE 59.1'	
NOTE: FOR DETAILED DESCRIPTION OF UNITS - SEE GENERALIZED GEOLOGIC COLUMN							

ENG FORM 1836  
MAR 71

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PROJECT

HOLE NO.

65

Hole No. 103

<b>DRILLING LOG</b>		<b>DIVISION</b> SOUTHWESTERN	<b>INSTALLATION</b> LITTLE ROCK DISTRICT	<b>SHEET</b> 1 OF 2 SHEETS
1. PROJECT CONWAY WATER SUPPLY			10. SIZE AND TYPE OF BIT NXL	
2. LOCATION (Coordinates or Station) STA 6+25 ON DIKE CENTERLINE			11. DATUM FOR ELEVATION SHOWN (TBM or MSL) MSL	
3. DRILLING AGENCY U. S. CORPS OF ENGINEERS			12. MANUFACTURER'S DESIGNATION OF DRILL FAILING 1500	
4. HOLE NO. (As shown on drawing title and file number) 103			13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN DISTURBED 3 UNDISTURBED -	
5. NAME OF DRILLER WOOD			14. TOTAL NUMBER CORE BOXES 7	
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG. FROM VERT.			15. ELEVATION GROUND WATER 312.8	
7. THICKNESS OF OVERBURDEN 7.4			16. DATE HOLE STARTED 12-27-77 COMPLETED 12-29-77	
8. DEPTH DRILLED INTO ROCK 93.0			17. ELEVATION TOP OF HOLE 331.7	
9. TOTAL DEPTH OF HOLE 100.4			18. TOTAL CORE RECOVERY FOR BORING 99 %	
			19. SIGNATURE OF INSPECTOR R. PERRY	

ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOV- ERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g
324.2			OVERBURDEN			
			TOP OF ROCK			BEGIN CORING
316.4	10	WEA	UNIT 13	95	1	0.1 CFM @ 9 PSI
		SL WEA C.L.				
	20		SHALE, SDY HD TO MOD HD	98		W.L. ▽ 12-29-77
	30			100	2	0.3 CFM @ 24 PSI
	40	FRAC	UNIT 14			
			SHALE, SDY HD TO MOD HD	100		0.7 CFM @ 30 PSI
	50		UNIT 15		3	
			SHALE, SDY HD TO MOD HD	100		0.0 CFM @ 30 PSI
	60	VERT JT			4	
			UNIT 16	100		40% WATER
						0.0 CFM @ 30 PSI

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PROJECT

HOLE NO.  
103

Hole No. 103

DRILLING LOG		DIVISION	INSTALLATION		SHEET 2 OF 2 SHEETS	
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVER- ERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g
	70		UNIT 16 (Cont)  SHALE MOD HD TO HD	100		REGAINED WATER
	80			100	5	0.0 CFM @ 30 PSI
	90			100		0.0 CFM @ 30 PSI
	100			100	6	0.0 CFM @ 30 PSI
231.3					7	
						BOTTOM OF HOLE 100.4'
			NOTE: FOR DETAILED DESCRIPTION OF UNITS - SEE GENERALIZED GEOLOGIC COLUMN			

078

Hole No. 132

DRILLING LOG		DIVISION		INSTALLATION		SHEET	
		SOUTHWESTERN		LITTLE ROCK DISTRICT		OF 1 SHEETS	
1. PROJECT CONWAY WATER SUPPLY				10. SIZE AND TYPE OF BIT NXL			
2. LOCATION (Coordinates or Station) Sta 20+00 ON DIKE CENTERLINE				11. DATUM FOR ELEVATION SHOWN (TBM or MSL) MSL			
3. DRILLING AGENCY U. S. Corps of Engineers				12. MANUFACTURER'S DESIGNATION OF DRILL FALLING 1500			
4. HOLE NO. (As shown on drawing title and file number) 132				13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN		DISTURBED 9	
5. NAME OF DRILLER NASH				14. TOTAL NUMBER CORE BOXES 1		UNDISTURBED -	
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG. FROM VERT.				15. ELEVATION GROUND WATER 341.8		16. DATE HOLE STARTED 4/27/78 COMPLETED 4/28/78	
7. THICKNESS OF OVERBURDEN 16.0				17. ELEVATION TOP OF HOLE 358.5		18. TOTAL CORE RECOVERY FOR BORING 63	
8. DEPTH DRILLED INTO ROCK 24.3				19. SIGNATURE OF INSPECTOR R. PERRY			
9. TOTAL DEPTH OF HOLE 40.3							
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g	
			OVERBURDEN				
342.5	10					BEGIN CORING	
	20	BADLY WEA		37		W.L. 16.7' <input checked="" type="checkbox"/> 4-28-78	
329.9		C.L.				0.0 CFM @ 8 PSI	
327.9	30	WEA	TOP OF ROCK	70	1		
FIRM ROCK			UNIT 13 SHALE, SDY HD TO MOD HD				
318.2	40			100			
	50					BOTTOM OF HOLE 40.3'	
			NOTE: FOR DETAILED DESCRIPTION OF UNITS - SEE GENERALIZED GEOLOGIC COLUMN				

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MAR 71 (TRANSLUCENT)

PROJECT

HOLE NO. 132

079

Hole No. 134

DRILLING LOG		DIVISION		INSTALLATION		SHEET	
		SOUTHWESTERN		LITTLE ROCK DISTRICT		5 of 1 SHEETS	
1. PROJECT CONWAY WATER SUPPLY				10. SIZE AND TYPE OF BIT (X)			
2. LOCATION (Coordinates or Station) STA 16+00 ON DIKE CENTERLINE				11. DAYUM FOR ELEVATION SHOWN (TBM or MSL) MSL			
3. DRILLING AGENCY U. S. Corps of Engineers				12. MANUFACTURER'S DESIGNATION OF DRILL FAILING 1500			
4. HOLE NO. (As shown on drawing title and file number) 134				13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN		DISTURBED 6 UNDISTURBED 2	
5. NAME OF DRILLER NASH				14. TOTAL NUMBER CORE BOXES 1		15. ELEVATION GROUND WATER -	
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG. FROM VERT.				16. DATE HOLE STARTED 4/14/78 COMPLETED 4/14/78		17. ELEVATION TOP OF HOLE 333.8	
7. THICKNESS OF OVERBURDEN 10.0				18. TOTAL CORE RECOVERY FOR BORING 93		19. SIGNATURE OF INSPECTOR R. PERRY	
8. DEPTH DRILLED INTO ROCK 14.7							
9. TOTAL DEPTH OF HOLE 24.7							
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (D. drilling time, water loss, depth of weathering, etc., if significant) g	
323.8			OVERBURDEN				
322.8	10					BEGIN CORING	
320.3		C.L.	TOP OF ROCK				
FIRM ROCK		WEA	UNIT 13	90	1	0.0 CFM @ 8 PSI	
	20		SHALE, SDY HD TO MOD HD	100			
309.1							
	30					BOTTOM OF HOLE 24.7'	
			NOTE: FOR DETAILED DESCRIPTION OF UNITS - SEE GENERALIZED GEOLOGIC COLUMN				

080

Hole No. 136

DRILLING LOG		DIVISION		INSTALLATION		SHEET	
		SOUTHWESTERN		LITTLE ROCK DISTRICT		1 OF 1 SHEETS	
1. PROJECT CONWAY WATER SUPPLY				10. SIZE AND TYPE OF BIT NXI			
2. LOCATION (Coordinates or Station) Sta 12+00 on DIKE CENTERLINE				11. DATUM FOR ELEVATION SHOWN (FSM or MSL) MSL			
3. DRILLING AGENCY U. S. Corps of Engineers				12. MANUFACTURER'S DESIGNATION C* DRILL FALLING 1500			
4. HOLE NO. (As shown on drawing title and file number) 136				13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN		DISTURBED 4 UNDISTURBED 3	
5. NAME OF DRILLER NASH				14. TOTAL NUMBER CORE BOXES 1		15. ELEVATION GROUND WATER -	
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG. FROM VERT.				16. DATE HOLE STARTED 4/17/78 COMPLETED 4/17/78			
7. THICKNESS OF OVERBURDEN 10.0				17. ELEVATION TOP OF HOLE 340.6			
8. DEPTH DRILLED INTO ROCK 16.5				18. TOTAL CORE RECOVERY FOR BORING 92 %			
9. TOTAL DEPTH OF HOLE 26.5				19. SIGNATURE OF INSPECTOR R. PERRY			
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g	
			OVERBURDEN				
330.6	10					BEGIN CORING	
326.3			CL. BADLY WEA TOP OF ROCK	86			
325.6			SL WEA UNIT 13	(9)			
FIRM ROCK	20		Fe STAINS SHALE, SDY HD TO MOD HD	100	1		
314.1				(82)			
	30					BOTTOM OF HOLE 26.5'	
NOTE: FOR DETAILED DESCRIPTION OF UNITS - SEE GENERALIZED GEOLOGIC COLUMN							

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PROJECT

HOLE NO.  
136

081



Hole No. 138

DRILLING LOG		DIVISION SOUTHWESTERN		INSTALLATION LITTLE ROCK DISTRICT		SHEET OF 1 SHEETS	
1. PROJECT CONWAY WATER SUPPLY				10. SIZE AND TYPE OF BIT NXL			
2. LOCATION (Coordinates or Station) STA 8+00 on DIKE CENTERLINE				11. DATUM FOR ELEVATION SHOWN (TBM or MSL) MSL			
3. DRILLING AGENCY U. S. Corps of Engineers				12. MANUFACTURER'S DESIGNATION OF DRILL FALLING 1500			
4. HOLE NO. (As shown on drawing title and file number) 138				13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN		DISTURBED 7 UNDISTURBED 1	
5. NAME OF DRILLER NASH				14. TOTAL NUMBER CORE BOXES 2		15. ELEVATION GROUND WATER -	
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG. FROM VERT.				16. DATE HOLE STARTED 4/18/78 COMPLETED 4/18/78			
7. THICKNESS OF OVERBURDEN 10.0				17. ELEVATION TOP OF HOLE 344.9			
8. DEPTH DRILLED INTO ROCK 21.7				18. TOTAL CORE RECOVERY FOR BORING 82 %			
9. TOTAL DEPTH OF HOLE 31.7				19. SIGNATURE OF INSPECTOR R. PERRY			
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOV- ERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g	
334.9			OVERBURDEN				
333.9	10		TOP OF ROCK			BEGIN CORING	
325.2	20	WEA C.L. WEA, BROKEN JT	UNIT 13 SHALE, SDY MOD HD TO HD	63 86 100	1 2	0.4 CFM @ 14 PSI	
313.2	30					BOTTOM OF HOLE 31.7'	
	40						
NOTE: FOR DETAILED DESCRIPTION OF UNITS - SEE GENERALIZED GEOLOGIC COLUMN							

082

Hole No. 139

DRILLING LOG		DIVISION SOUTHWESTERN		INSTALLATION LITTLE ROCK DISTRICT		SHEET 1 OF 2 SHEETS	
1. PROJECT CONWAY WATER SUPPLY				10. SIZE AND TYPE OF BIT NXL			
2. LOCATION (Coordinates or Station) STA 6+00 ON DIKE CENTERLINE				11. DATUM FOR ELEVATION SHOWN (TBM or MSL) MSL			
3. DRILLING AGENCY U. S. CORPS OF ENGINEERS				12. MANUFACTURER'S DESIGNATION OF DRILL FALLING 1500			
4. HOLE NO. (As shown on drawing title and file number) 139				13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN		DISTURBED 6 UNDISTURBED 1	
5. NAME OF DRILLER NASH				14. TOTAL NUMBER CORE BOXES 7		15. ELEVATION GROUND WATER 312.0	
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG. FROM VERT.				16. DATE HOLE STARTED 4-19-78 COMPLETED 4-25-78		17. ELEVATION TOP OF HOLE 347.3	
7. THICKNESS OF OVERBURDEN 10.0				18. TOTAL CORE RECOVERY FOR BORING 93 %			
8. DEPTH DRILLED INTO ROCK 106.8				19. SIGNATURE OF INSPECTOR R. PERRY			
9. TOTAL DEPTH OF HOLE 116.8							

ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g
337.3			O.B.			
336.6	10					BEGIN CORING
335.8			TOP OF ROCK	93		
FIRM ROCK		WEA SL WEA Fe STAINS	UNIT 13	(35)	1	0.0 CFM @ 11 PSI
	20		SHALE, SDY HD TO MOD HD	98		0.0 CFM @ 15 PSI
	30			(81)		
	40	C.L. C.L.	UNIT 14	90 (31)	2	FREE FLOW @ 0 PSI NO WATER RETURN W.L. 35.3 4-24-78
	50	FRAC FRACS FRAC C.L.	UNIT 15	81 (56)		
	60		SHALE, SDY HD TO MOD HD	98 (74)	3	2.5 CFM @ 30 PSI
			UNIT 16	87 (8)	4	2.8 CFM @ 30 PSI
						3.1 CFM @ 30 PSI

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PROJECT

HOLE NO.  
139

083

Hole No. 139

DRILLING LOG		DIVISION SOUTHWESTERN		INSTALLATION LITTLE ROCK DISTRICT		SHEET 2 OF 2 SHEETS		
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVER- ERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g		
			UNIT 16 (cont)	98				
	70	C.L. SILTST	SHALE MOD HD TO HD	(8)		0.4 CFM @ 30 PSI		
		..		94				
		C.L.						
	80	SILTST		..	(24)	5	0.0 CFM @ 30 PSI	
		..		..	98			
		C.L.						
	90	SILTST		..	(56)	6	0.0 CFM @ 30 PSI	
		..		..	100			
		..		..	(57)			
	100				100 (0)			
					93		0.0 CFM @ 30 PSI	
		C.L. SILTST			(21)			
	110	..		76	7	0.0 CFM @ 30 PSI		
		2.4' SCATT C.L. SILTST		(0)				
230.5		..						
	120						BOTTOM OF HOLE 116.8'	
			NOTE: FOR DETAILED DESCRIPTION OF UNITS - SEE GENERALIZED GEOLOGIC COLUMN					

084

084

Hole No. 140

DRILLING LOG		DIVISION		INSTALLATION		SHEET	
		SOUTHWESTERN		LITTLE ROCK DISTRICT		OF 1 SHEETS	
1. PROJECT CONWAY WATER SUPPLY				10. SIZE AND TYPE OF BIT NXL			
2. LOCATION (Coordinates or Station) STA 4+00 on DIKE CENTERLINE				11. DATUM FOR ELEVATION SHOWN (TBM or MSL) MSL			
3. DRILLING AGENCY U. S. Corps of Engineers				12. MANUFACTURER'S DESIGNATION OF DRILL FALLING 1500			
4. HOLE NO. (As shown on drawing title and file number) 140				13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN		DISTURBED 6 UNDISTURBED -	
5. NAME OF DRILLER NASH				14. TOTAL NUMBER CORE BOXES 1		15. ELEVATION GROUND WATER -	
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG. FROM VERT.				16. DATE HOLE		STARTED 4/25/78 COMPLETED 4/25/78	
7. THICKNESS OF OVERBURDEN 9.8				17. ELEVATION TOP OF HOLE 349.9		18. TOTAL CORE RECOVERY FOR BORING 98	
8. DEPTH DRILLED INTO ROCK 11.8				19. SIGNATURE OF INSPECTOR R. PERRY			
9. TOTAL DEPTH OF HOLE 21.6							
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g	
			OVERBURDEN				
340.1	10		TOP OF ROCK			BEGIN CORING	
339.7		C.L. Fe STAINS FRACS JTS	UNIT 13 SHALE, SDY HD TO MOD HD	98	1	0.0 CFM @ 5 PSI	
328.3	20			100			
	30		NOTE: FOR DETAILED DESCRIPTION OF UNITS - SEE GENERALIZED GEOLOGIC COLUMN			BOTTOM OF HOLE 21.6'	

085

Hole No. 142

DRILLING LOG		DIVISION SOUTHWESTERN		INSTALLATION LITTLE ROCK DISTRICT		SHEET 1 OF 2 SHEETS	
1. PROJECT CONWAY WATER SUPPLY				10. SIZE AND TYPE OF BIT ROCK BIT, NXL			
2. LOCATION (Coordinates or Station) STA 7+00 ON DIKE CENTERLINE				11. DATUM FOR ELEVATION SHOWN (TBM or MSL) MSL			
3. DRILLING AGENCY U. S. CORPS OF ENGINEERS				12. MANUFACTURER'S DESIGNATION OF DRILL FAILING 1500			
4. HOLE NO. (As shown on drawing title and file number) 142				13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN		DISTURBED 5 UNDISTURBED -	
5. NAME OF DRILLER NASH				14. TOTAL NUMBER CORE BOXES 5		15. ELEVATION GROUND WATER 314.2	
6. DIRECTION OF HOLE <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> INCLINED _____ DEG. FROM VERT.				16. DATE HOLE 5-8-78		STARTED 5-10-78 COMPLETED	
7. THICKNESS OF OVERBURDEN 9.5				17. ELEVATION TOP OF HOLE 345.1			
8. DEPTH DRILLED INTO ROCK 72.1				18. TOTAL CORE RECOVERY FOR BORING 100 %			
9. TOTAL DEPTH OF HOLE 81.6				19. SIGNATURE OF INSPECTOR R. PERRY			
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g	
335.6	10		O.B. TOP OR ROCK			ROCK BIT	
327.6	20	WEA	Fe STAINS	100 (41)	1	BEGIN CORING	
FIRM ROCK			SHALE, SDY HD TO MOD HD	100 (62)		0.0 CFM @ 12 PSI	
326.4	30			100 (62)		W.L. 30.9' ▽ 5-11-78	
	40		UNIT 14 SHALE, SDY HD TO MOD HD	100 (83)	2	0.0 CFM @ 22 PSI	
	50		UNIT 15 SHALE, SDY HD TO MOD HD	100 (81)	3	0.0 CFM @ 30 PSI	
	60	FRAC	UNIT 16 SHALE MOD HD TO HD	100		0.0 CFM @ 30 PSI	
		SOFT				1.4 CFM @ 30 PSI	

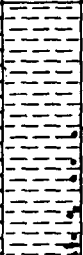
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PROJECT

HOLE NO.

142

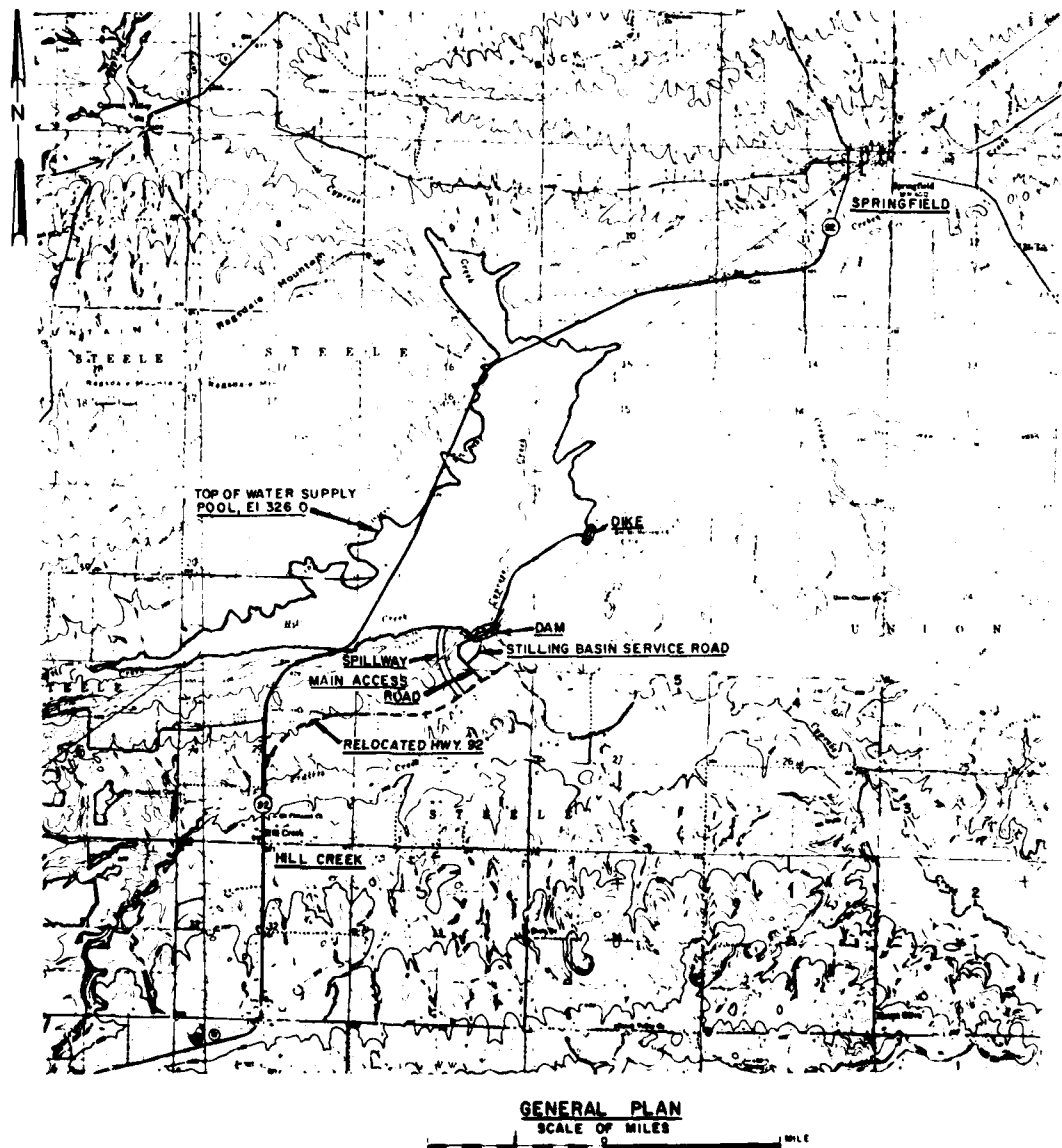
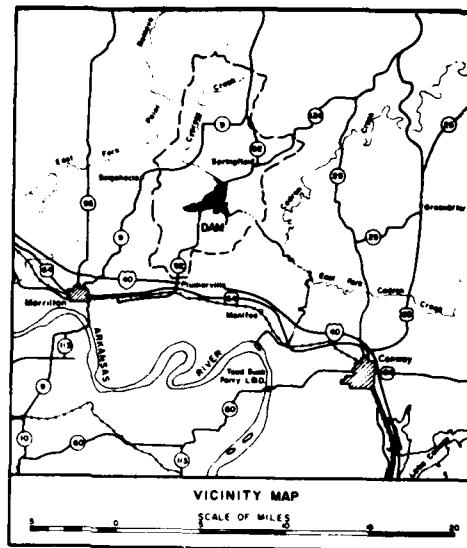
Hole No. 142

DRILLING LOG		DIVISION SOUTHWESTERN		INSTALLATION LITTLE ROCK DISTRICT		SHEET 2 OF 2 SHEETS	
ELEVATION a	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIALS (Description) d	% CORE RECOVERY e	BOX OR SAMPLE NO. f	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant) g	
263.5	70		UNIT 16 (cont)	100	4	75% WATER  1.1 CFM @ 30 PSI	
			SHALE MOD HD TO HD	100			
	80		SILTSTS	(90)	5		
	90		NOTE: FOR DETAILED DESCRIPTION OF UNITS - SEE GENERALIZED GEOLOGIC COLUMN			BOTTOM OF HOLE 81.6'	

087

APPENDIX C

PLATES

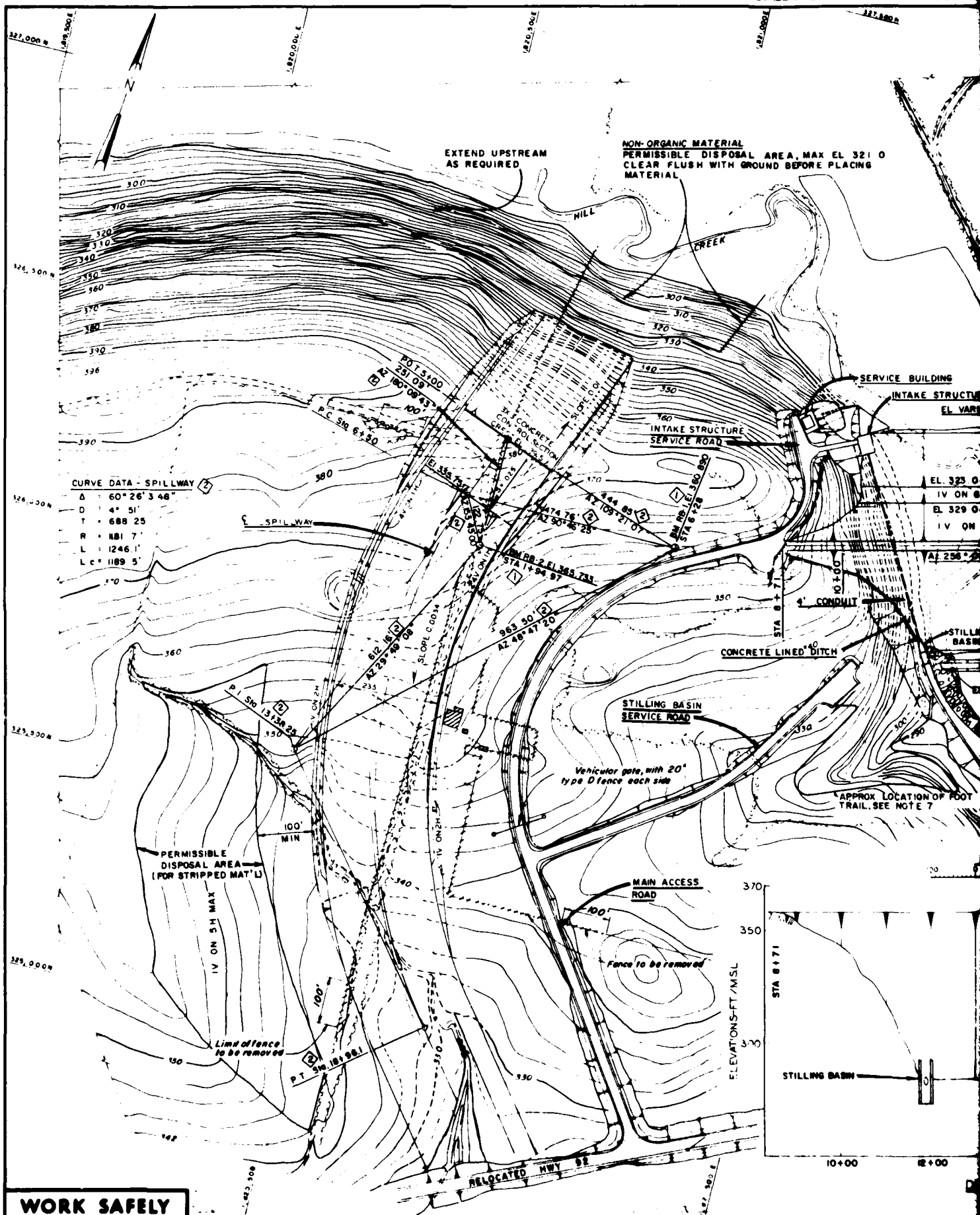


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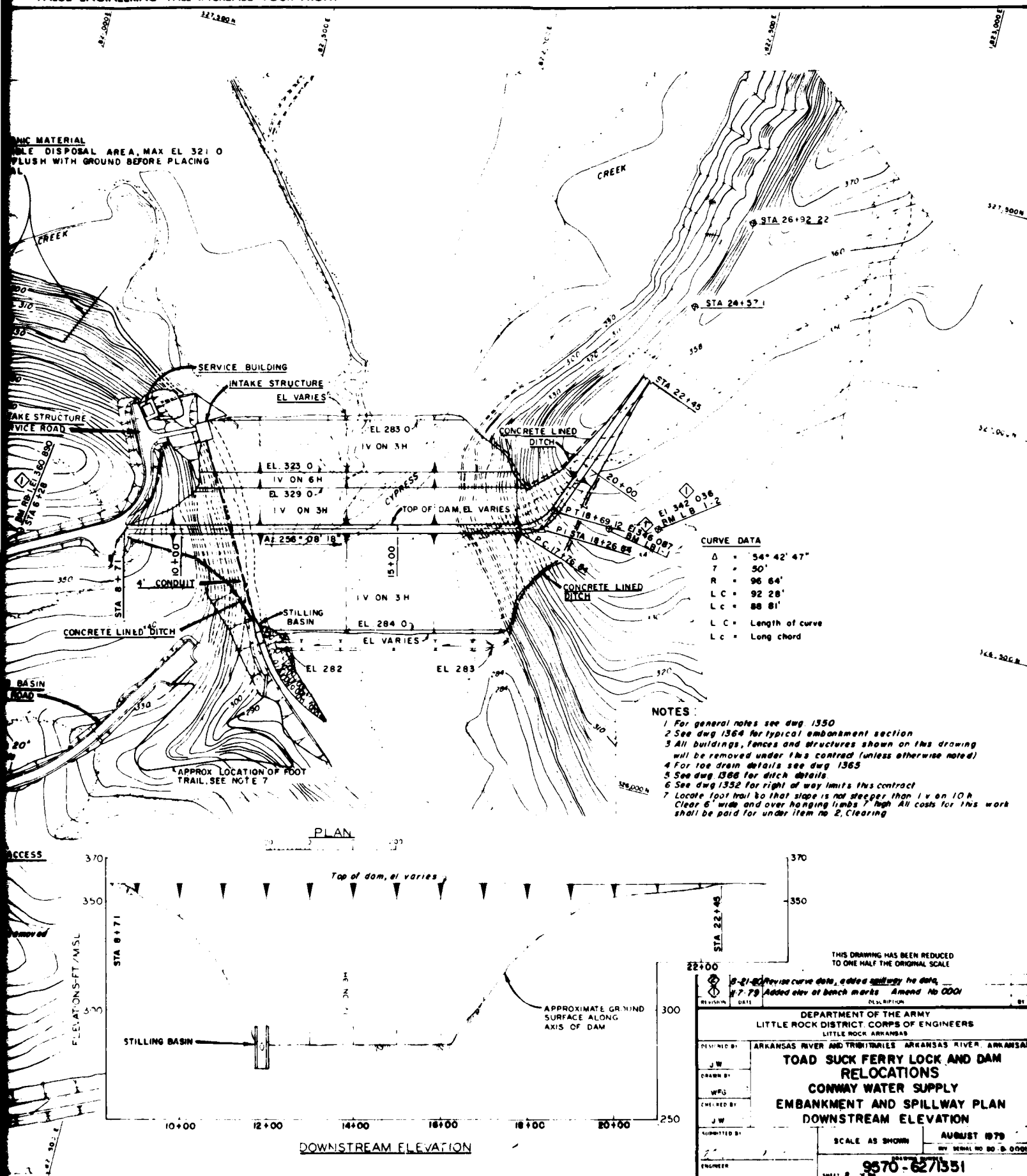


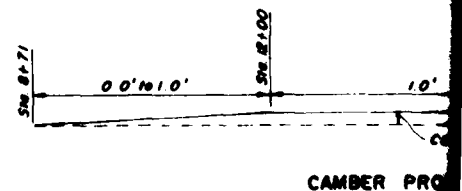
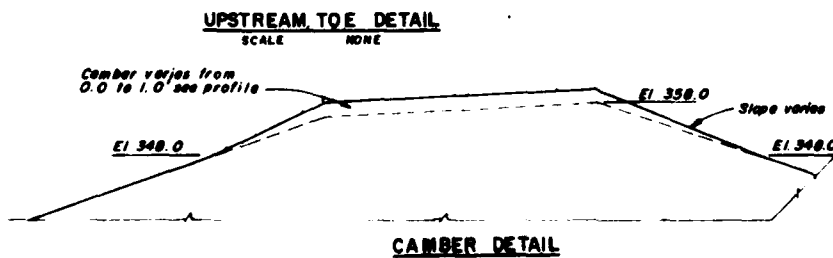
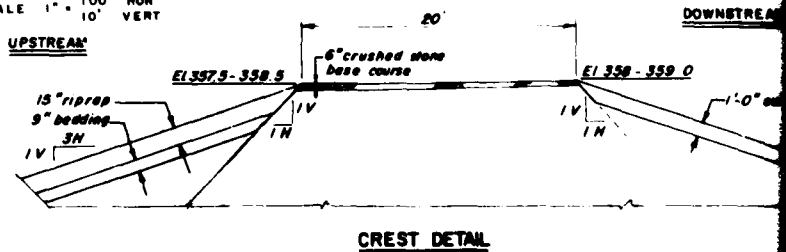
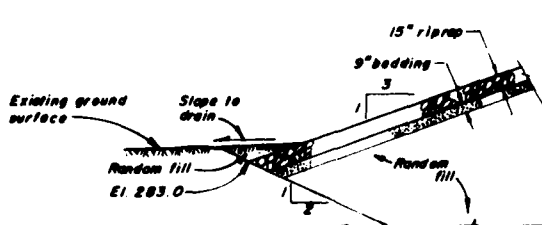
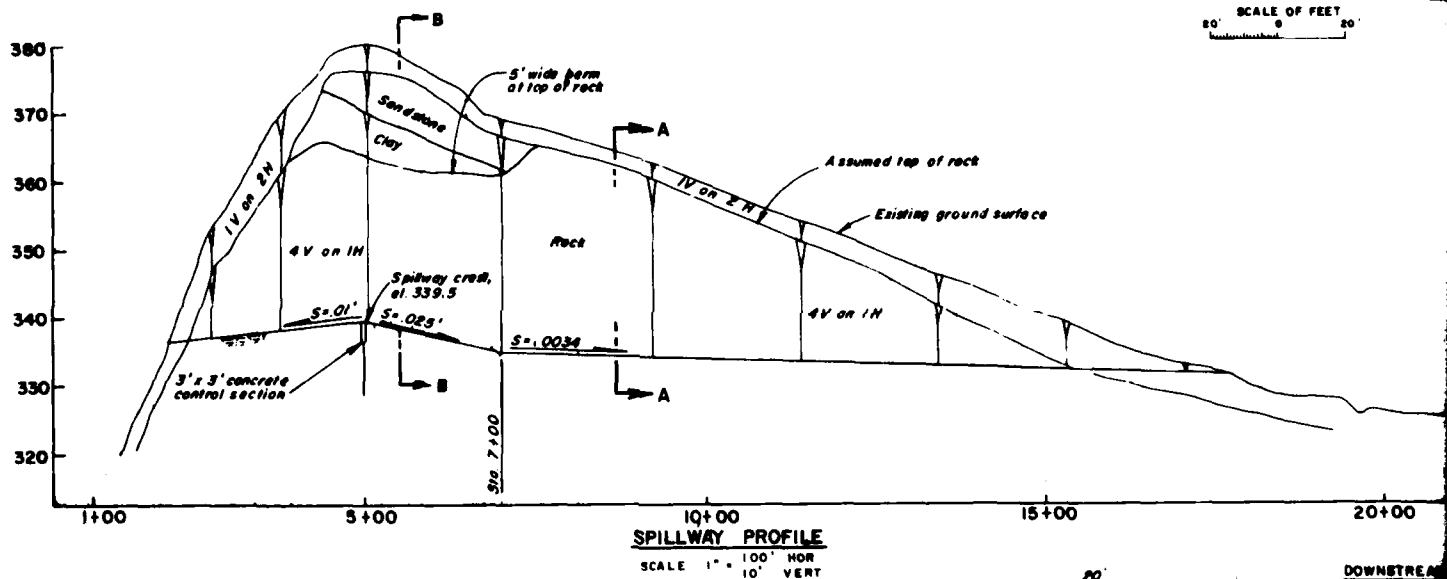
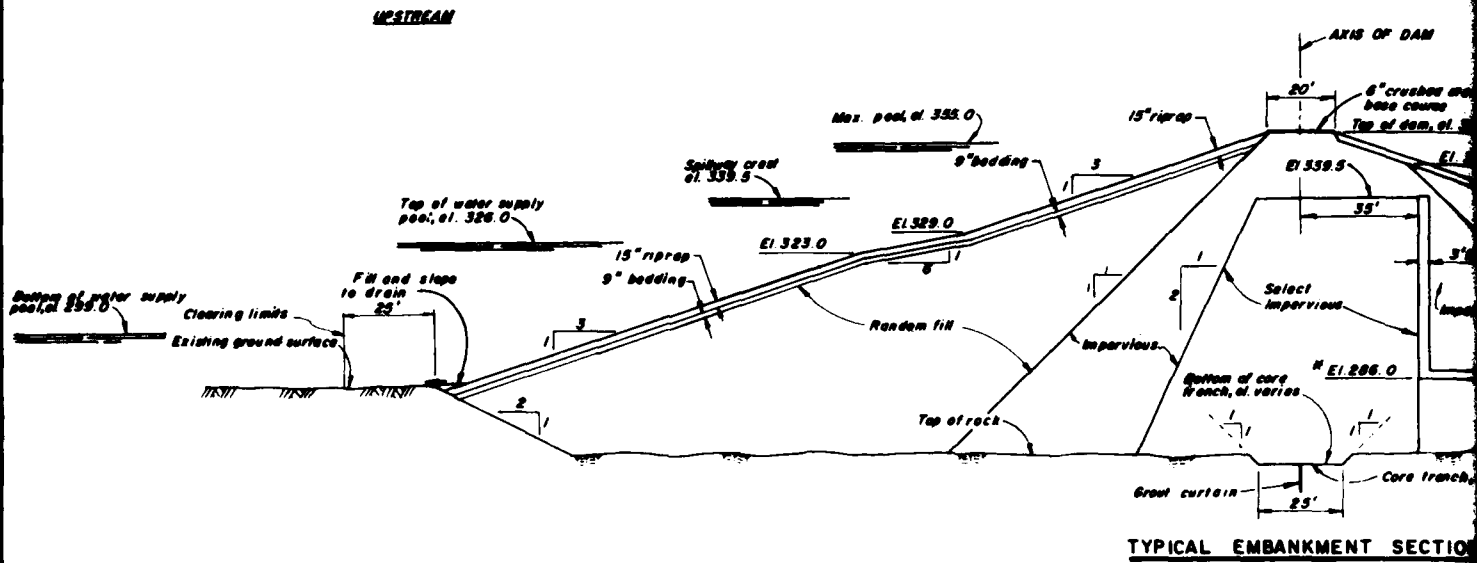
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FILE NO.	SHEET NO.	TITLE
GENERAL		
9689-62/1349	1	PROJECT LOCATION & INDEX TO DRAWINGS
9570-62/1351	2	EMBANKMENT & SPILLWAY PLAN
9570-62/1364	3	TYPICAL EMBANKMENT SECTION
9570-62/1357	4	EMBANKMENT & OUTLET WORKS EXCAV. PLAN
9570-62/1477	5	PLAN OF EXPLORATIONS-DAM & SPILLWAY
9570-62/1479	6	GEOLOGIC SECTIONS
9570-62/1372	7	DIKE PLAN & SECTION
9570-62/1486	8	GEOLOGIC SECTION-DIKE CENTER LINE
9570-62/1359	9	OUTLET WORKS PLAN & SECTION
9570-62/1435	10	STILLING BASIN PLAN & SECTION
9570-62/1482	11	GEOLOGIC SECTIONS-STILLING BASIN
9570-62/1487	12	FOUNDATION TREATMENT
FOUNDATION MAPS		
9689-62/1659	13	DAM AXIS-STA 9+10 TO STA 11+02
9689-62/1660	14	DAM AXIS-STA 11+10 TO STA 13+60
9689-62/1661	15	DAM AXIS-STA 13+60 TO STA 18+70
9689-62/1662	16	DAM AXIS-STA 18+70 TO STA 18+95
9689-62/1663	17	DAM AXIS-STA 18+95 TO STA 20+65
9689-62/1664	18	DIKE CORE TRENCH STA 19+50 TO STA 25+00
9689-62/1665	19	OUTLET WORKS-STILLING BASIN & INTAKE
9689-62/1666	20	OUTLET-CONDUIT STA 7+96.75 TO STA 9+56.75
9689-62/1667	21	OUTLET-CONDUIT STA 9+56.75 TO STA 11+36.75
9689-62/1668	22	OUTLET-CONDUIT STA 11+36.75 TO STA 12+16.75
9689-62/1669	23	GROUTING
9689-62/1670	24	GROUTING

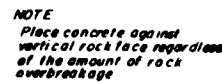
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DEPARTMENT OF THE ARMY LITTLE ROCK DISTRICT, CORPS OF ENGINEERS LITTLE ROCK, ARKANSAS			
DESIGNED BY	ARKANSAS RIVER AND TRIBUTARIES ARKANSAS RIVER, ARKANSAS		
RC	TOAD SUCK FERRY LOCK AND DAM		
DRAWN BY	RELOCATIONS		
CH	CONWAY WATER SUPPLY		
CHECKED BY	PROJECT LOCATION		
CD	AND INDEX TO DRAWINGS		
QUANTITY BY	APRIL 1983		
ENGINEER	DRAWING NUMBER 9689-62/1349		
SHEET 1 OF 24			



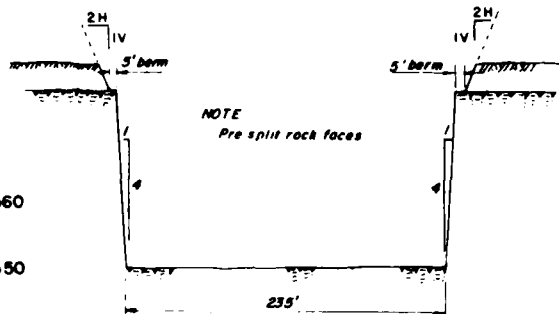
## WORK SAFELY



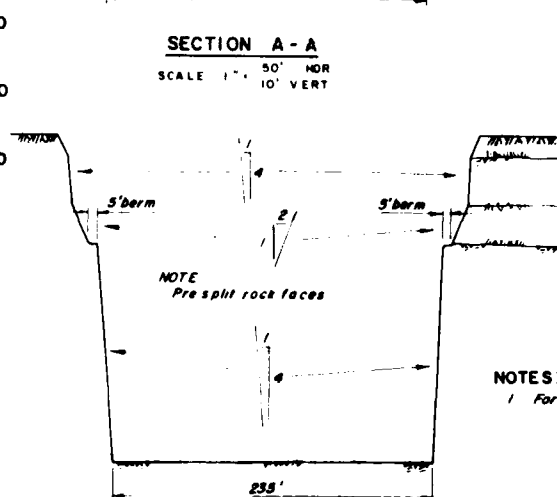




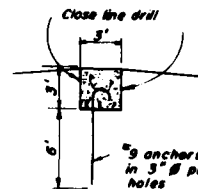
SCALE OF FEET  
20 0 20



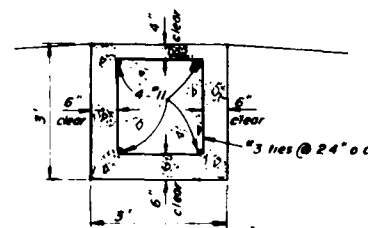
SCALE 1" = 50' HOR  
10' VERT



SCALE: 1" = 50' HORIZ  
10' VERT

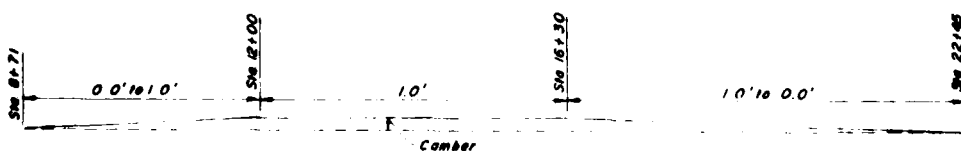


SCALE NONE

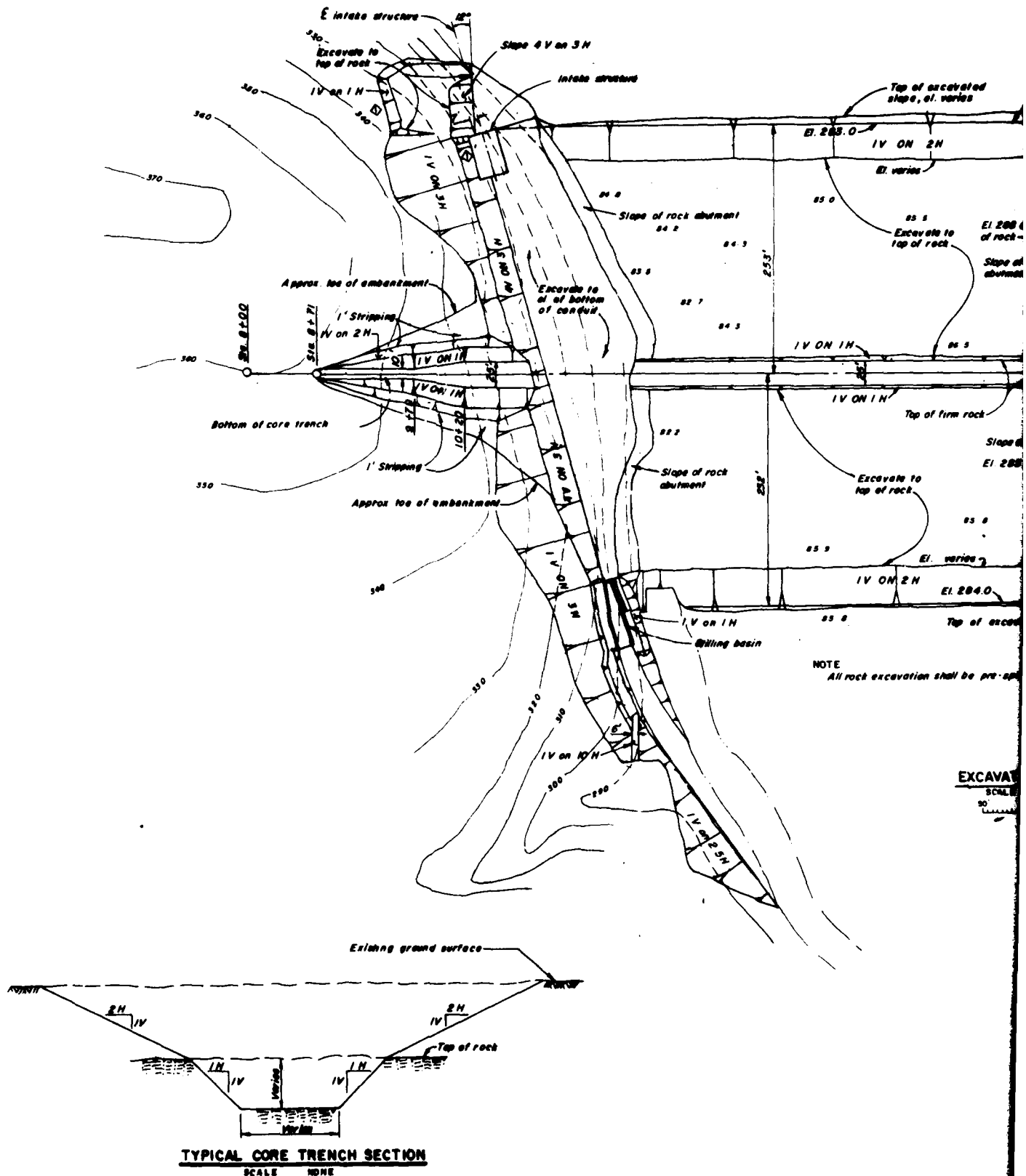


SCALE NONE

**CREST DETAIL**



REVISION	DATE	DESCRIPTION	BY
<p align="center"><b>DEPARTMENT OF THE ARMY</b>  <b>LITTLE ROCK DISTRICT. CORPS OF ENGINEERS</b>  <b>LITTLE ROCK, ARKANSAS</b></p>			
DESIGNED BY	ARKANSAS RIVER AND TRIBUTARIES	ARKANSAS RIVER, ARKANSAS	
J W	<p align="center"><b>TOAD SUCK FERRY LOCK AND DAM</b>  <b>RELOCATIONS</b>  <b>CONWAY WATER SUPPLY</b>  <b>TYPICAL EMBANKMENT SECTION</b>  <b>AND SPILLWAY PROFILE</b></p>		
DRAWN BY			
L L B			
CHECKED BY			
J W			
SUBMITTED BY	SCALE AS SHOWN	<p align="center"><b>AUGUST 1979</b>          HY. SERIAL NO. 80-C-0094</p>	
<i>Alvin C. Austin</i> ENGINEER	DRAWING NUMBER <p align="center"><b>9570/1364</b></p>		



WORK SAFELY

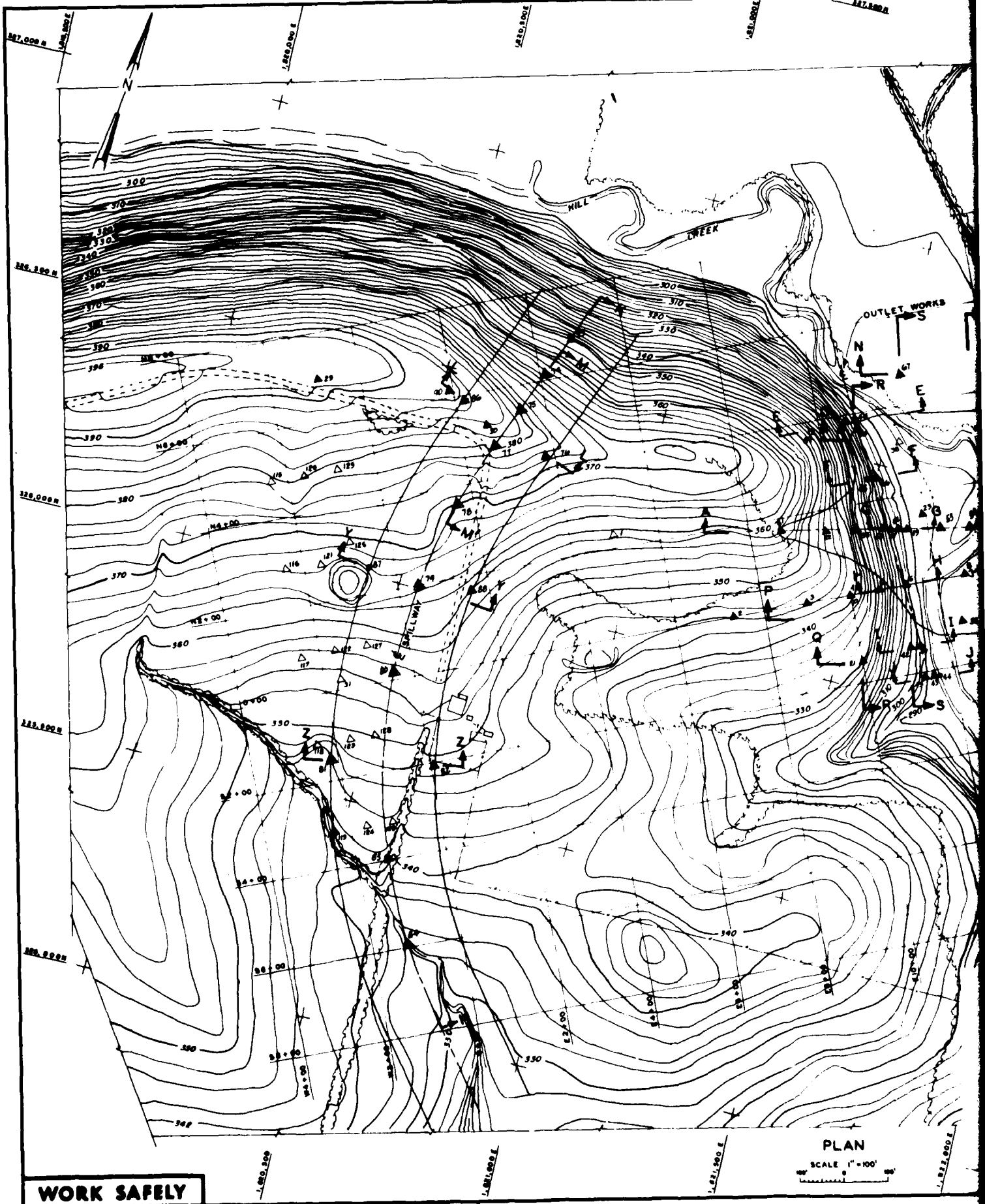
SCALE OF FEET  
50 0 50

**NOTE**  
*All rock excavation shall be pre-split*

- 1 For general notes See dwg 1350.
- 2 Excavation plan along conduit is shown on dwg.1358.
- 3 Excavation section along conduit and outlet channel is shown on dwg.1361
- 4 Existing topography is shown on dwg.1351
- 5 See dwg 1479 for elevation of core trench
- 6 See sections 2D and 2F for the specifications for foundation preparation

THIS DRAWING HAS BEEN REDUCED  
TO ONE-HALF THE ORIGINAL SCALE

⑦ <i>M-172</i> <i>Review station sheet in place</i> <i>Amend No. 000</i>		116 BY
REVISION	DATE	DESCRIPTION
DEPARTMENT OF THE ARMY LITTLE ROCK DISTRICT, CORPS OF ENGINEERS LITTLE ROCK, ARKANSAS		
DESIGNED BY J W	ARKANSAS RIVER AND TOWNSHIPS ARKANSAS RIVER, ARKANSAS TOAD SUCK FERRY LOCK AND DAM RELOCATIONS CONWAY WATER SUPPLY EMBANKMENT AND OUTLET WORKS EXCAVATION PLAN	
DRAWN BY L L B		
CHECKED BY J W		
DESIGNED BY <i>William C. Austin</i> (Signature)	SCALE AS SHOWN	AUGUST 1979 BY: <i>WILLIAM C. AUSTIN</i>
SHEET NO. <b>2570 - 62/1357</b>		



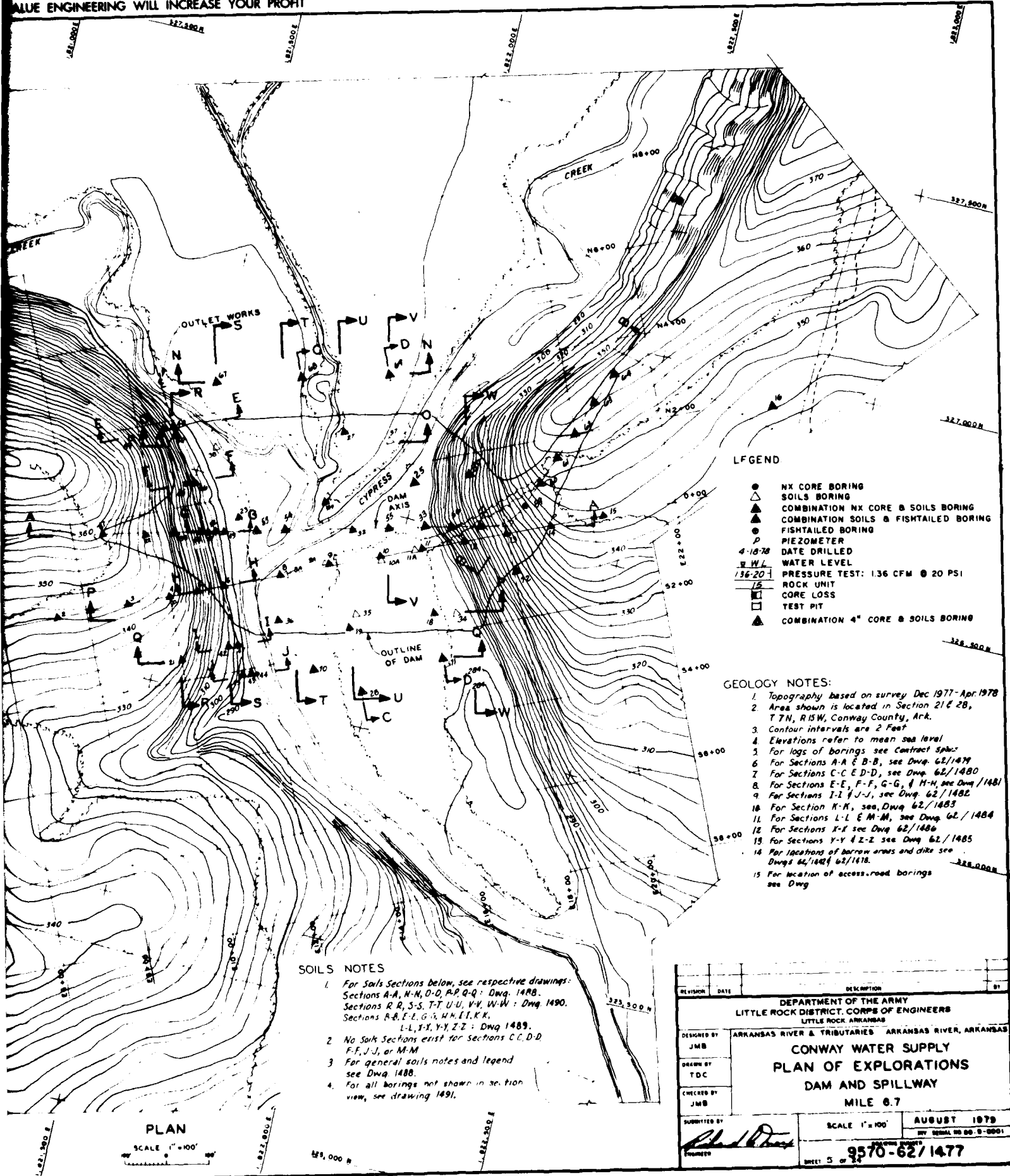
WORK SAFELY

PLAN

SCALE 1" = 100'



VALUE ENGINEERING WILL INCREASE YOUR PROFIT



LEGEND

- NX CORE BORING
- △ SOILS BORING
- ▲ COMBINATION NX CORE & SOILS BORING
- ⊙ COMBINATION SOILS & FISHTAILED BORING
- PIEZOMETER
- ⊖ DATE DRILLED
- W/L WATER LEVEL
- 136-20 PRESSURE TEST: 1.36 CFM @ 20 PSI
- 15 ROCK UNIT
- CORE LOSS
- TEST PIT
- ▲ COMBINATION 4" CORE & SOILS BORING

GEOLOGY NOTES:

1. Topography based on survey Dec 1977-Apr 1978
2. Area shown is located in Section 21 & 28, T 7 N, R 15 W, Conway County, Ark.
3. Contour intervals are 2 Feet
4. Elevations refer to mean sea level
5. For logs of borings see Contract specs
6. For Sections A-A & B-B, see Dwg. 62/1479
7. For Sections C-C & D-D, see Dwg. 62/1480
8. For Sections E-E, F-F, G-G, & H-H, see Dwg. 62/1481
9. For Sections I-I & J-J, see Dwg. 62/1482
10. For Section K-K, see Dwg. 62/1483
11. For Sections L-L & M-M, see Dwg. 62/1484
12. For Sections X-X & Y-Y, see Dwg. 62/1486
13. For Sections V-V & Z-Z, see Dwg. 62/1485
14. For locations of borrow areas and dike see Dwg. 64/1484 & 62/1478
15. For location of access road borings see Dwg.

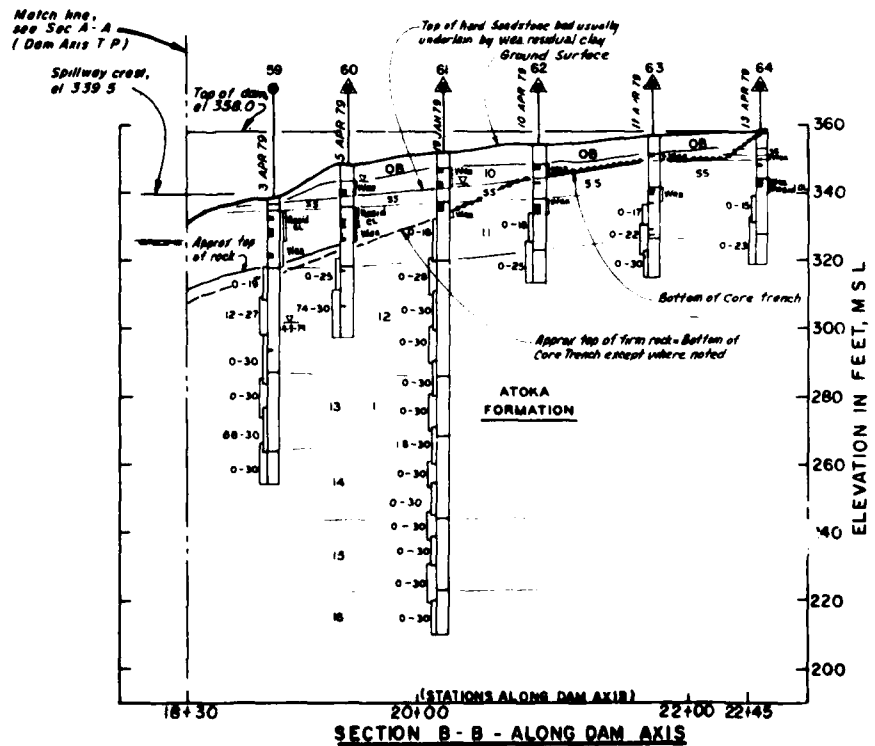
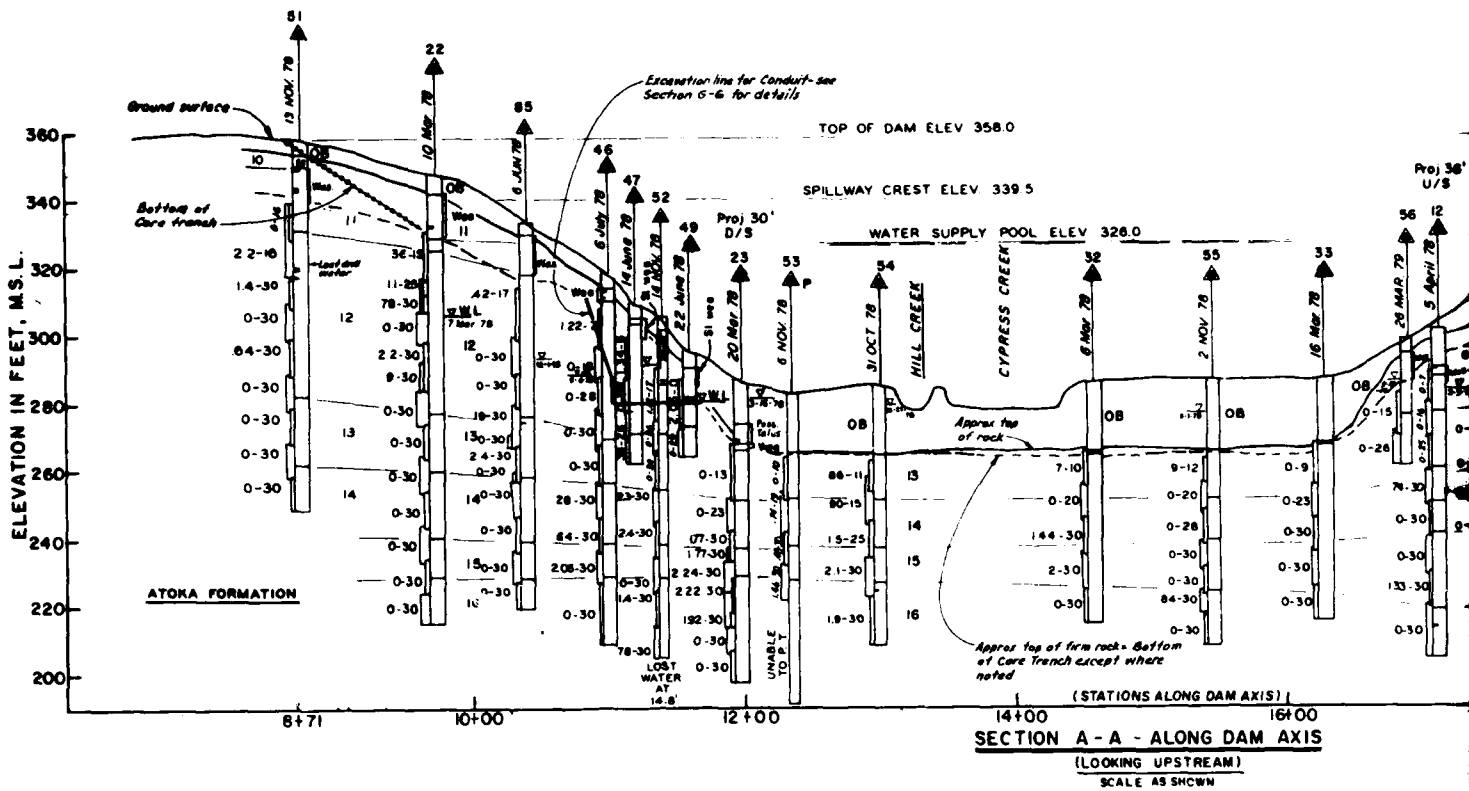
SOILS NOTES

1. For Soils Sections below, see respective drawings:  
Sections A-A, N-N, D-D, R-R, Q-Q: Dwg. 1488.  
Sections R-R, S-S, T-T, U-U, V-V, W-W: Dwg. 1490.  
Sections R-R, E-E, G-G, H-H, I-I, K-K, L-L, X-X, Y-Y, Z-Z: Dwg. 1489.
2. No Soils Sections exist for Sections C-C, D-D, F-F, J-J, or M-M
3. For general soils notes and legend see Dwg. 1488.
4. For all borings not shown in section view, see drawing 1491.

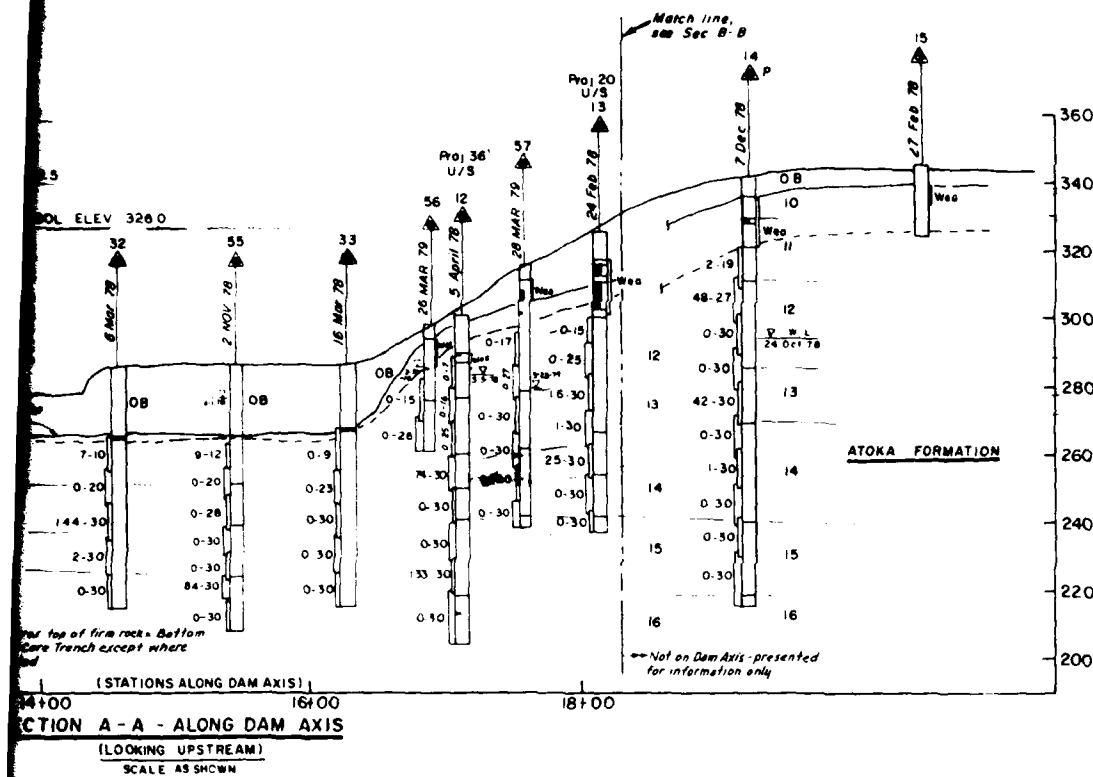
PLAN

SCALE 1" = 100'

REVISION	DATE	DESCRIPTION	BY
DEPARTMENT OF THE ARMY LITTLE ROCK DISTRICT, CORPS OF ENGINEERS LITTLE ROCK, ARKANSAS			
DESIGNED BY	JMB	ARKANSAS RIVER & TRIBUTARIES ARKANSAS RIVER, ARKANSAS	
DRAWN BY	TDC	CONWAY WATER SUPPLY	
CHECKED BY	JMB	PLAN OF EXPLORATIONS	
SUBMITTED BY		DAM AND SPILLWAY	
THOMAS		MILE 6.7	
SCALE 1" = 100'		AUGUST 1979	
BY SERIAL NO. 00-0-0001		9570-62/1477	
SHEET 5 OF 11			



## WORK SAFELY



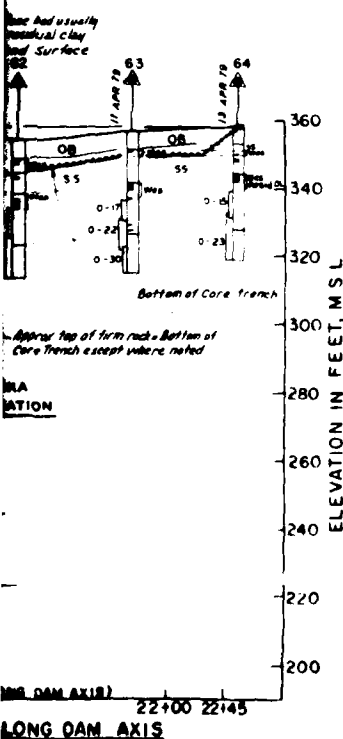
GENERALIZED GEOLOGIC COLUMN			
SYSTEM	FORMATION	SECTION	DESCRIPTION
PENNSYLVANIAN	ATOKA	7	SANDSTONE, HARD, FINE TO MEDIUM GRAINED, MEDIUM GRAY, BRICKLE, FOUND ONLY IN THE HIGHER ELEVATIONS OF BOTH ABUTMENTS AS A CAPPING STRATA, USUALLY SLIGHTLY WEATHERED
		10	
		14	SANDSTONE, MODERATELY HARD TO HARD, CEMENTED, FINE GRAINED, BLACK TO MEDIUM GRAY, BRICKLE, NUMEROUS SANDSTONE LAMINATIONS & INCLUSIONS, SOME LENSES OF SHALE SANDSTONE
		11	
		13	SANDSTONE, HARD TO MODERATELY HARD, FINE GRAINED, CEMENTED, BLACK TO MEDIUM GRAY, BRICKLE, NUMEROUS THICK TO THIN, OFTEN IRREGULAR SANDSTONE LAMINATIONS & INCLUSIONS, FORMS OF WHICH OCCASIONALLY GRADE INTO SHALE SANDSTONE
		12	
		11	SHALE, SANDY, HARD TO MODERATELY HARD, FINE GRAINED, CEMENTED, BLACK TO MEDIUM GRAY, BRICKLE, NUMEROUS SANDSTONE LAMINATIONS & INCLUSIONS, OCCASIONAL SHALE SANDSTONE LENSES
		13	
		5	SHALE, SANDY, HARD TO MODERATELY HARD, FINE GRAINED, CEMENTED, BLACK TO MEDIUM GRAY, BRICKLE, SCATTERED SANDSTONE LAMINATIONS & INCLUSIONS
		14	
		7	SHALE, SANDY, HARD TO MODERATELY HARD, FINE GRAINED, CEMENTED, BLACK TO MEDIUM GRAY, BRICKLE, SCATTERED SANDSTONE LAMINATIONS & INCLUSIONS
		15	
		10	SHALE, MODERATELY HARD TO HARD, FINE GRAINED TO SILTY, BLACK, BRICKLE, SCATTERED HARD SILTYSTONE, MUDCLASTS & LENSES ARE ENCOUNTERED IN THIS UNIT STARTING FROM ABOUT 10 TO 15 FEET BELOW ITS TOP SURFACE
		16	

# LEGEND

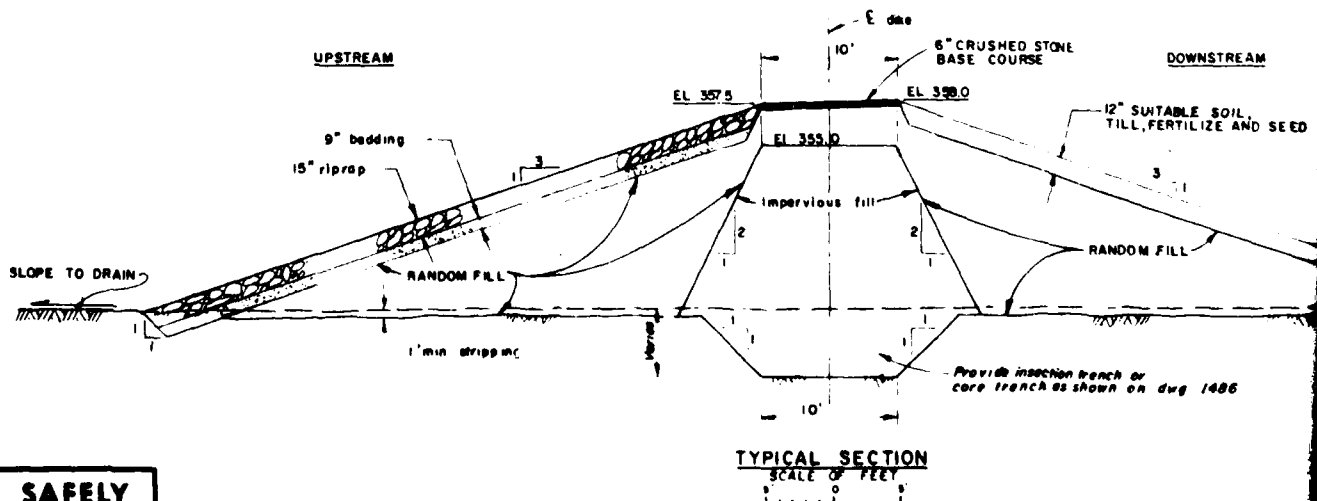
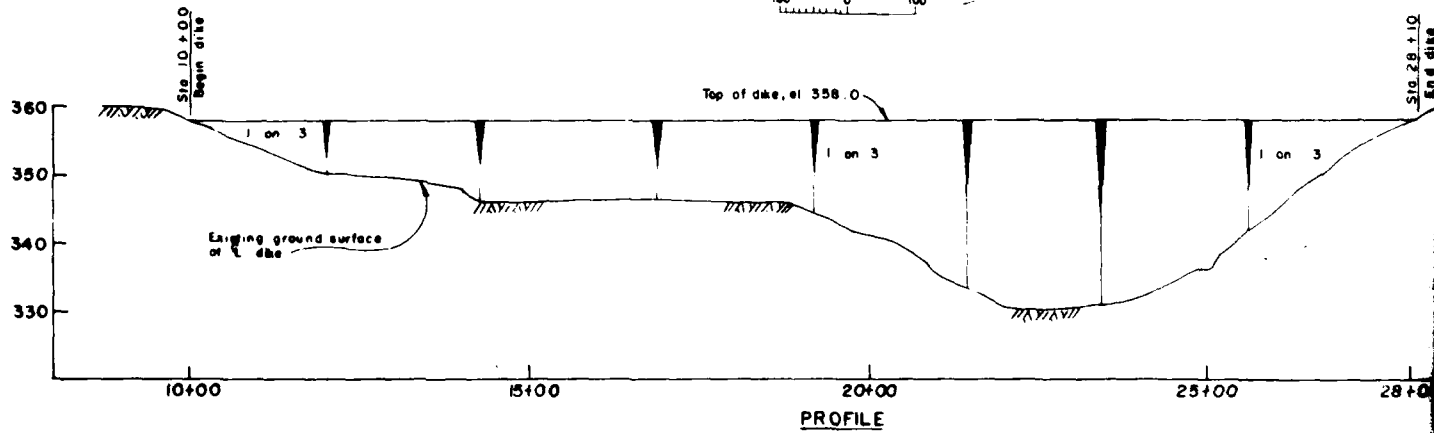
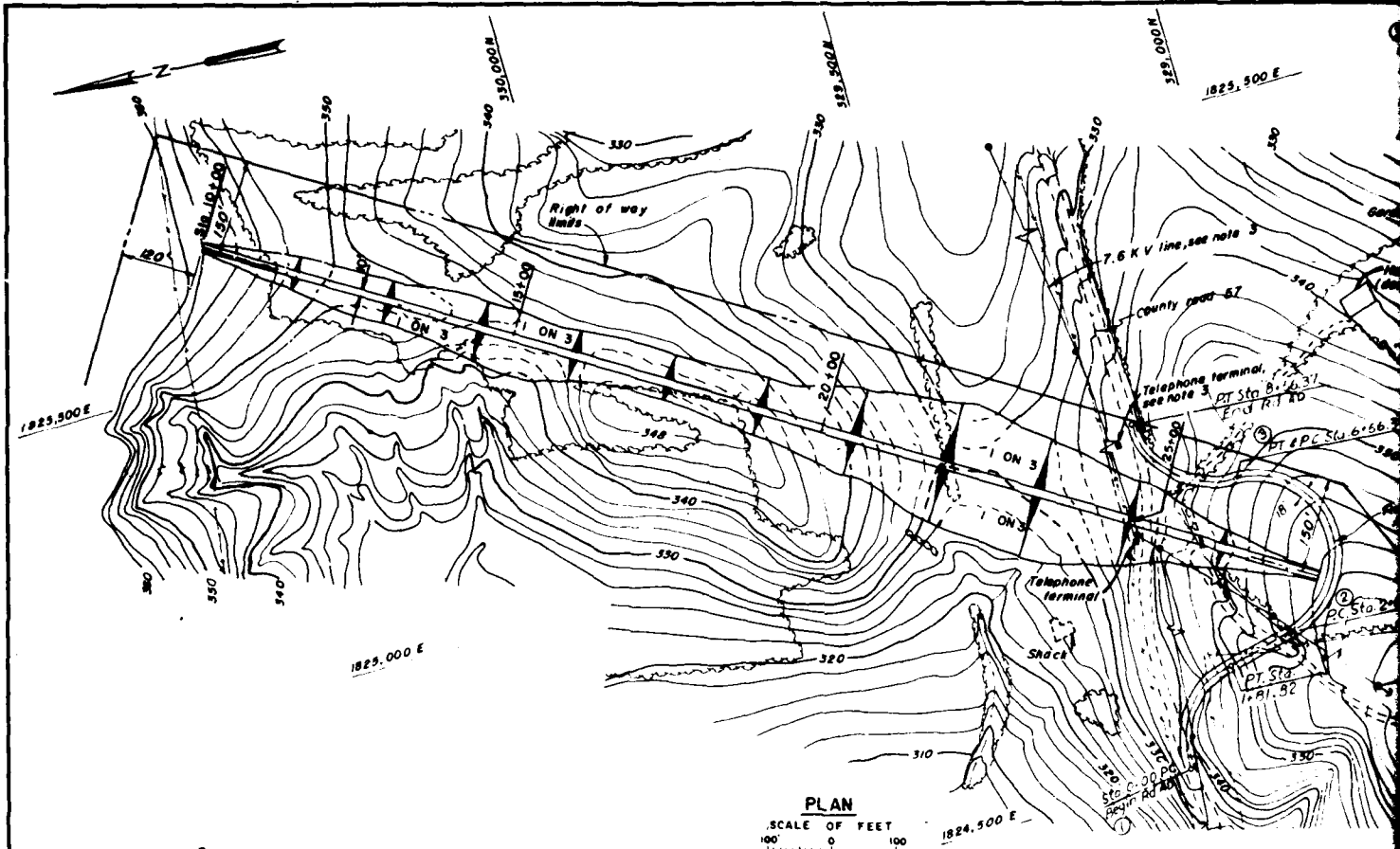
- NX CORE BORING
- ▲ SOILS BORING
- ▲ COMBINATION NX CORE & SOILS BORING
- ▲ COMBINATION SOILS & FISHTAILED BORING
- FISHTAILED BORING
- P PIEZOMETER
- 4-10-78 DATE DRILLED
- W.L. WATER LEVEL
- 136-20-1 PRESSURE TEST: 136 CFM @ 20 PSI
- 15 ROCK UNIT
- CORE LOSS
- TEST PIT

## NOTES

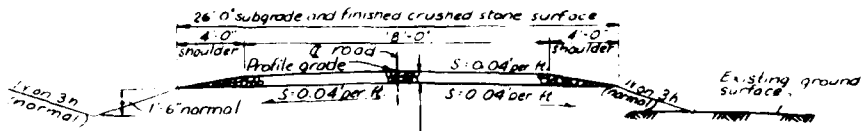
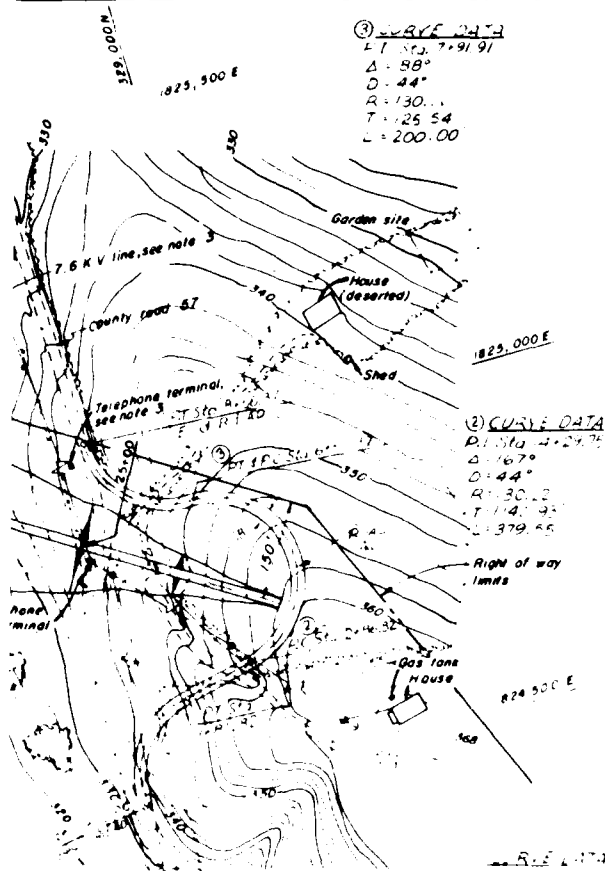
- For general notes see Drawing 62/1477
- For location of sections, see Drawing 62/1477
- For detailed information of borings, pressure tests, core loss, weathering, fractures, joints, see logs of borings, contract specs
- For overburden information see soil logs, contract specs



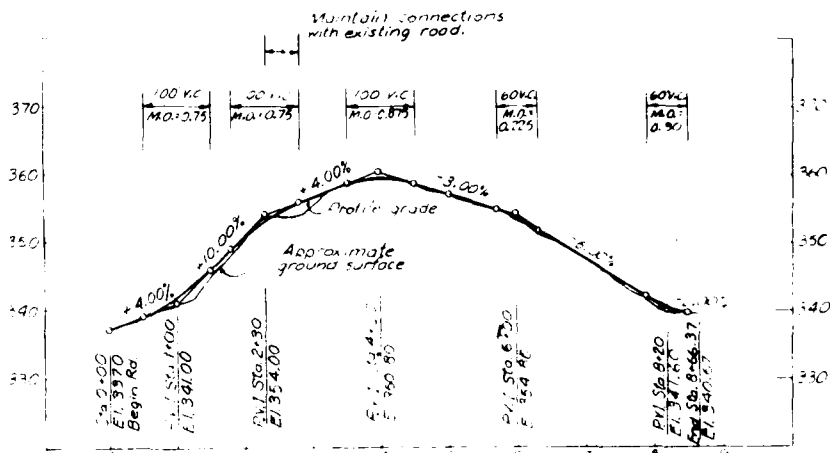
DEPARTMENT OF THE ARMY LITTLE ROCK DISTRICT, CORPS OF ENGINEERS LITTLE ROCK, ARKANSAS	
DESIGNED BY S C H	ARKANSAS RIVER AND TRIBUTARIES ARKANSAS RIVER, ARKANSAS
DRAWN BY L L B	TOAD SUCK FERRY LOCK AND DAM RELOCATIONS CONWAY WATER SUPPLY
CHECKED BY R H F	GEOLOGIC SECTIONS A-A AND B-B ALONG DAM AXIS
SUBMITTED BY <i>Robert H. Foy</i>	SCALE AS SHOWN
ENGINEER	AUGUST 1978 REV. SERIAL NO. 80, S. 008
DRAWING NUMBER 9570-62/1479	
SHEET 6 OF 8	



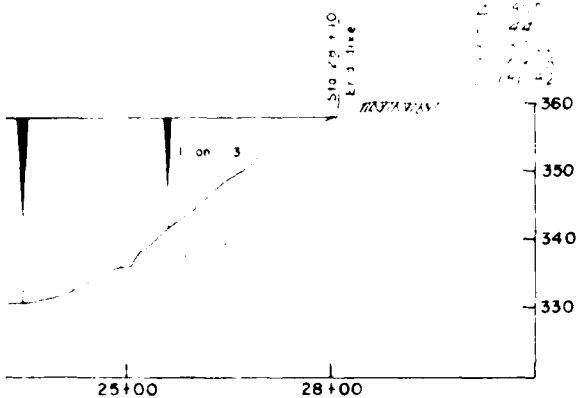
**WORK SAFELY**



TYPICAL SECTION  
(Rel. AD) Road around dike

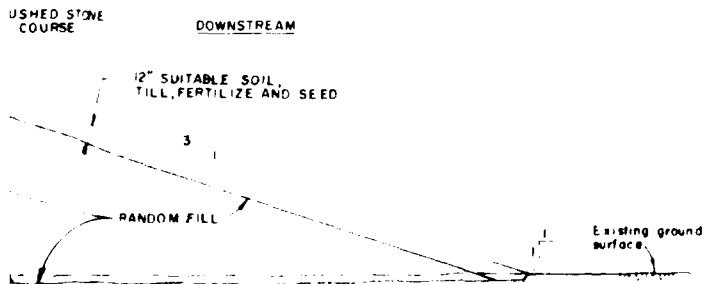


PROFILE (80) A 214 03 10703 Jike



## NOTES

- 1 For limits of ROW see dwg 1352
- 2 Clear 25' upstream and downstream of for
- 3 The contractor shall be responsible for arrangements with the owners of the utility lines for the relocation of these lines, see general notes dwg 1350



vide inspection trench of  
e trench as shown on dwg 1486

REPORT NO.	DATE	DESCRIPTION	BY
DESIGNED BY	JOHANNAS RIVER AND TRIBUTARIES	ARKANSAS RIVER ARKANSAS	
CHECKED BY			
DRAWN BY			
LISTED BY			
REVIEWED BY			
APPROVED BY			
PROJECT NO.			
DATE			
ENGINEER			

DEPARTMENT OF THE ARMY  
 LITTLE ROCK DISTRICT CORPS OF ENGINEERS  
 LITTLE ROCK ARKANSAS

TOAD SUCK FERRY LOCK AND DAM  
 RELOCATIONS  
 CONWAY WATER SUPPLY  
 DIKE  
 PLAN, PROFILE AND TYPICAL SECTION

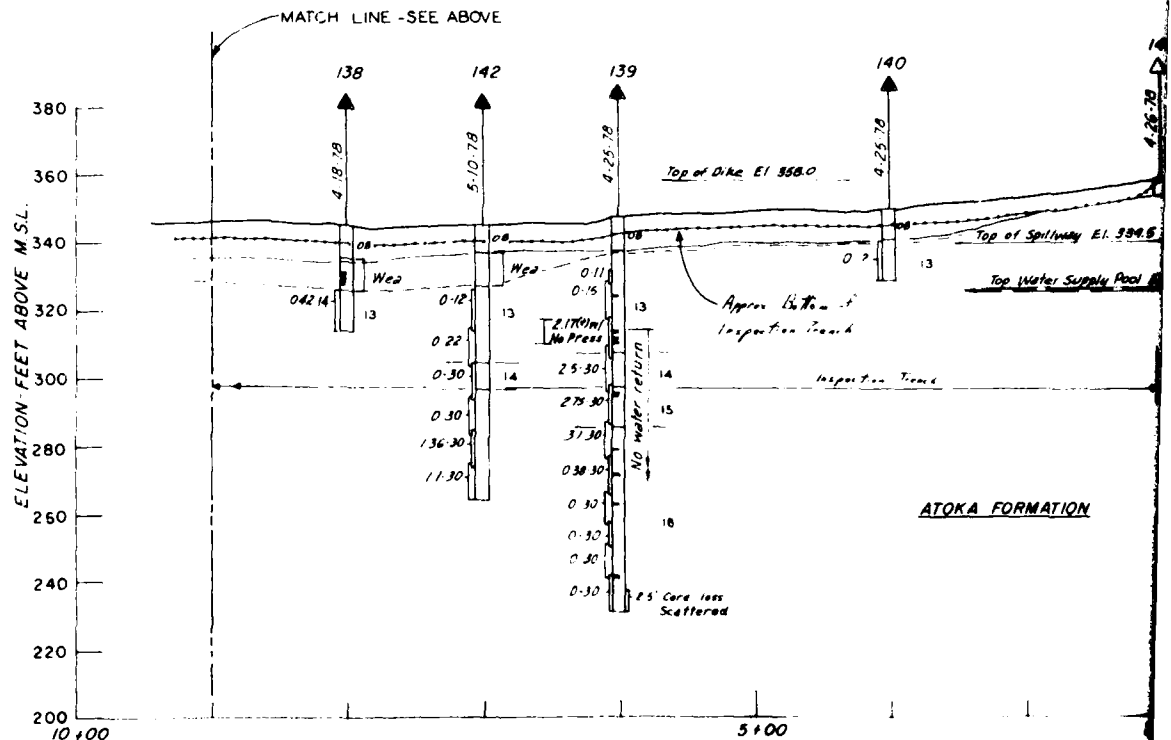
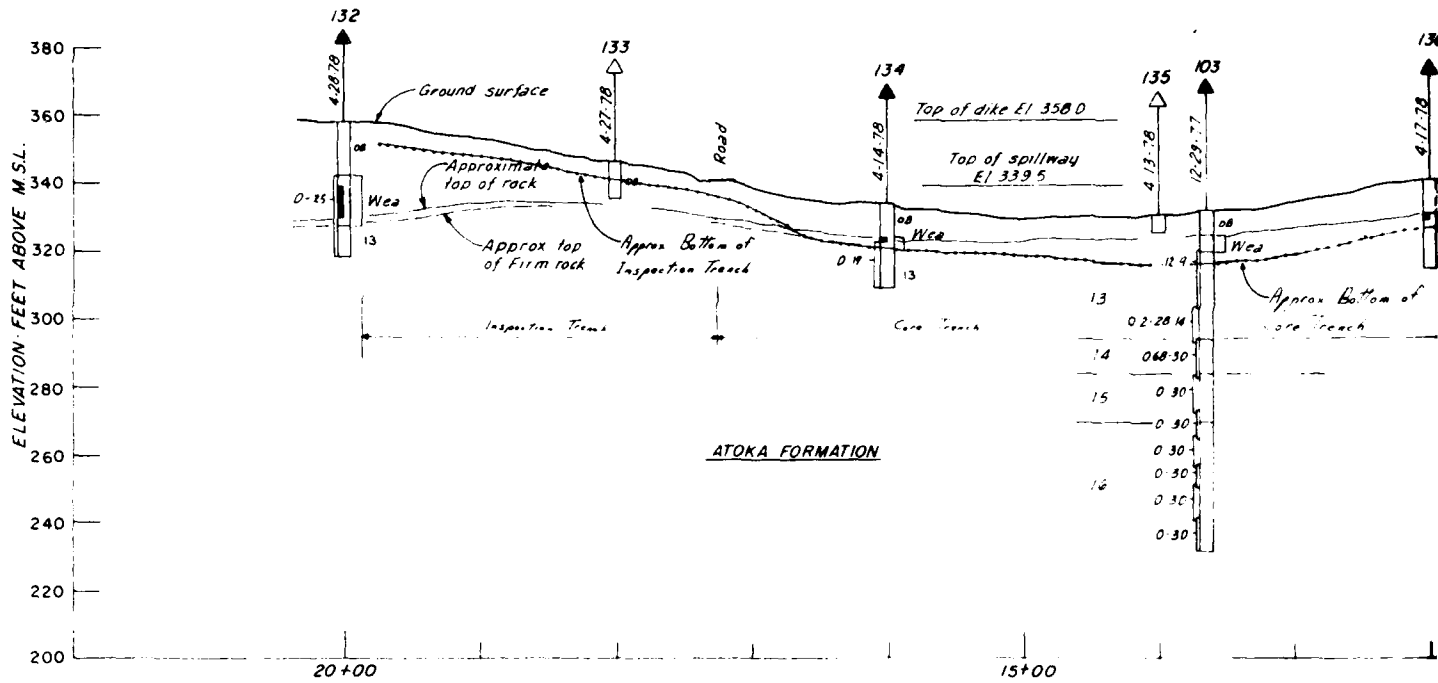
SCALE AS SHOWN

AUGUST 1979

REV. SERIAL NO. 80-B 0001

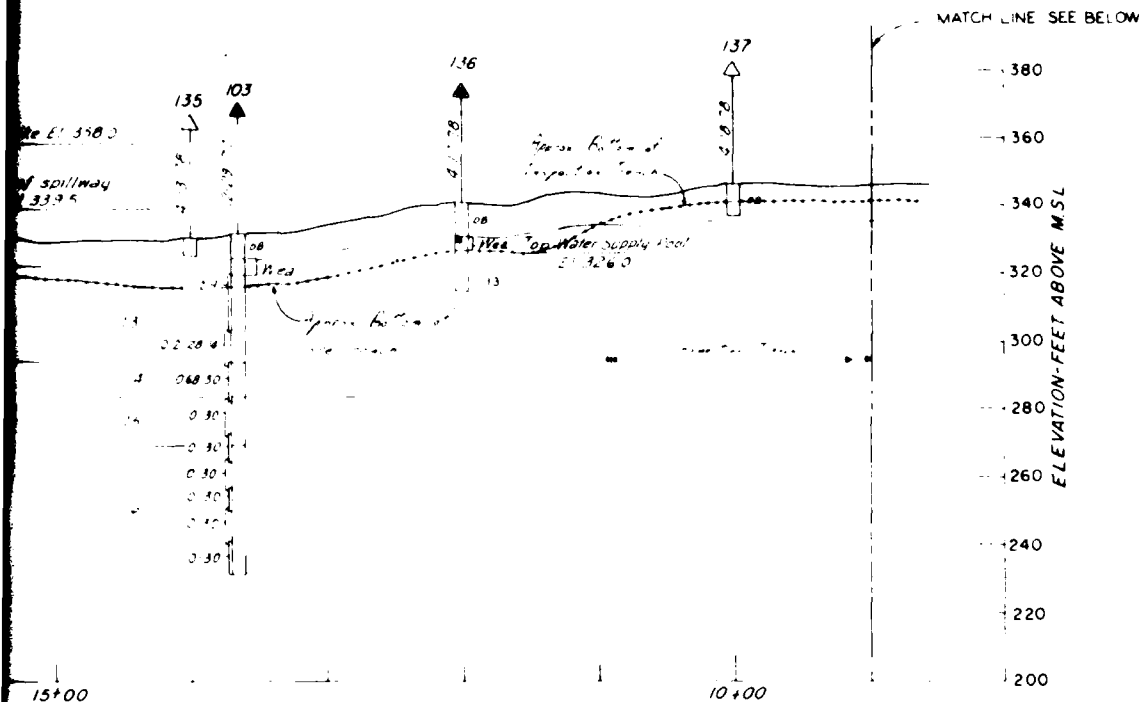
DRAWING NUMBER

5750-62/1372



**SECTION X-X**  
**ALONG E OF DIKE**  
**(LOOKING LAKEWARD)**  
**SCALE AS SHOWN**

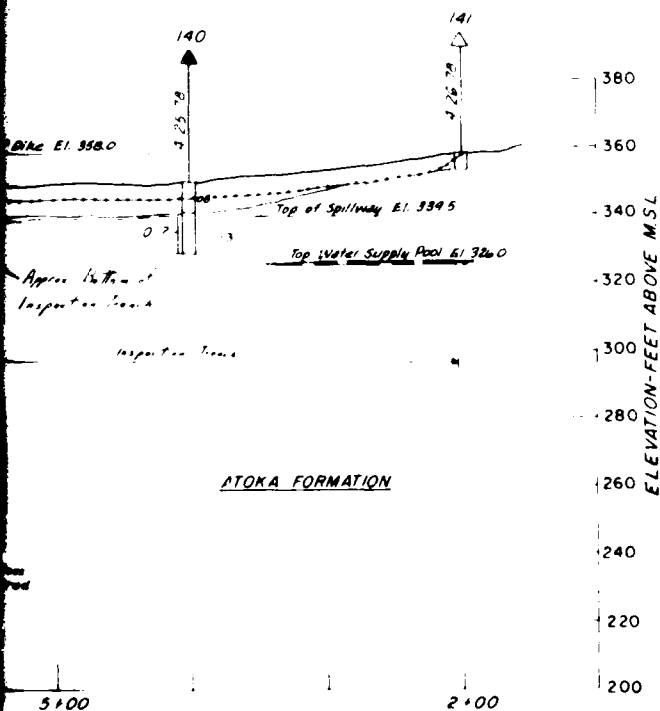
## WORK SAFELY



GENERALIZED GEOLOGIC COLUMN					
SYSTEM	FORMATION	SECTION	THICKNESS IN FEET	UNIT	DESCRIPTION
PENNSYLVANIAN	ATOKA		1 10 30	40	SANDSTONE, HARD FINE TO MEDIUM GRAINED, MEDIUM GRAY MICACEOUS, FOLDED ONLY IN THE HIGHER ELEVATIONS OF BOTH SUBTERRANEAN AS A CAPPING STRATA, USUALLY SLIGHTLY WEATHERED
			14 27	11	SANDSTONE, MODERATELY HARD TO HARD, CEMENTED FINE GRAINED, BLACK TO MEDIUM GRAY MICACEOUS, NUMEROUS SANDSTONE LAMINATIONS & INCLUSIONS, SOME LENSES OF SHALE & SANDSTONE
			13 48	12	SANDSTONE, HARD TO MODERATELY HARD, FINE GRAINED, CEMENTED BLACK TO MEDIUM GRAY MICACEOUS, NUMEROUS THICK TO THIN, OFTEN MEDIUM SANDSTONE LAMINATIONS & INCLUSIONS, SOME OF WHICH OCCASIONALLY GRADE UP TO SHALE & SANDSTONE
			11 27	13	SANDSTONE, HARD TO MODERATELY HARD, FINE GRAINED, CEMENTED BLACK TO MEDIUM GRAY MICACEOUS, NUMEROUS SANDSTONE LAMINATIONS & INCLUSIONS, OCCASIONALLY SHALE & SANDSTONE LENSES
			5 14 20	14	SANDSTONE, MODERATELY HARD TO MODERATELY HARD, FINE GRAINED, CEMENTED BLACK TO MEDIUM GRAY MICACEOUS, SCATTERED SANDSTONE LAMINATIONS & INCLUSIONS
			7 24	15	SANDSTONE, MODERATELY HARD TO MODERATELY HARD, FINE GRAINED, CEMENTED BLACK TO MEDIUM GRAY, WIDELY SCATTERED SANDSTONE LAMINATIONS & INCLUSIONS
			37	16	SANDSTONE, MODERATELY HARD TO HARD, FINE GRAINED TO MEDIUM GRAY MICACEOUS, SCATTERED HARD IN STONE MODULES & LENSES ARE ENCOUNTERED IN THIS UNIT, STARTING FROM ABOUT 10 TO 15 FEET BELOW ITS TOP SURFACE

LEGEND

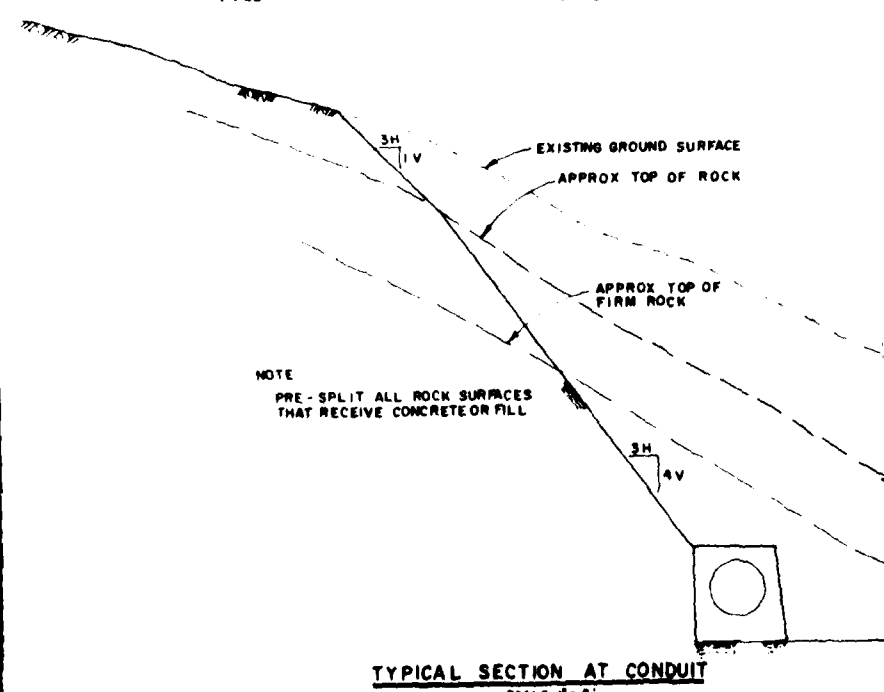
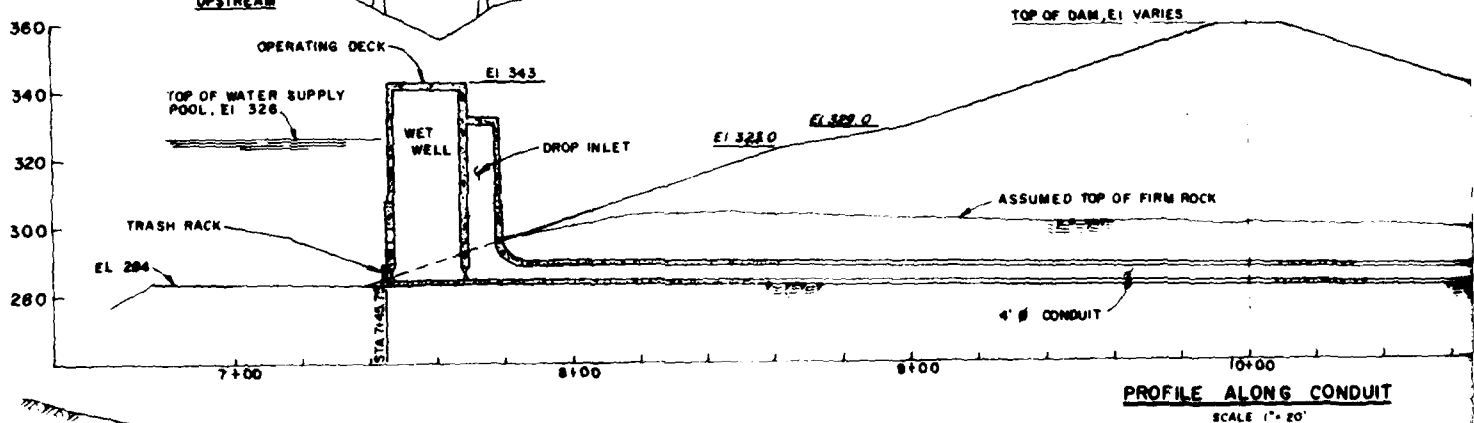
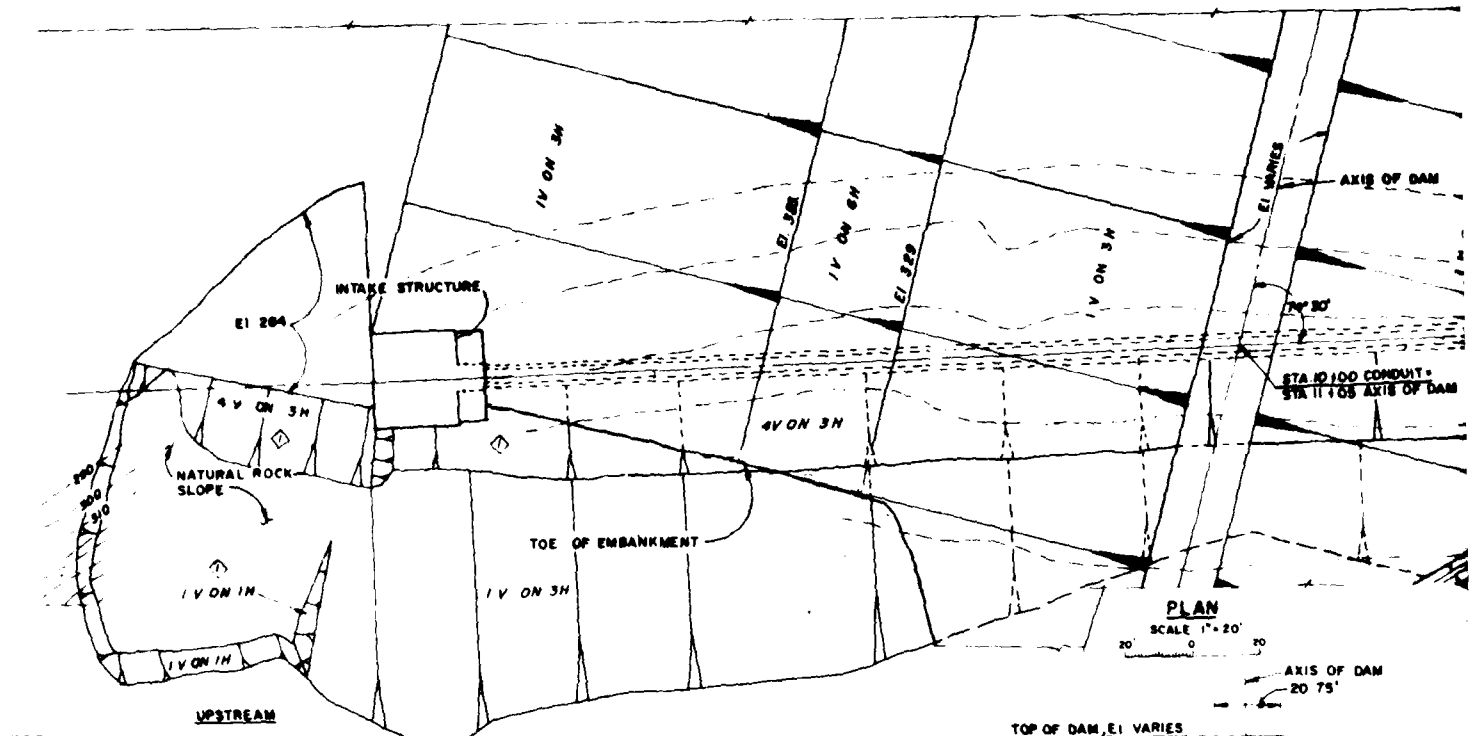
- NX CORE BORING
- △ SOILS BORING
- ▲ COMBINATION NX CORE & SOILS BORING
- ▲ COMBINATION SOILS & FISHTAILED BORING
- FISHTAILED BORING
- P PIEZOMETER
- 4-18-78 DATE DRILLED
- W.L. WATER LEVEL
- 136-20-1 PRESSURE TEST: 136 CFM @ 20 PSI
- 14 ROCK UNIT
- 1 CORE LOSS



NOTES

- 1 For general notes see drawing 62/1477
- 2 For location of Section see drawing 62/1478
- 3 For detailed information of Borings, Pressure Tests, Core Loss, weathering, fractures, joints, see Boring Logs, Contract Specs
- 4 For overburden information see Soils Logs, Contract Specs

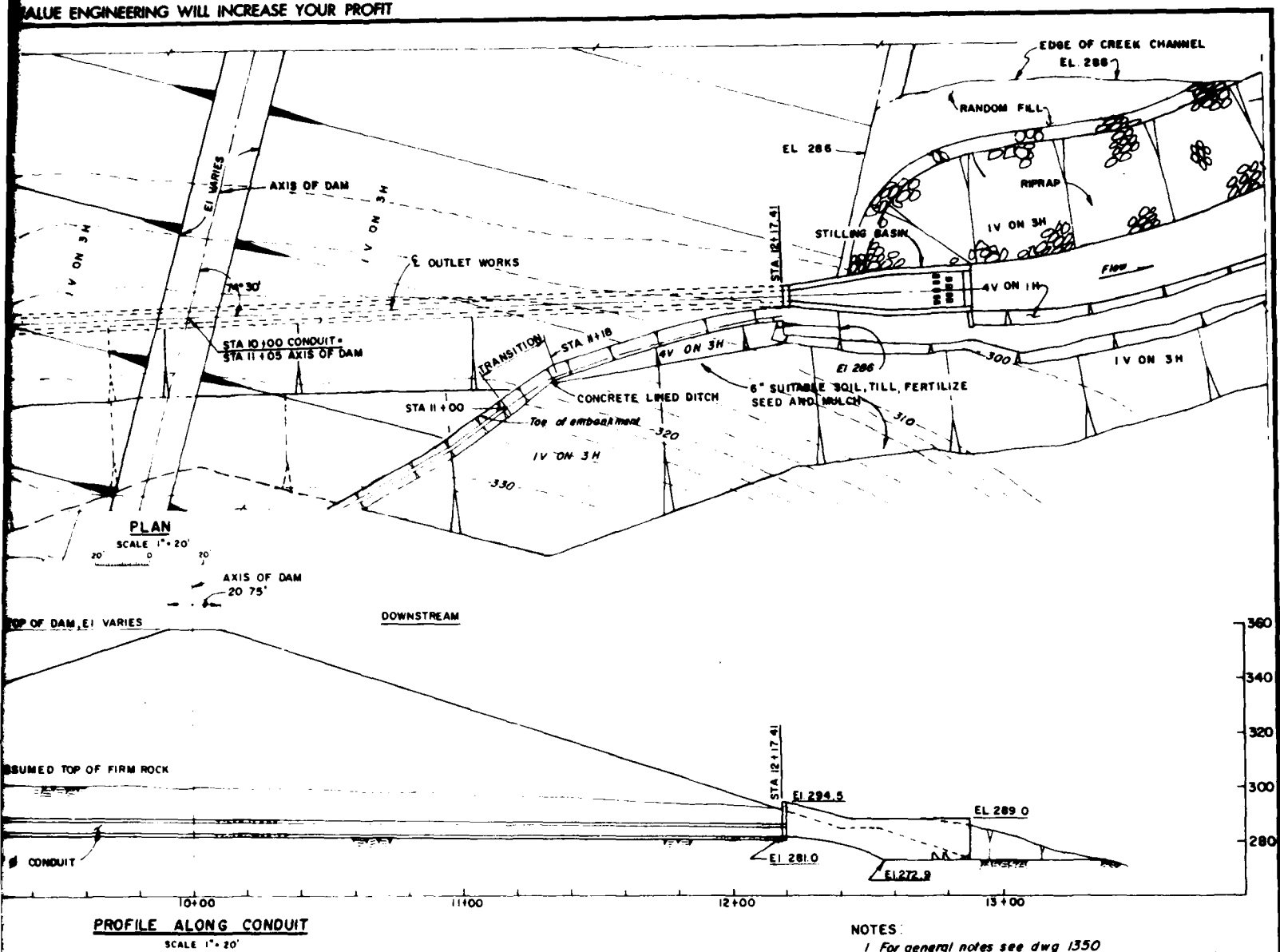
REVISION	DATE	DESCRIPTION	BY
DEPARTMENT OF THE ARMY LITTLE ROCK DISTRICT, CORPS OF ENGINEERS LITTLE ROCK, ARKANSAS			
DESIGNED BY	JMB	ARIZONA RIVER AND TRIBUTARIES	ARIZONA RIVER, ARIZONA
DRAWN BY	JEP	TOAD SUCK FERRY LOCK AND DAM	
CHECKED BY	RKF	RELOCATIONS	
SUBMITTED BY		AUGUST 1978	
ENGINEER		SCALE AS SHOWN	BY SERIAL NO. 60-1-60-1
9570-62/1486		SHEET 8 OF 28	



WORK SAFELY



VALUE ENGINEERING WILL INCREASE YOUR PROFIT

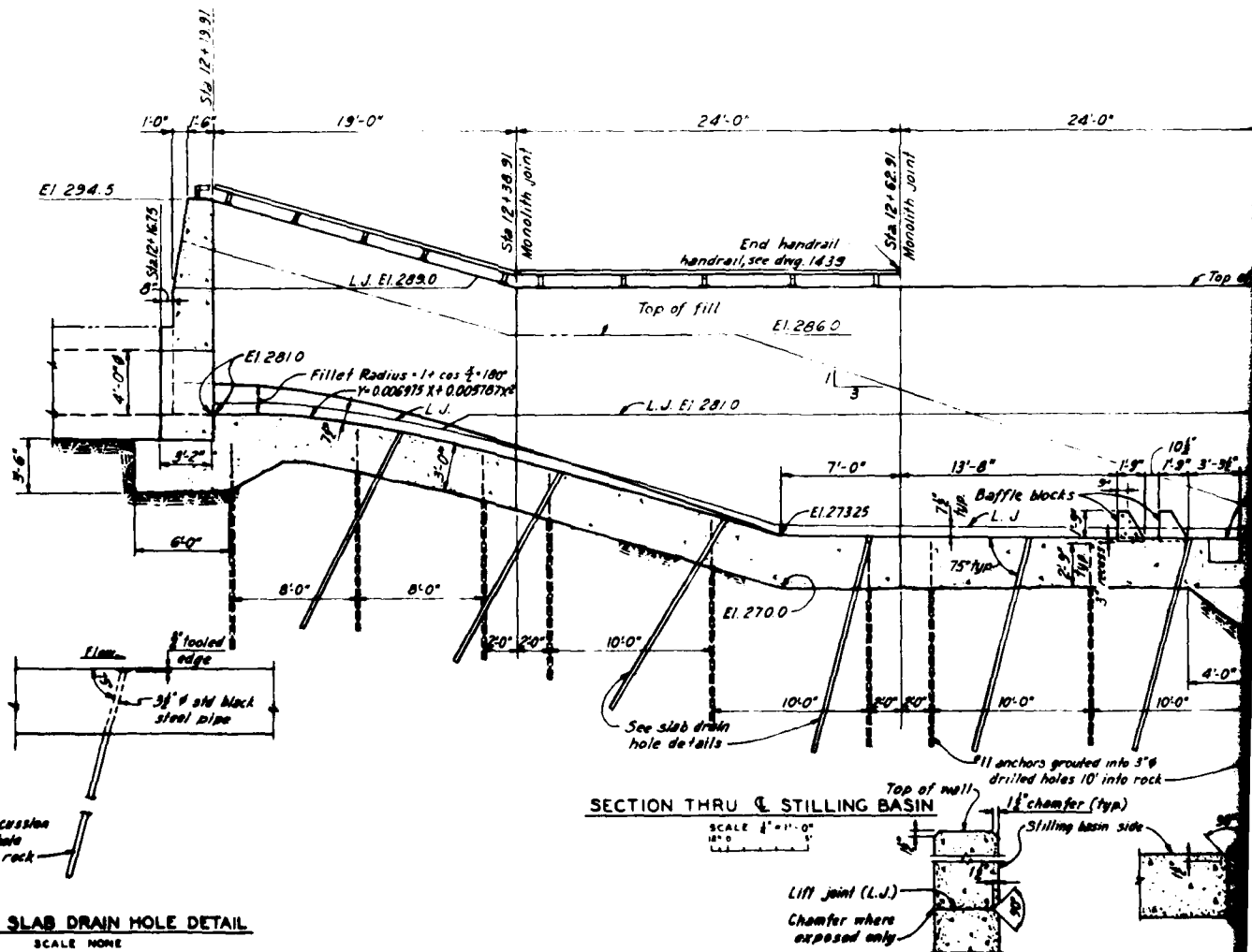
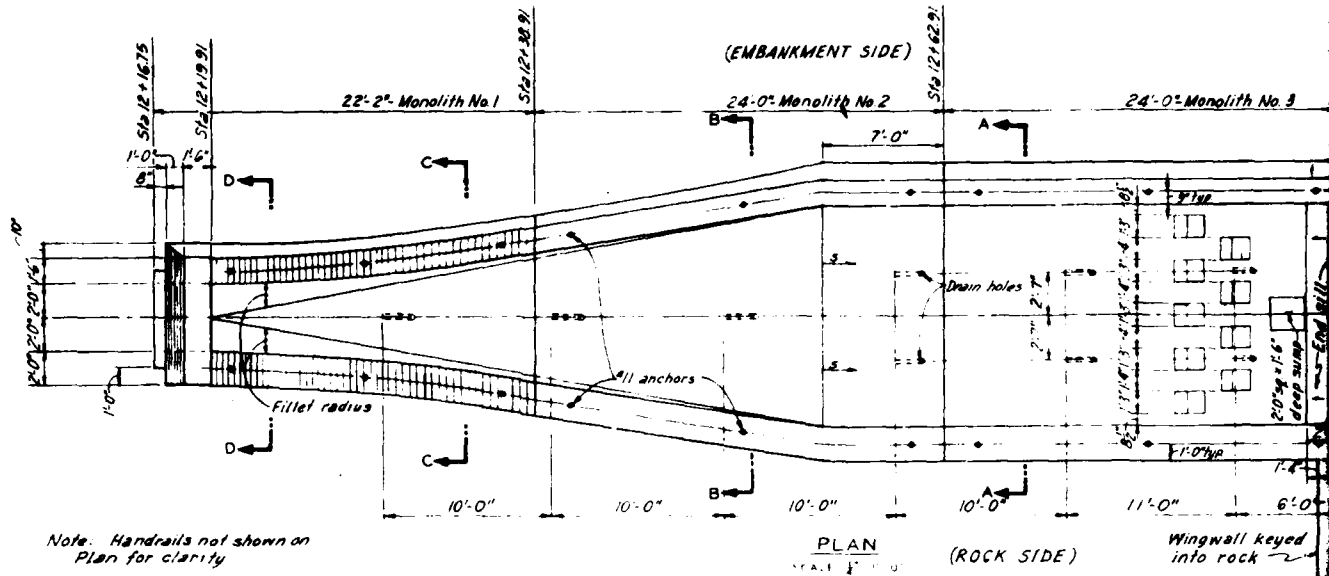


THIS DRAWING HAS BEEN REDUCED  
TO ONE-HALF THE ORIGINAL SCALE

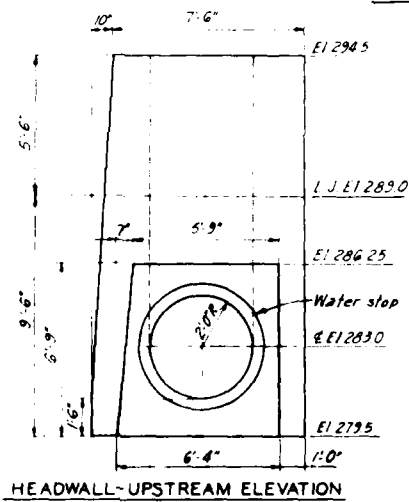
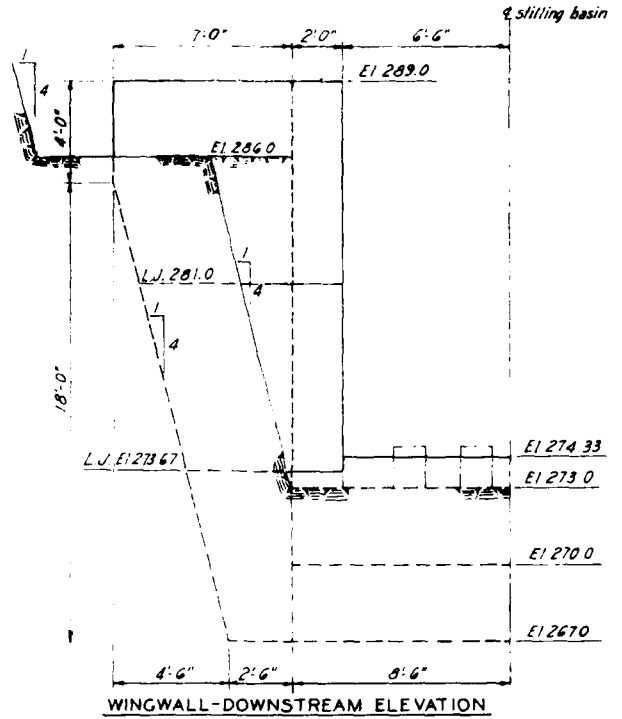
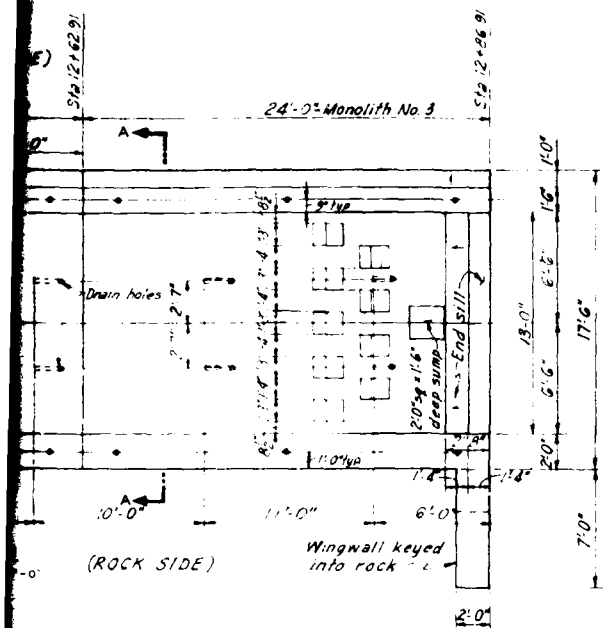
REVISION	DATE	DESCRIPTION	BY
VI-1-79		Revised upstream slopes of intake structure	LLB
Amend No. 0001			
DEPARTMENT OF THE ARMY LITTLE ROCK DISTRICT, CORPS OF ENGINEERS LITTLE ROCK, ARKANSAS			
DESIGNED BY	ARANSAS RIVER AND TRIBUTARIES	ARANSAS RIVER, ARKANSAS	
DRAWN BY	TOAD SUCK FERRY LOCK AND DAM RELOCATIONS		
CHECKED BY	CONWAY WATER SUPPLY OUTLET WORKS		
QUANTITY BY	PLAN, PROFILE AND TYPICAL SECTION		
DATE	AUGUST 1979		
PROJECT	SCALE AS SHOWN		
	9570-62/1359		

INC'L 1

AMEND NO 006

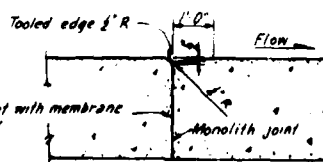
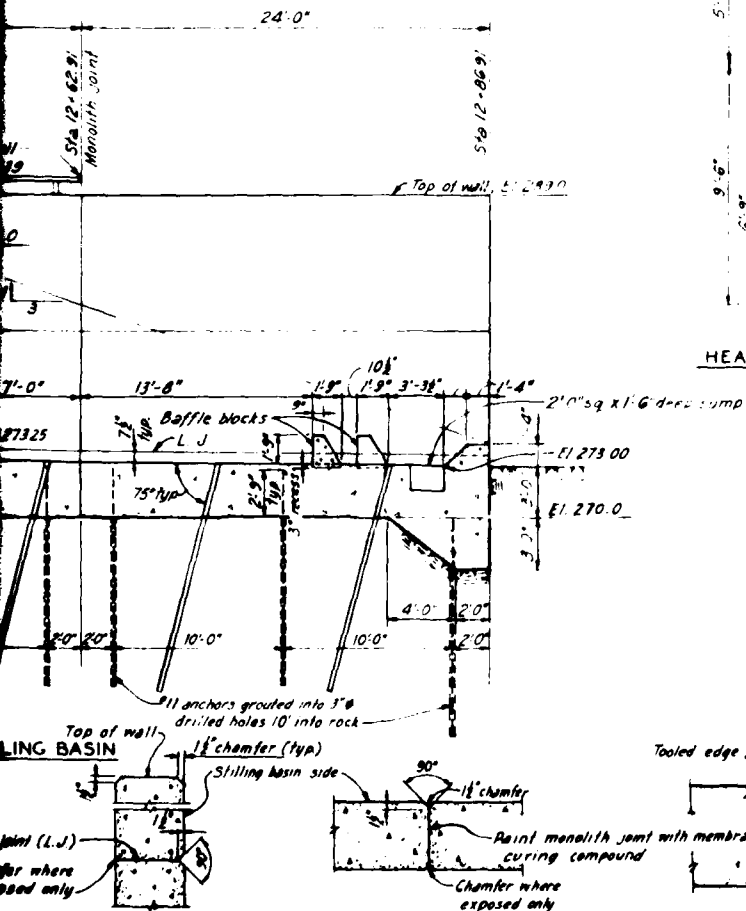


WORK SAFELY



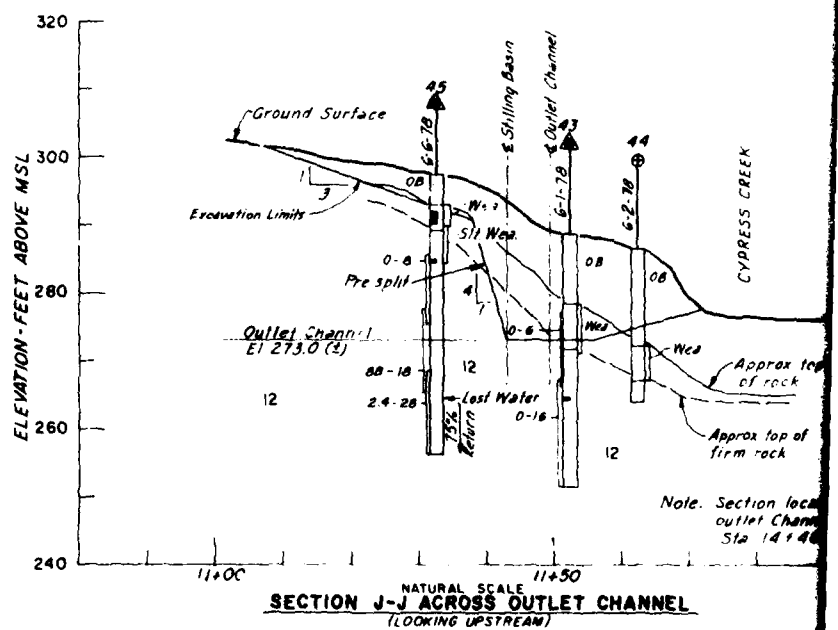
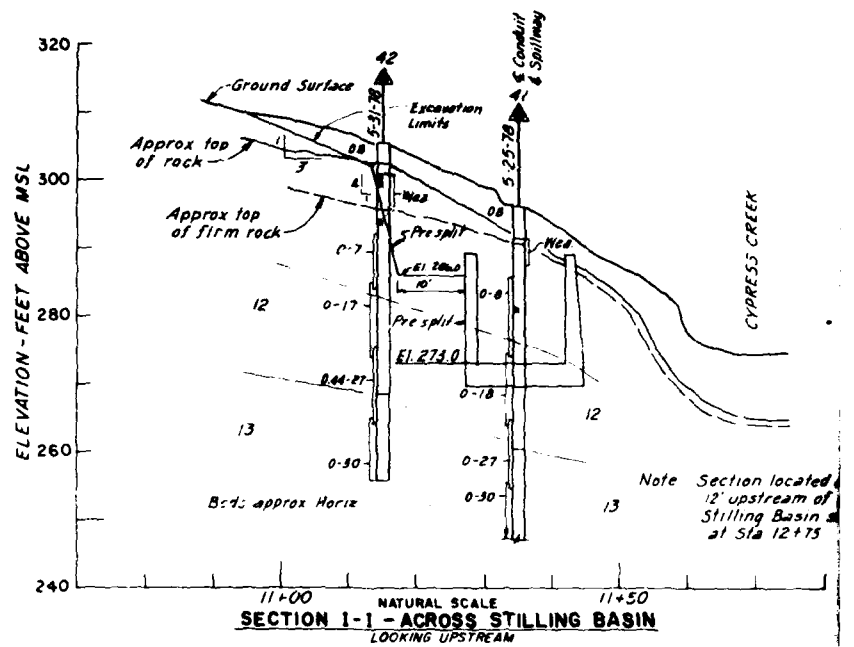
NOTES.

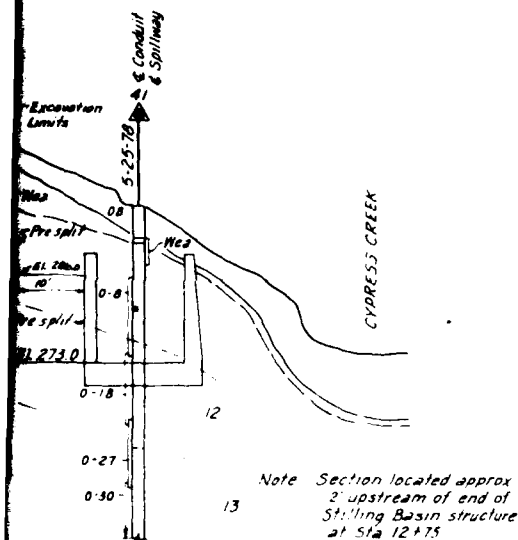
- 1 Concrete for slab, end sill, and baffle blocks to have a 28 day compressive strength of 4,000 p.s.i.
- 2 Concrete for walls, headwall, and wingwall to have a 28 day compressive strength of 3,000 p.s.i.
- 3 For water stop details see dwg. 1433
- 4 The last few inches of rock excavation adjacent to concrete pours shall be removed during clean up operations just prior to concrete placement
- 5 Sections A-A, B-B, C-C and D-D appear on drawing 1436.



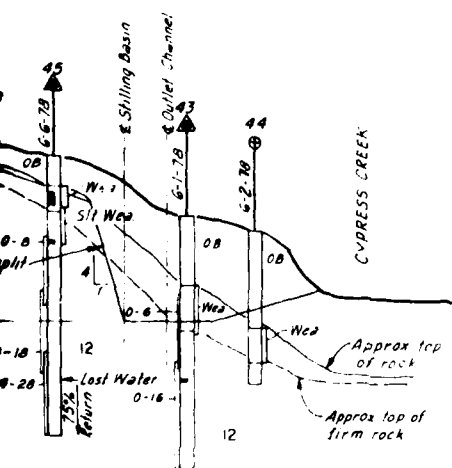
**TYPICAL SLAB MONOLITH JOINT**  
SCALE NONE

REVISION	DATE	DESCRIPTION	BY
DEPARTMENT OF THE ARMY LITTLE ROCK DISTRICT, CORPS OF ENGINEERS LITTLE ROCK, ARKANSAS			
DESIGNED BY	ARKANSAS RIVER AND TRIBUTARIES		ARKANSAS RIVER, ARKANSAS
AJP	TOAD SUCK FERRY LOCK AND DAM RELOCATIONS CONWAY WATER SUPPLY OUTLET WORKS-STILLING BASIN PLAN, ELEVATION AND SECTIONS		
DRAWN BY			
JED			
CHECKED BY			
AJP			
SUBMITTED BY	SCALE AS SHOWN	AUGUST 1979	
<i>Frank Smith</i>		BY SERIAL NO. 60-2-OF	
NUMBER	9570-627/435		





NATURAL SCALE  
I-I ACROSS STILLING BASIN  
(LOOKING UPSTREAM)



NATURAL SCALE  
J-J ACROSS OUTLET CHANNEL  
(LOOKING UPSTREAM)

GENERALIZED GEOLOGIC COLUMN			
SYSTEM	FORMATION	SECTION	THICKNESS IN FEET
PENNSYLVANIAN	ATOKA	7	10
		10	50
		14	11
		17	11
		13	12
		16	12
		11	13
		12	13
		5	14
		20	14
MISSISSIPPIAN	OSAGE	7	15
		10	15
		37	16

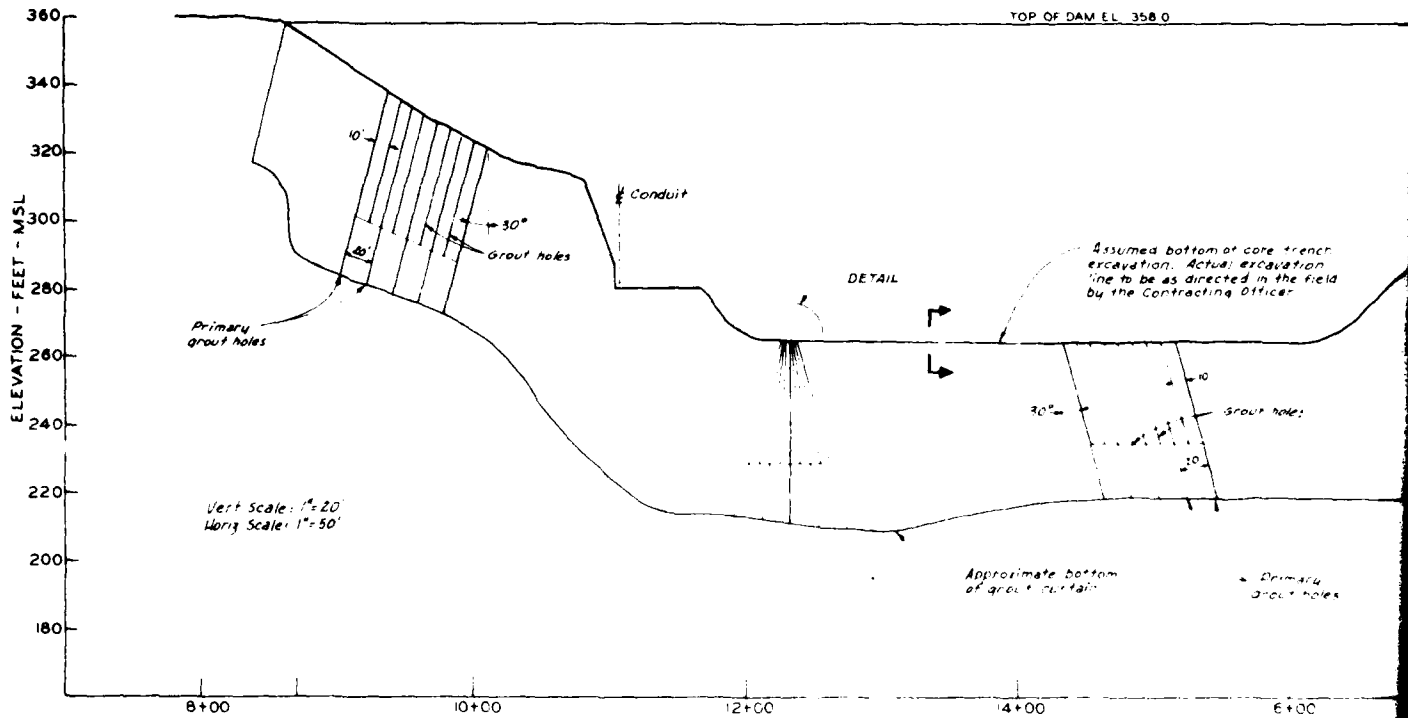
# LEGEND

- NX CORE BORING
- △ SOILS BORING
- ▲ COMBINATION NX CORE & SOILS BORING
- ▲ COMBINATION SOILS & FISHTAILED BORING
- FISHTAILED BORING
- PIEZOMETER
- 4-18-70 DATE DRILLED
- W.L. WATER LEVEL
- 136-20 PRESSURE TEST: 136 CFM @ 20 PSI
- 15 ROCK UNIT
- CORE LOSS
- TEST PIT

# NOTES:

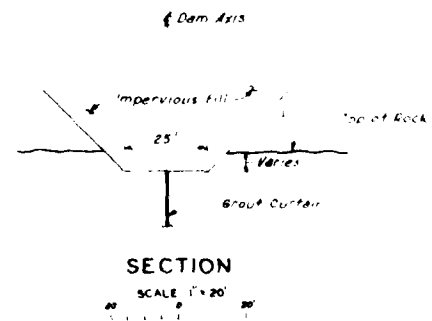
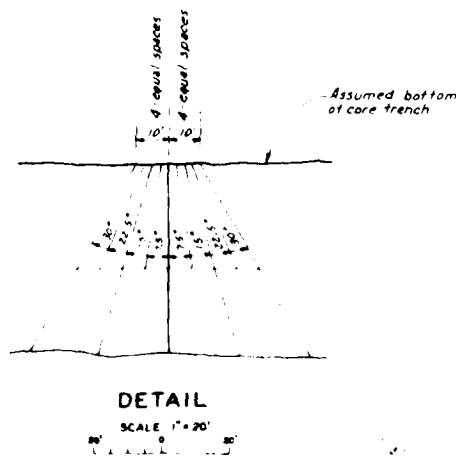
- 1 For general notes see Drawing 62/1477
- 2 For location of Section see Drawing 62/1477
- 3 For detailed information of Borings, Pressure Tests, Core Loss, weathering, fractures, joints, see Boring Logs, Contract Specs.
- 4 For overburden information see Soils Logs, Contract Specs.

REVISION	DATE	DESCRIPTION	BY
<p>DEPARTMENT OF THE ARMY LITTLE ROCK DISTRICT, CORPS OF ENGINEERS LITTLE ROCK, ARKANSAS</p> <p>DESIGNED BY: JMB DRAWN BY: JMB CHECKED BY: RRF SUBMITTED BY: <i>Robert D. Lutz</i> ENGINEER</p> <p>ARANSAS RIVER AND TRIBUTARIES TOAD SUCK FERRY LOCK AND DAM RELOCATIONS CONWAY WATER SUPPLY GEOLOGIC SECTIONS ACROSS STILLING BASIN, SECTIONS I-I &amp; J-J</p> <p>SCALE AS SHOWN AUGUST 1979 BY SERIAL NO. 8-0001</p> <p>9570-62/1482</p>			



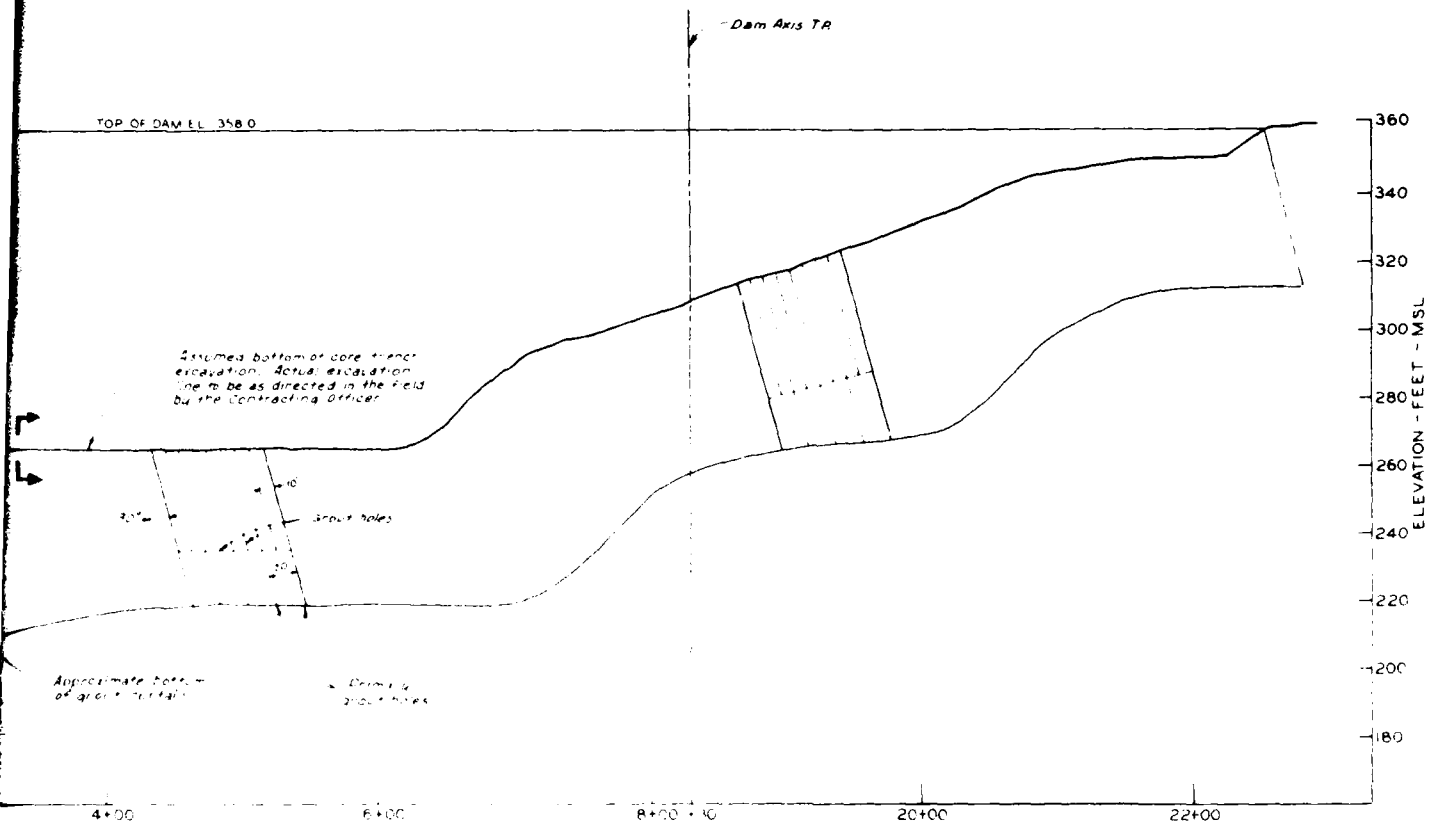
# SECTION ALONG LINE OF GROUT CURTAIN

(LOOKING UPSTREAM)  
SCALE AS SHOWN

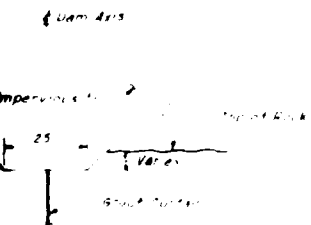


NOT

WORK SAFELY



SECTION ALONG LINE OF GROUT CURTAIN  
(LOOKING UPSTREAM)  
SCALE AS SHOWN

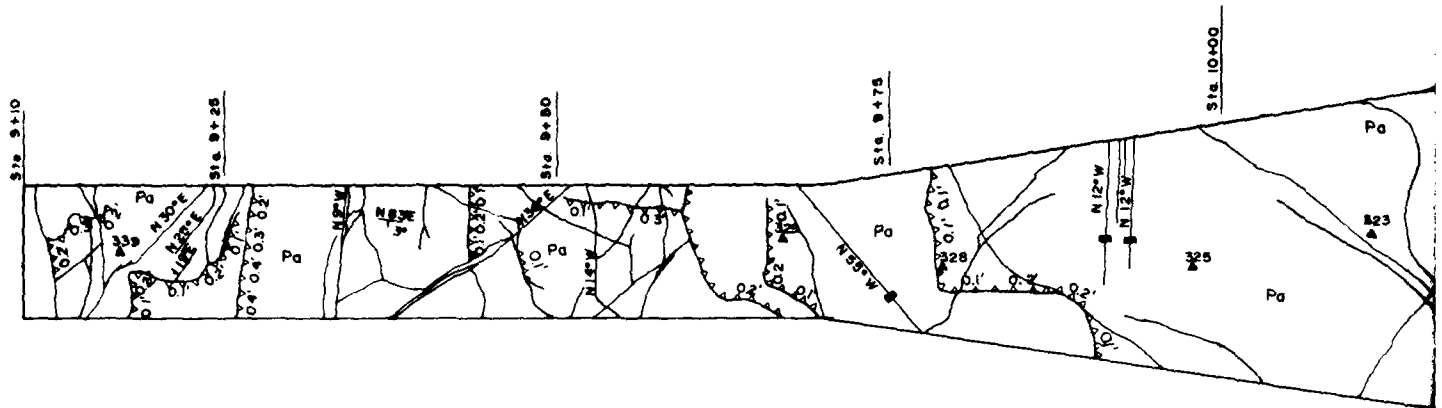


NOTES:

1. All grout holes to be drilled from top of rock (excavation grade) through holes grouted into top of rock or as otherwise directed by the Contracting Officer. Lengths, spacing, pressure testing and grouting will be as directed by the Contracting Officer.

SECTION  
SCALE 1" = 20'

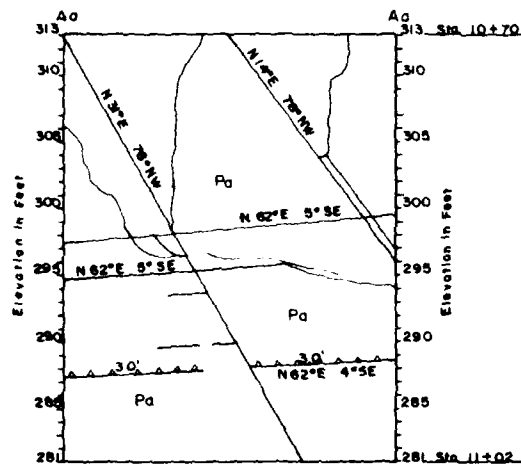
DESIGNED BY JMB	ARCHITECT JMB	ENGINEER JMB	DATE AUGUST 1978
<p>DEPARTMENT OF THE ARMY LITTLE ROCK DISTRICT CORPS OF ENGINEERS LITTLE ROCK ARKANSAS</p> <p>ARKANSAS RIVER &amp; TRIBUTARIES ARKANSAS RIVER ARKANSAS</p> <p>TOAD SUCK FERRY LOCK AND DAM RELOCATIONS CONWAY WATER SUPPLY FOUNDATION TREATMENT</p>			
<p>ENGINEER JMB</p>			<p>NO. 9570-62/1487</p>



**PLAN**

Scale: 1" = 5'

54321Q12345



**GEOLOGIC SECTION Aa-Aa**

Scale: 1" = 5'

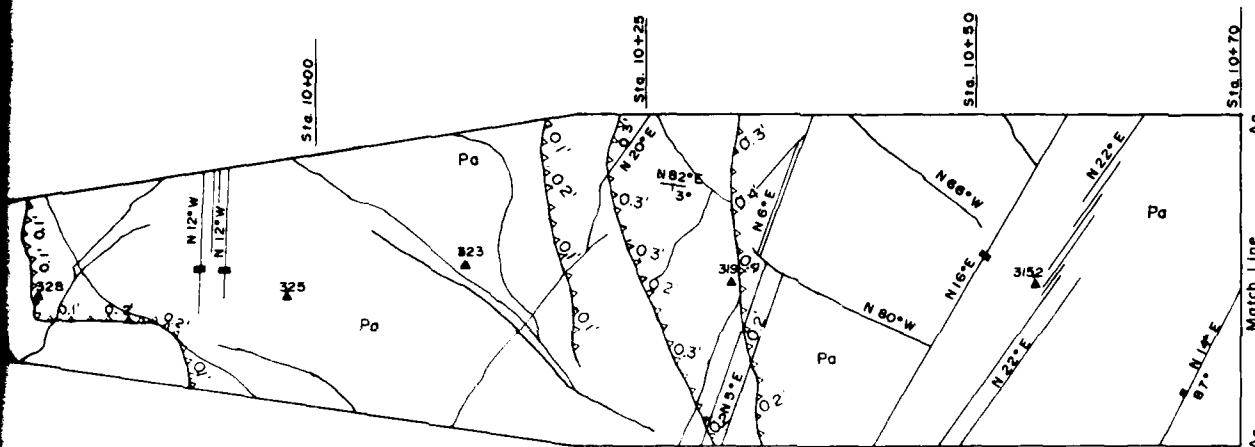
54321Q12345

**EXPLANATION**

- N 12° E 87° Joint, showing where approx
- Fracture, irregular strike and dip
- 0.3' 0.4' 0.2' Rock Ledges, ledge, number
- ▲ 539 Elevation (measured by triangle)
- Pa Atoka Formation, moderately well compacted, the shale weathers to occasional firm. At 3.5' thick, reddish tan
- Joint, vertical

**WORK SAFELY**





# PLAN

Scale: 1" = 5'

5 4 3 2 1 0 1 2 3 4 5

## EXPLANATION

- Joint, showing strike and dip, dashed where approximate or unclear when mapped.
- Fracture, irregular without distinct strike and dip.
- Rock Ledge, with barbs on face of ledge, numerical thickness shown in feet.
- Elevation, (m.s.l.) at point marked by triangle.
- Pa** Atoka Formation, shale, sandy, hard to moderately hard, gray to dark gray, black, well compacted and cemented, micaceous. From stations 9+10 to 9+70 and from 20+28 to 20+58.2 the shale was somewhat weathered, gray to buff to occasionally reddish brown, and moderately soft to firm. At station 20+58.2 there was sandstone 3.5± thick, fine grained, hard, and gray, with reddish tan staining. (Pennsylvanian Period)
- Joint, vertical dip.

## REFERENCE DRAWINGS

Embankment Plan 9570-62/1351  
 Typical Embankment Section 9570-62/1364  
 Geologic Sections A-A & B-B 9570-62/1479

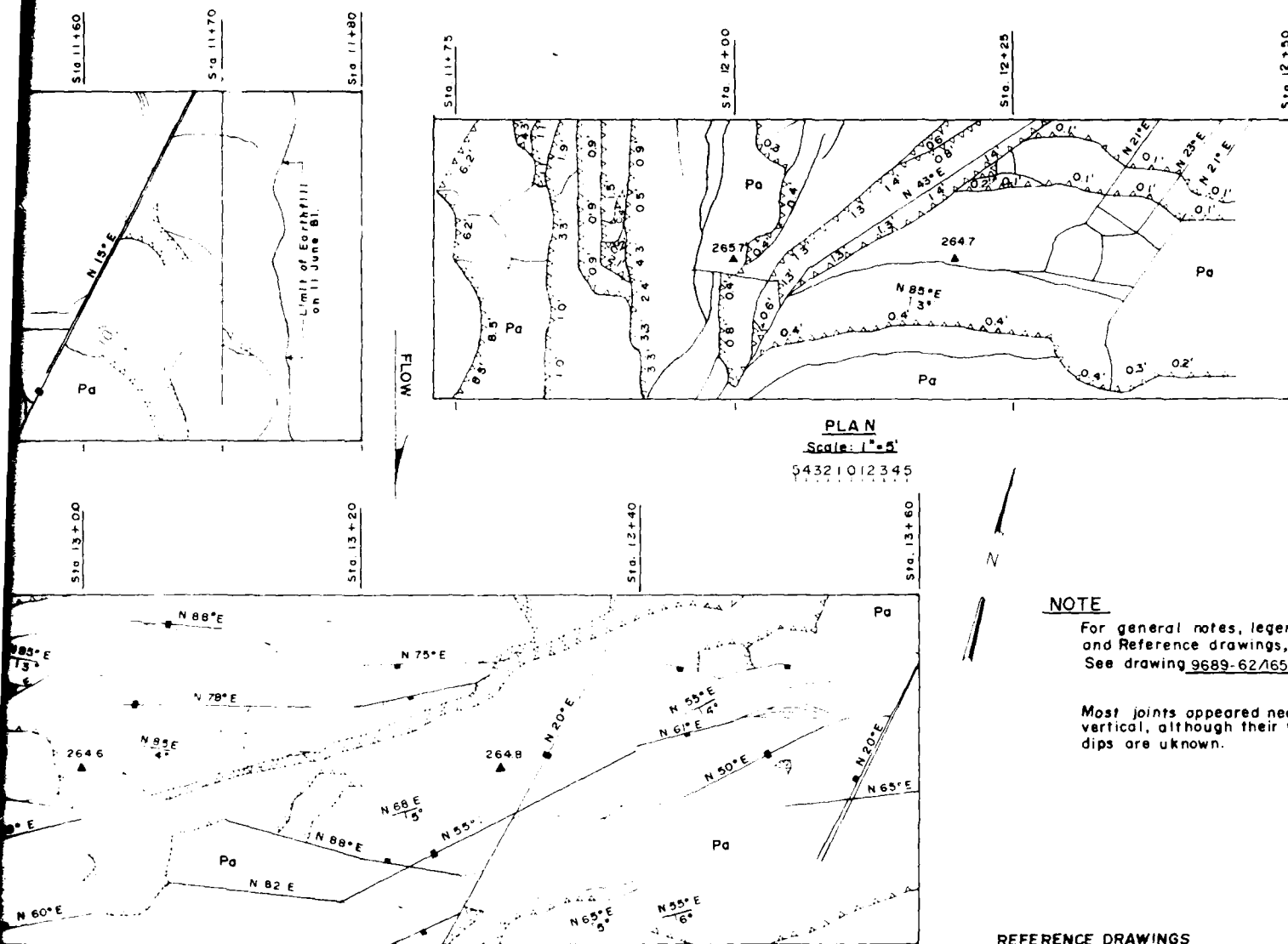
DESIGNED BY RC	DATE	DESCRIPTION DEPARTMENT OF THE ARMY LITTLE ROCK DISTRICT, CORPS OF ENGINEERS LITTLE ROCK, ARKANSAS
DRAWN BY CH		ARKANSAS RIVER AND TRIBUTARIES
CHECKED BY CD		TOADSUCK FERRY LOCK AND DAM RELOCATIONS CONWAY WATER SUPPLY DAM AXIS-CORE TRENCH STA 9+10 TO STA 11+02
SUBMITTED BY		APRIL 1983
ENGINEER		9689-62/1659

**PLAN**

**Scale: 1"=4'**

432101234

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PLAN  
Scale: 1"=5'

54321012345

#### NOTE

For general notes, legend,  
and Reference drawings,  
See drawing 9689-62/1659

Most joints appeared nearly  
vertical, although their true  
dips are unknown.

#### REFERENCE DRAWINGS

Embankment Plan 9570-62/1351  
Typical Embankment Section 9570-62/1364  
Geologic Sections A-A and B-B 9570-62/1479

#### PLAN

Scale: 1"=4'

5432101234

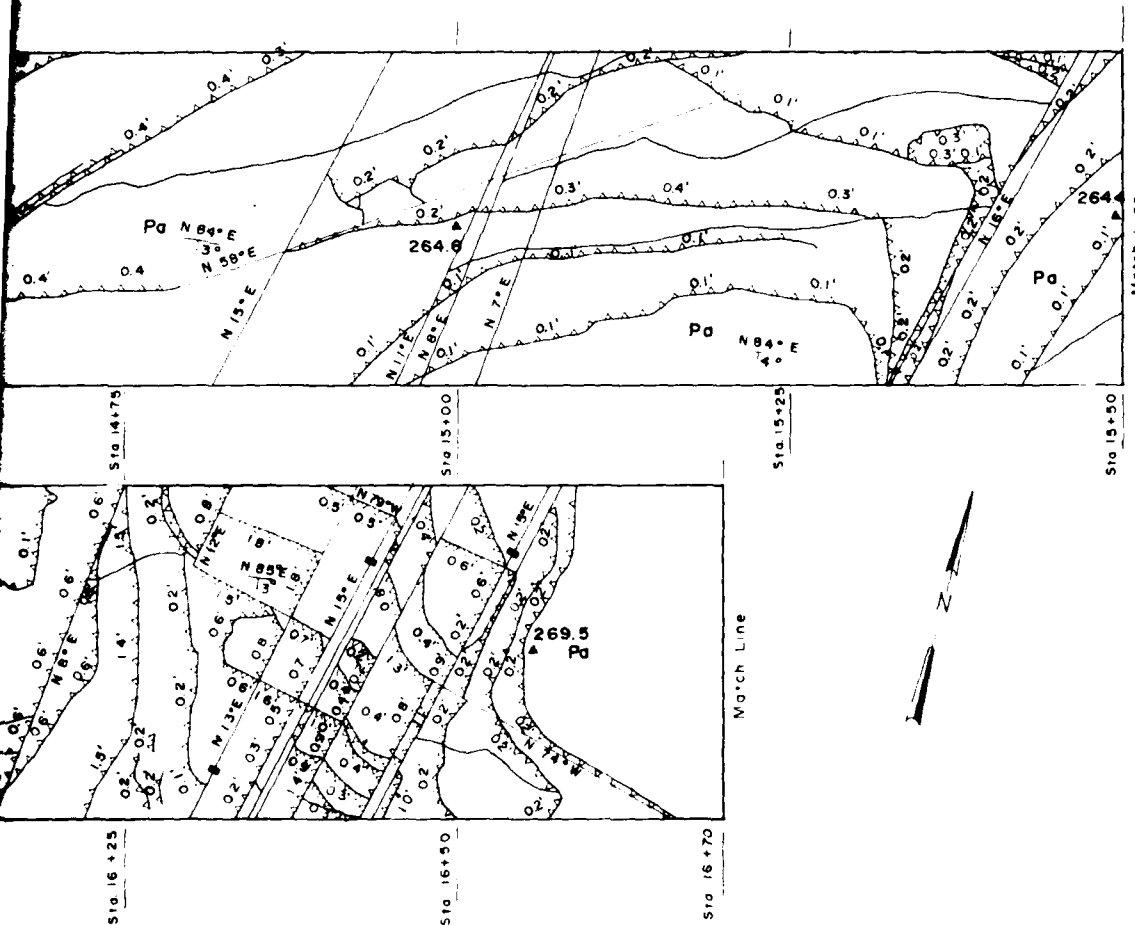
DESIGNED BY	RC	DEPARTMENT OF THE ARMY LITTLE ROCK DISTRICT CORPS OF ENGINEERS LITTLE ROCK, ARKANSAS
DRAWN BY	CH	ARKANSAS RIVER AND TRIBUTARIES ARKANSAS RIVER, ARKANSAS
CHECKED BY	CD	TOAD SUCK FERRY LOCK AND DAM RELOCATIONS CONWAY WATER SUPPLY DAM AXIS-CORE TRENCH STA 11+10 TO STA 13+60
SUBMITTED BY		APRIL 1983 BY SERIAL NO. 67 R 0001
ENGINEER		9689-62/1660 SHEET 14 OF 24

\_\_\_\_\_

FLOW

**NOTE**

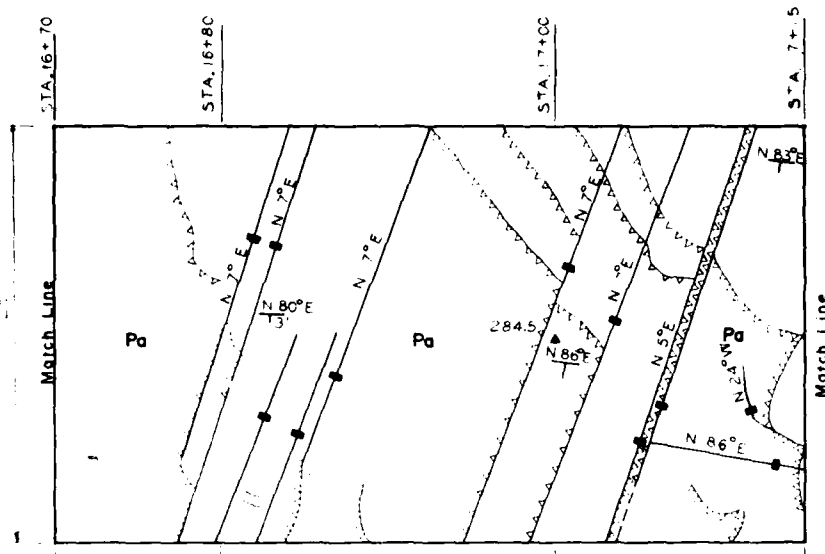
For general notes, legend,  
and reference drawings,  
see drawing 9689-62/1659



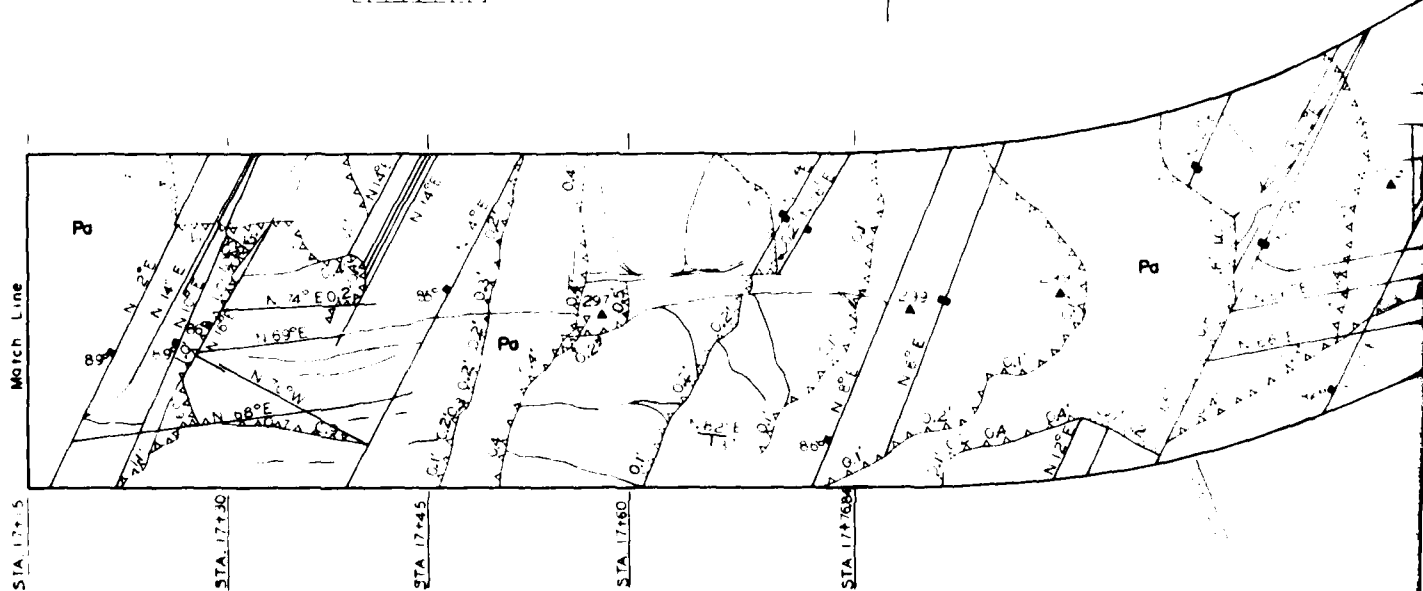
**REFERENCE DRAWINGS**

Embankment Plan 9570-62/135  
Typical Embankment Section 9570-62/1364  
Geologic Sections A A B B-B 9570-62/1479

DEPARTMENT OF THE ARMY LITTLE ROCK DISTRICT CORPS OF ENGINEERS LITTLE ROCK, ARKANSAS	
DESIGNED BY <b>RC</b>	ADJ. ARKANSAS RIVER AND TERRITORIES ARKANSAS RIVER, ARKANSAS
DRAWN BY <b>CH</b>	<b>TOAD SUCK FERRY LOCK AND DAM</b>
CHECKED BY <b>CD</b>	<b>RELOCATIONS</b>
SUBMITTED BY	<b>CONWAY WATER SUPPLY</b>
ENGINEER	<b>DAM AXIS-CORE TRENCH</b>
DATE	<b>STA 13+60 TO STA 16+70</b>
APRIL 1983	DRAWING NUMBER <b>9689-62/1661</b>
SHEET 15	OF 24

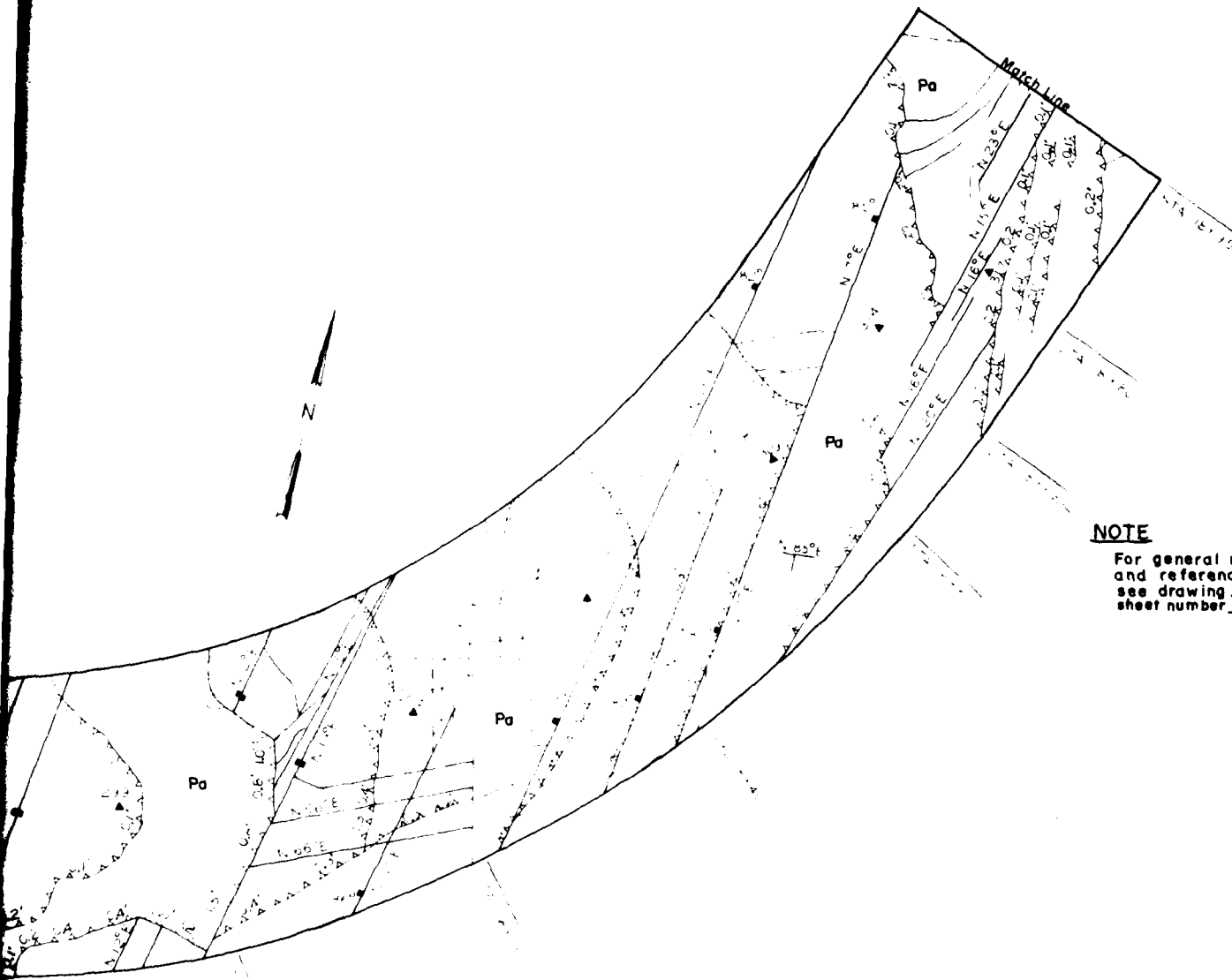


PLAN  
SCALE 1" = 40'



PLAN  
SCALE 1" = 40'

WORK SAFELY



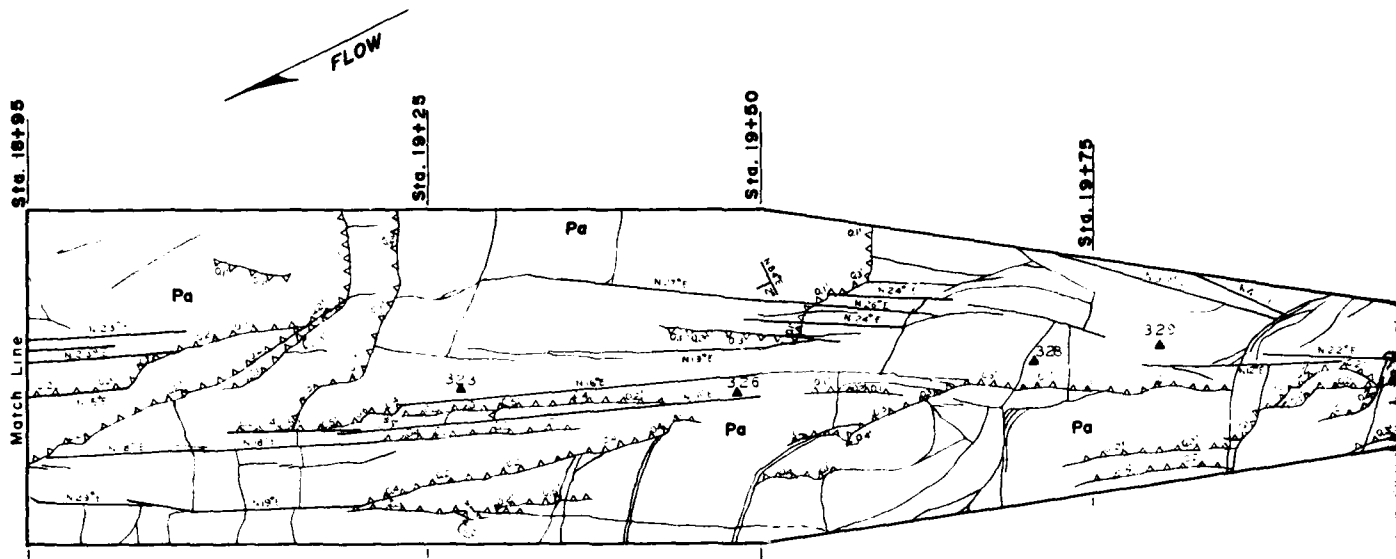
**NOTE**

For general notes, explanation,  
and reference drawings,  
see drawing 9689-62/1659,  
sheet number 13

**REFERENCE DRAWINGS**

Embankment Plan 9570-62/1351  
Typical Embankment Section 9570-62/1364  
Geological Sections A-A & B-B 9570-62/1479

REVISION	DATE	DESCRIPTION	BY
DEPARTMENT OF THE ARMY LITTLE ROCK DISTRICT, CORPS OF ENGINEERS LITTLE ROCK, ARKANSAS			
DESIGNED BY	ARIZONA RIVER AND TRIBUTARIES	ARIZONA RIVER, ARIZONA	
RC	TOAD SUCK FERRY LOCK AND DAM		
DRAWN BY	RELOCATIONS		
CH	CONWAY WATER SUPPLY		
CHECKED BY	DAM AXIS-CORE TRENCH		
CD	STA 16+70 TO STA. 18+95		
SUBMITTED BY			APRIL 1983
ENGINEER	9689-62/1662		BY SERIAL NO. 80 8 0002



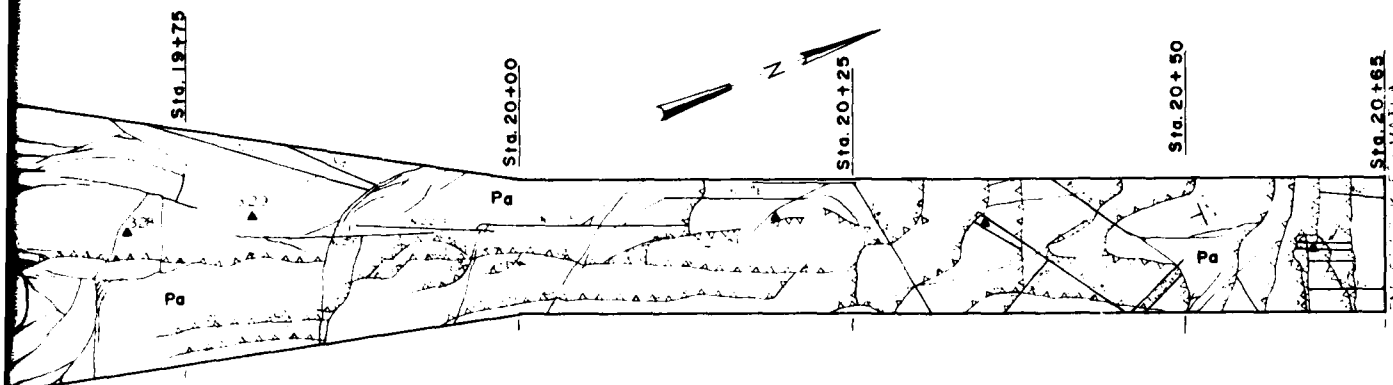
PLAN

Scale: 1" = 5'

5432 1 0 12 345

WORK SAFELY





PLAN

Scale: 1" = 5'

543210 2345

NOTE

For general notes, explanation,  
and reference drawings, see  
drawing 9689-62/1659  
sheet number 13

REFERENCE DRAWINGS

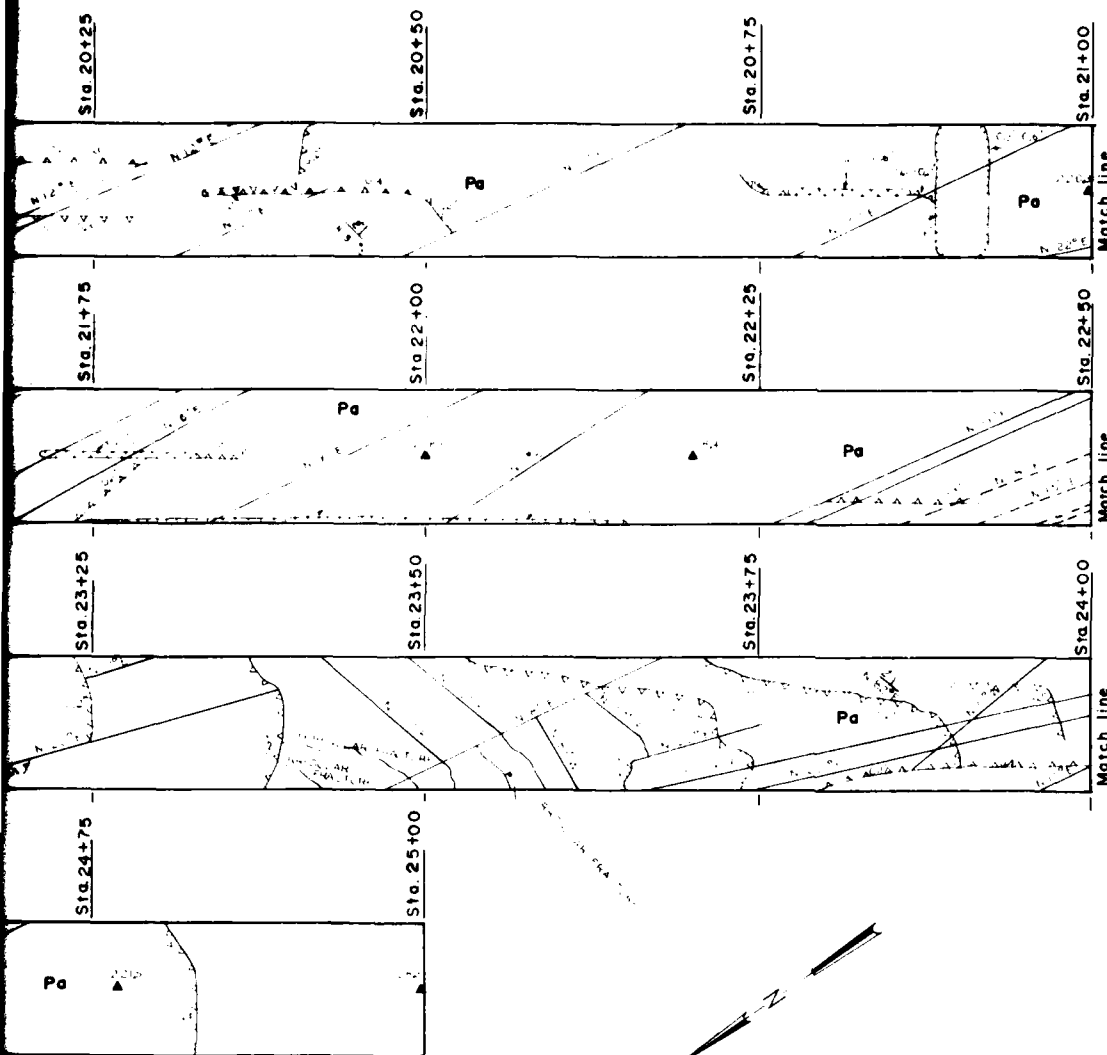
Embankment Plan	9570-62/1351
Typical Embankment Section	9570-62/1364
Geologic Sections A-A & B-B	9570-62/1479

REVISION	DATE	DESCRIPTION	BY
DEPARTMENT OF THE ARMY LITTLE ROCK DISTRICT, CORPS OF ENGINEERS LITTLE ROCK, ARKANSAS			
DESIGNED BY	ARKANSAS RIVER AND TRIBUTARIES	ARKANSAS RIVER, ARKANSAS	
RC	TOAD SUCK FERRY LOCK AND DAM		
DRAWN BY	RELOCATIONS		
CH	CONWAY WATER SUPPLY		
CHECKED BY	DAM AXIS-CORE TRENCH		
CD	STA 18+95 TO STA 20+65		
SUBMITTED BY			APRIL 1983
ENGINEER			BY SERIAL NO. 80-B-0001
9689-62/663			SHEET 17 OF 24

Geological cross-section of the Paoli Formation in the Mt. Vernon area. The section is divided into several segments with stationing labels on both sides. Key features include:

- Sta. 19+50:** BEGINNING OF FIRM ROCK. Stationing labels: Sta. 19+50, Sta. 19+75, Sta. 20+00, Sta. 20+25, Sta. 20+50.
- Sta. 20+25:** N 12° E fault. Stationing labels: Sta. 20+25, Sta. 21+00, Sta. 21+25, Sta. 21+50, Sta. 21+75, Sta. 22+00.
- Sta. 21+75:** IRREGULAR FRACTURE. Stationing labels: Sta. 21+75, Sta. 22+00, Sta. 22+25, Sta. 22+50, Sta. 22+75, Sta. 23+00.
- Sta. 22+75:** Stationing labels: Sta. 22+75, Sta. 23+00, Sta. 23+25, Sta. 23+50, Sta. 23+75, Sta. 24+00.
- Sta. 23+75:** Stationing labels: Sta. 23+75, Sta. 24+00, Sta. 24+25, Sta. 24+50, Sta. 24+75, Sta. 25+00.
- Sta. 24+75:** Stationing labels: Sta. 24+75, Sta. 25+00.

The cross-section shows various geological features, including faults, fractures, and different rock units labeled 'Pa'. The section is oriented with 'Match line' labels on the left and right sides.



**PLAN**

Scale: 1" = 5'

5432 012345

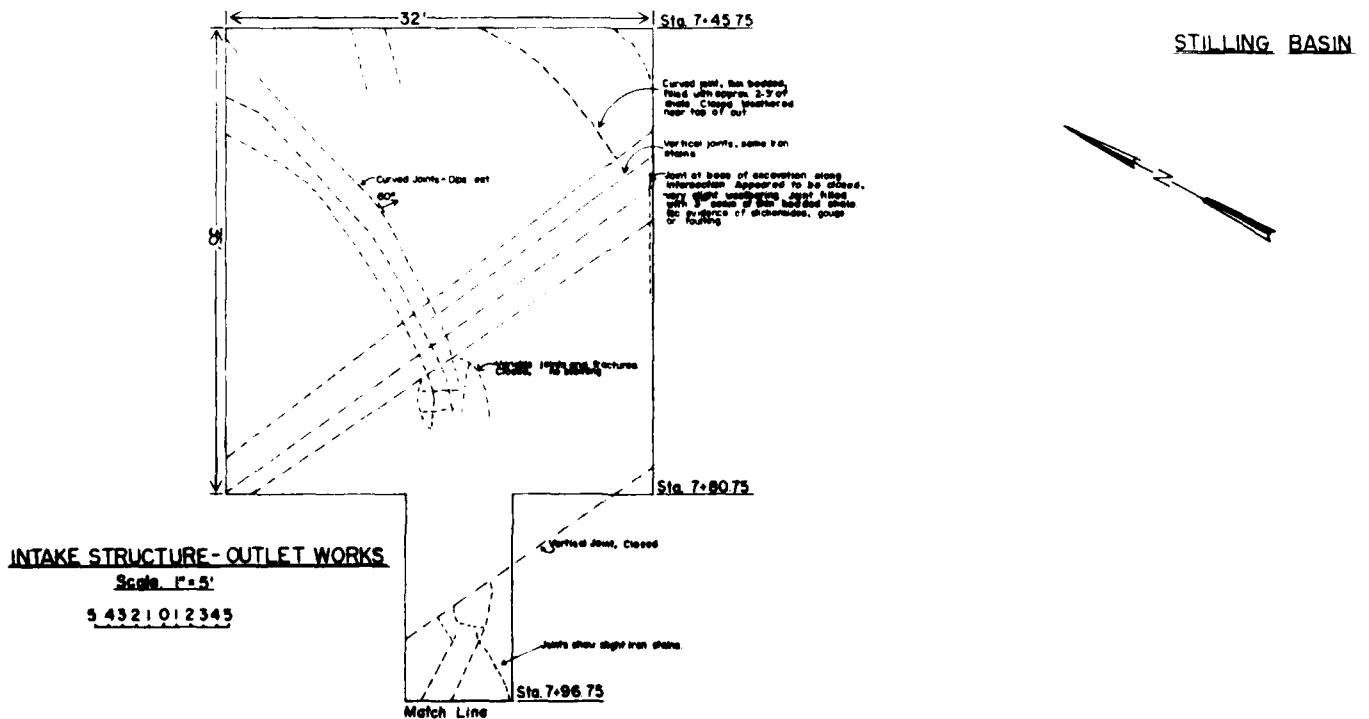
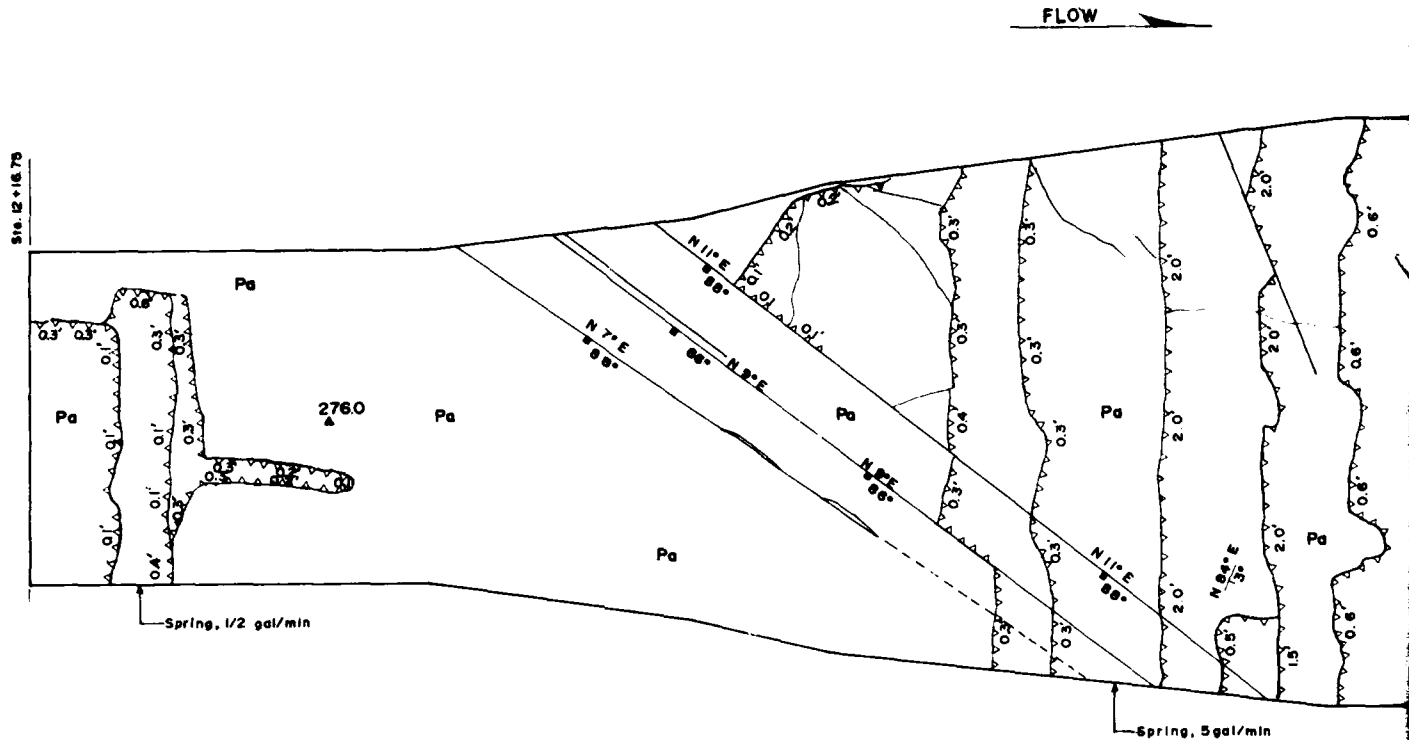
**EXPLANATION**

- Joint**, showing direction of strike, dashed, where approximate or unclear when mapped.
- IRREGULAR FRA.** **Fracture**, mostly tight and irregular.
- ROCK LEDGE** **Rock Ledge**, with barbs on face of ledge; numerical thickness shown in feet.
- ENCLOS. DEP. OR TRENCH** **Enclosed Depression or Trench**, with barbs toward center of depression; numerical depth shown in feet.
- Pa** **Atoka Formation**, shale, sandy, hard to moderately hard, gray to dark gray compacted and cemented, with occasional shaly sandstone lenses.
- ELEVATION**, in feet, msl.

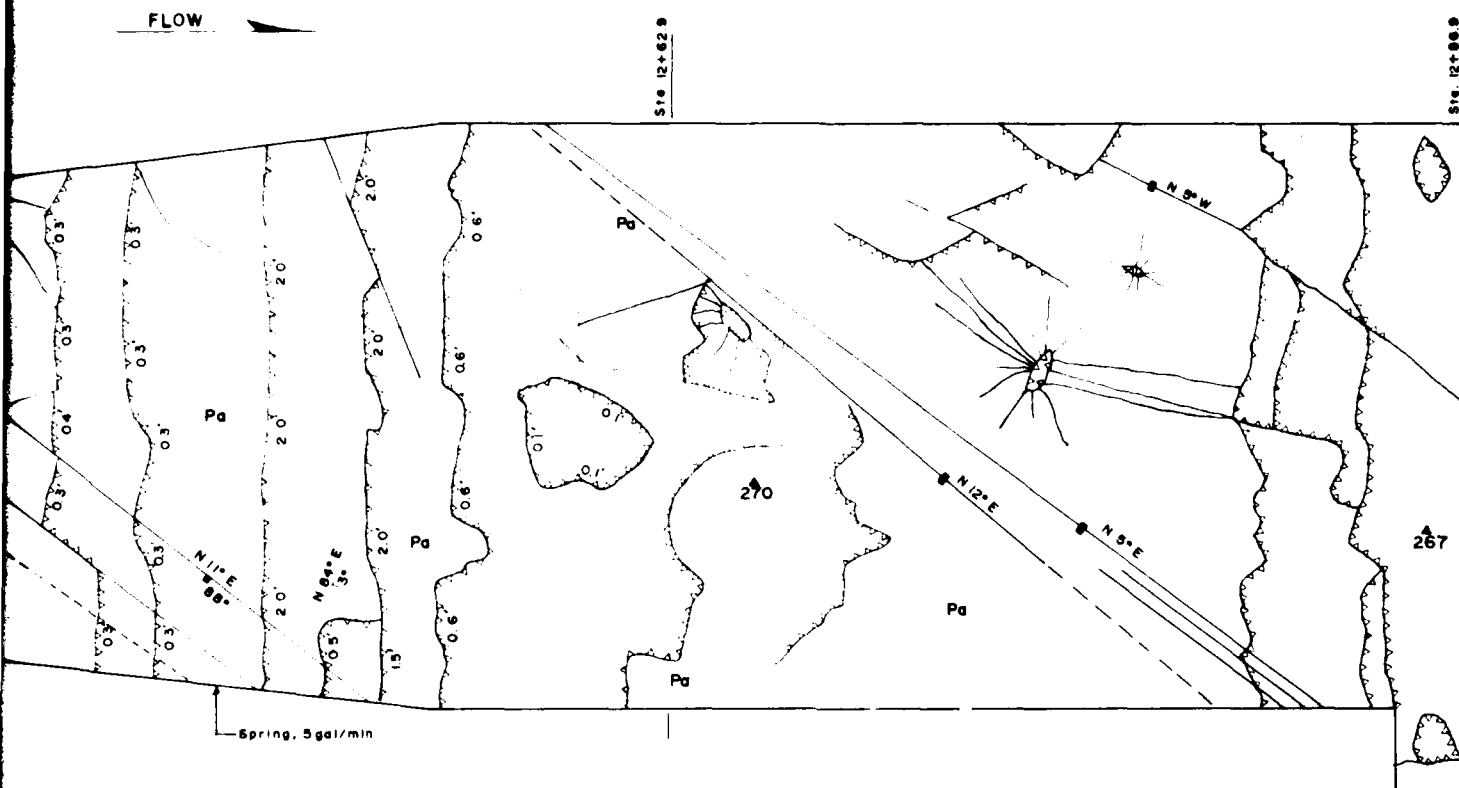
**REFERENCE DRAWINGS**

- Dike, plan, profile and typical section. 9570-62/1372
- Geologic section along  $\bar{L}$  of dike. 9570-62/1486

REVISION	DATE	DESCRIPTION	BY
DEPARTMENT OF THE ARMY LITTLE ROCK DISTRICT CORPS OF ENGINEERS LITTLE ROCK, ARKANSAS			
DESIGNED BY	ARKANSAS RIVER AND TRIBUTARIES		ARKANSAS RIVER, ARKANSAS
RC	TOAD SUCK FERRY LOCK AND DAM		
DRAWN BY	RELOCATIONS		
CH	CONWAY WATER SUPPLY		
CHECKED BY	DIKE-CORE TRENCH		
CD	STA. 19+50 TO STA. 25+00		
SUBMITTED BY			APRIL 1983
ENGINEER			REV. SERIAL NO. 80-8-0001
		9689-62/1664	
		SHEET 18 OF 24	



WORK SAFELY



# STILLING BASIN

## EXPLANATION

N 9° E  
86°

Joint, showing strike and dip,  
dashed where approximate or  
unclear when mapped.

2.0' 2.0'

Fracture, irregular without  
distinct strike and dip.

Pa

Rock Ledges, with barbs on face  
of ledge, numerical thickness  
shown in ft.

Atoka Formation, shale,  
sandy, hard to moderately hard,  
gray to dark gray, well compacted  
and cemented micaceous.

270

Elevation, (m.s.l.)

Joint, vertical dip

## PLAN

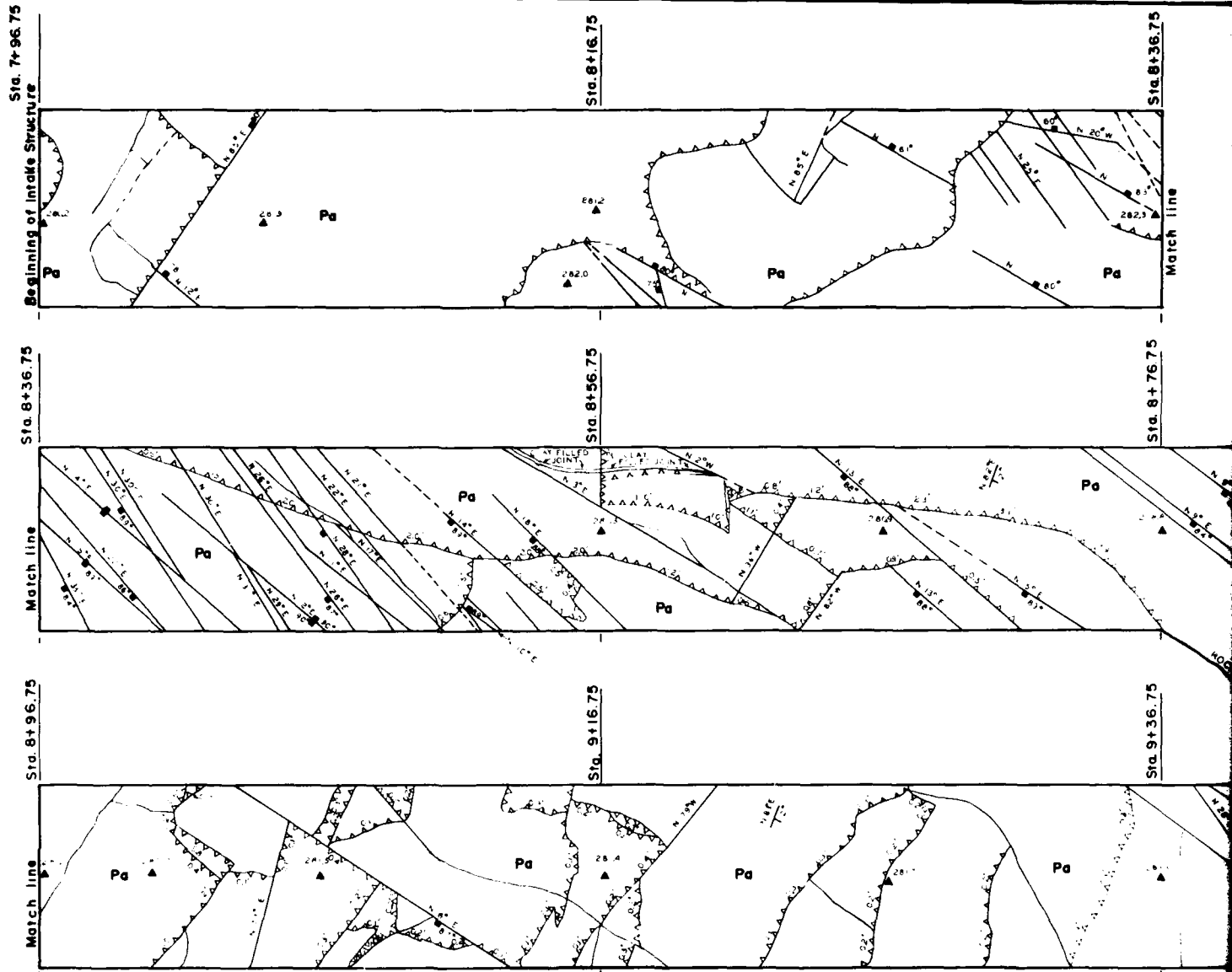
Scale 1" = 2'

2 1 0 1 2

## REFERENCE DRAWINGS

Outlet works  
Plan, Profile, and Typical Section 9570-62/1359  
Outlet Works-Stilling Basin  
Plan, Elevation, and Sections 9570-62/1435  
Geologic Sections Across  
Stilling Basin, I-I, J-J 9570-62/1482

REVISION	DATE	DESCRIPTION	BY
DEPARTMENT OF THE ARMY LITTLE ROCK DISTRICT, CORPS OF ENGINEERS LITTLE ROCK, ARKANSAS			
DESIGNED BY	ARKANSAS RIVER AND TRIBUTARIES		
RC	ARKANSAS RIVER, ARKANSAS		
DRAWN BY	TOADSUCK FERRY LOCK AND DAM		
CH	RELOCATIONS		
CHECKED BY	CONWAY WATER SUPPLY		
CD	OUTLET WORKS-STILLING BASIN		
SUBMITTED BY			APRIL 1983
DRAWING NUMBER			9689-62/1665
SHEET 18			OF 20



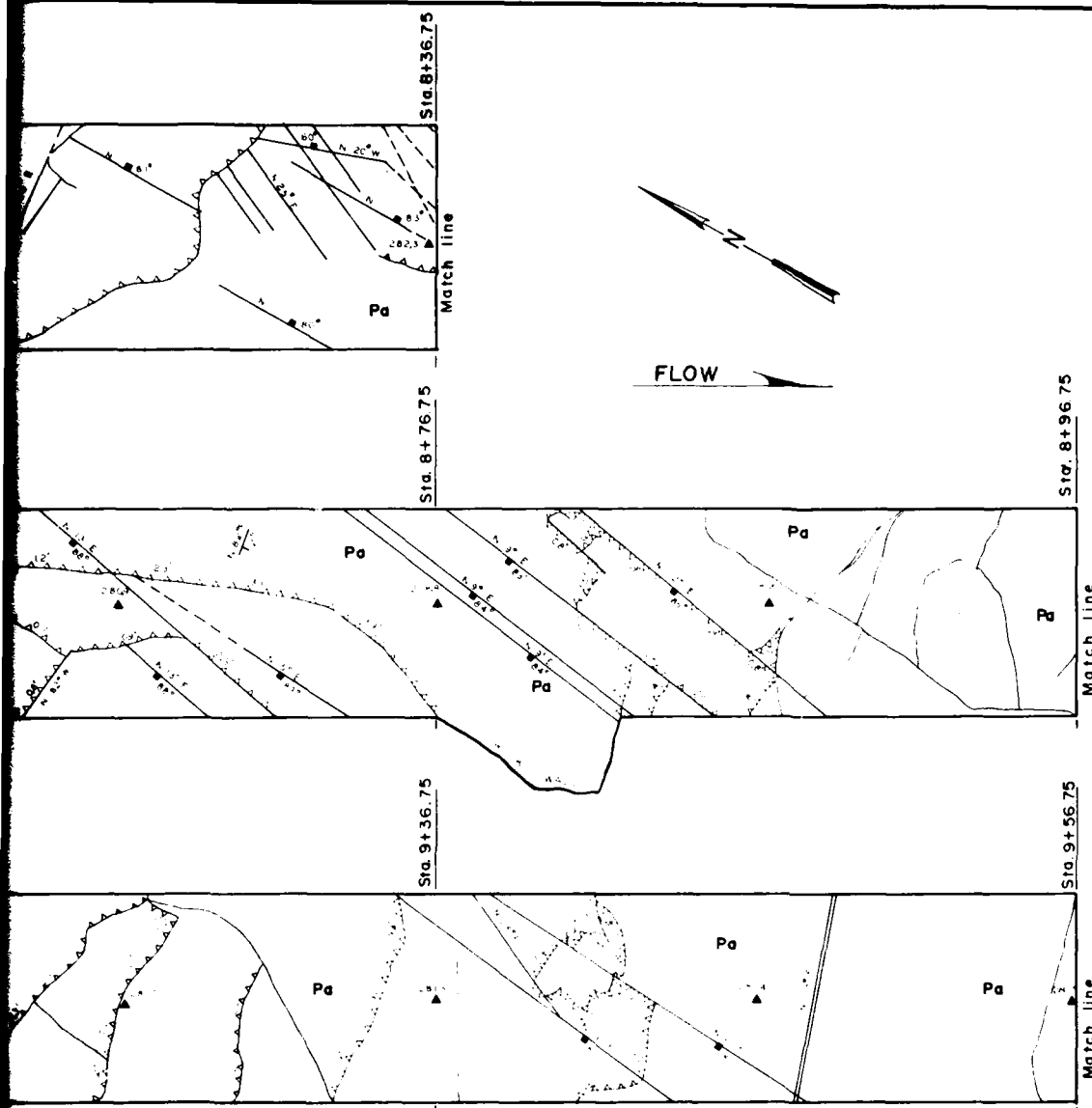
PLAN

Scale: 1" = 2'

2 1 0 1 2

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# EXPLANATION

- Joint, showing strike and dip dashed where approximate or unclear when mapped.
- Fracture, irregular, without distinct strike and dip.
- Rock Ledge, with barbs on face of ledge; numerical thickness shown in feet.
- Pa Atoka Formation, shale, sandy, hard to moderately hard gray to dark gray, well compacted and cemented, calcareous
- Elevation, in m.s.l.
- Blast Hole, remnant pre-splitting shows radiating fractures.

## REFERENCE DRAWINGS

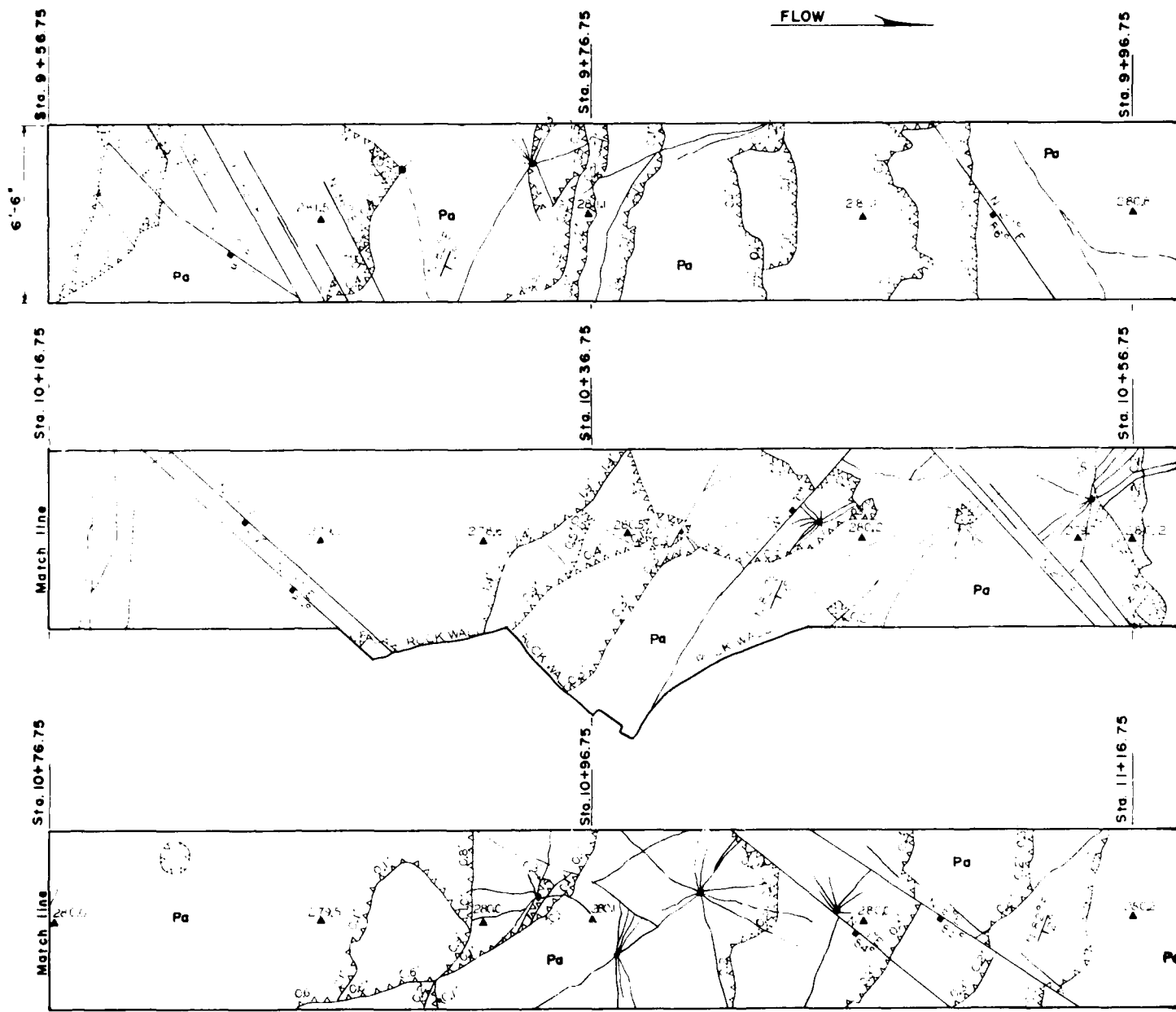
Concrete and Reinforcing 9570-62/1433  
Geologic Sections 9570-62/1481

## PLAN

Scale: 1" = 2'

2 1 0 1 2

REVISION	DATE	DESCRIPTION
DEPARTMENT OF THE ARMY LITTLE ROCK DISTRICT, CORPS OF ENGINEERS LITTLE ROCK, ARKANSAS		
DESIGNED BY	RC	ARKANSAS RIVER AND TRIBUTARIES
DRAWN BY	CH	ARKANSAS RIVER, ARKANSAS
CHECKED BY	CD	
SUBMITTED BY		
TOAD SUCK FERRY LOCK AND DAM RELOCATIONS CONWAY WATER SUPPLY OUTLET WORKS - CONDUIT STA. 7+96.75 TO STA. 9+56.75		APRIL 1983 HW SERIAL NO. 87-8 0001
DRAWING NUMBER 9689-62/1666		SHEET 20 OF 24



## WORK SAFELY



FLOW

Sta. 9+96.75

Sta. 10+16.75

Match line

Sta. 10+56.75

Sta. 10+76.75

Match line

Sta. 11+16.75

Sta. 11+36.75

Match line

**NOTE**

For general notes, explanation,  
and reference drawings,  
see drawing 9689-62/1666  
sheet 20

**Reference Drawings**

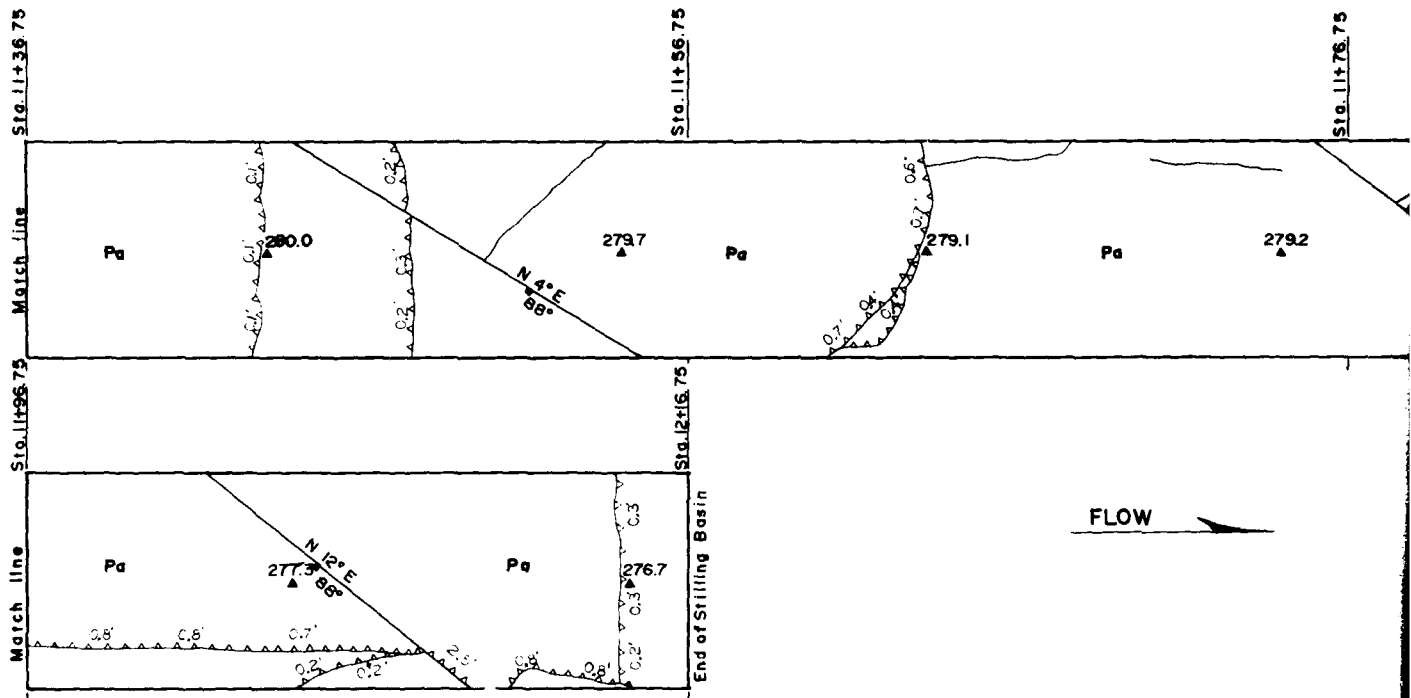
Concrete and Reinforcing..... 9570-62/1433  
Geologic Sections..... 9570-62/1481

**PLAN**

Scale 1" = 2'

2 1 0 1 2

DESIGNED BY RC	DATE	DESCRIPTION	BY
DRAWN BY CH		DEPARTMENT OF THE ARMY LITTLE ROCK DISTRICT CORPS OF ENGINEERS LITTLE ROCK, ARKANSAS	
CHECKED BY CD		ARKANSAS RIVER AND TRIBUTARIES	ARKANSAS RIVER, ARKANSAS
SUBMITTED BY		<b>TOAD SUCK FERRY LOCK AND DAM</b> <b>RELOCATIONS</b> <b>CONWAY WATER SUPPLY</b> <b>OUTLET WORKS-CONDUIT</b> <b>STA 9+56.75 TO STA 11+36.75</b>	
ENGINEER		APRIL 1983	REV. SERIAL NO. 00-00001
		DRAWING NUMBER <b>9689-62/1667</b> SHEET 21 OF 24	

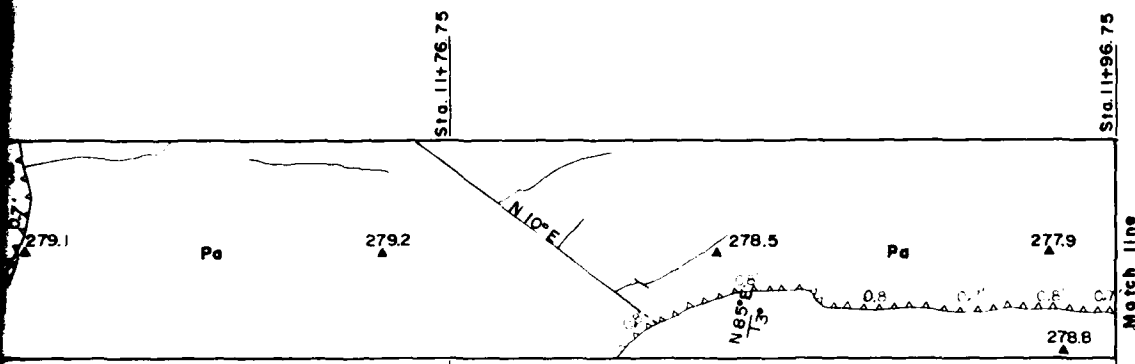


**PLAN**

Scale: 1" = 2'

2 1 0 1 2

**WORK SAFELY**



**NOTE**

For general notes, explanation, and reference drawings, see drawing 9689-62/666, sheet 20

FLOW

**PLAN**

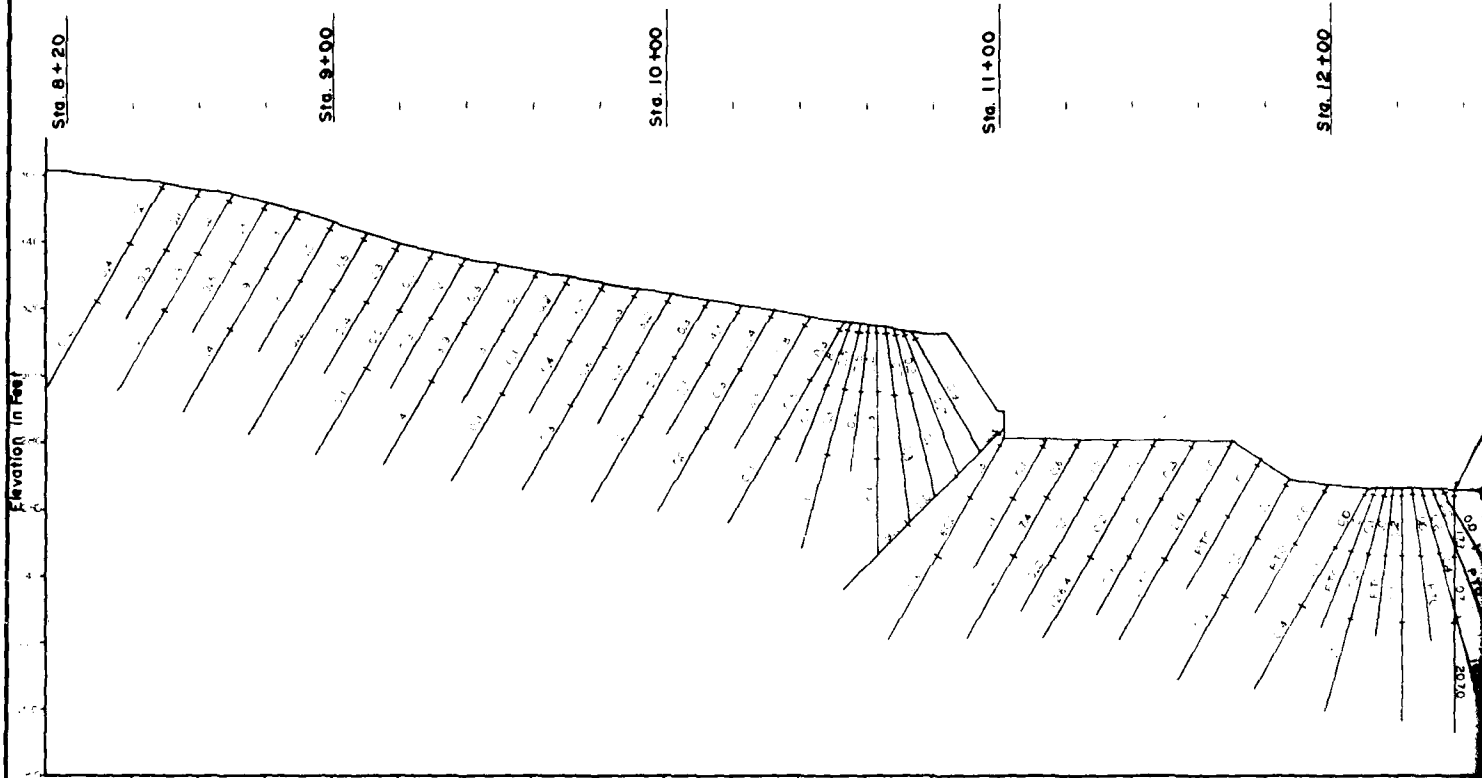
Scale: 1" = 2'

2 1 0 1 2

**REFERENCE DRAWINGS**

Concrete and Reinforcing ..... 9570-62/1433  
Geologic Sections ..... 9570-62/1481

REVISION	DATE	DESCRIPTION	BY
DEPARTMENT OF THE ARMY LITTLE ROCK DISTRICT, CORPS OF ENGINEERS LITTLE ROCK, ARKANSAS			
DESIGNED BY	ARKANSAS RIVER AND TRIBUTARIES ARKANSAS RIVER, ARKANSAS		
RC	TOAD SUCK FERRY LOCK AND DAM		
DRAWN BY	RELOCATIONS		
CH	CONWAY WATER SUPPLY		
CHECKED BY	OUTLET WORKS - CONDUIT		
CD	STA 11+3675 TO STA 12+1675		
SUBMITTED BY			APRIL 1983
ENGINEER	9689-62/1668		BY SERIAL NO. 8 0001



**SECTION ALONG GROUT CURTAIN ON DAM AX**

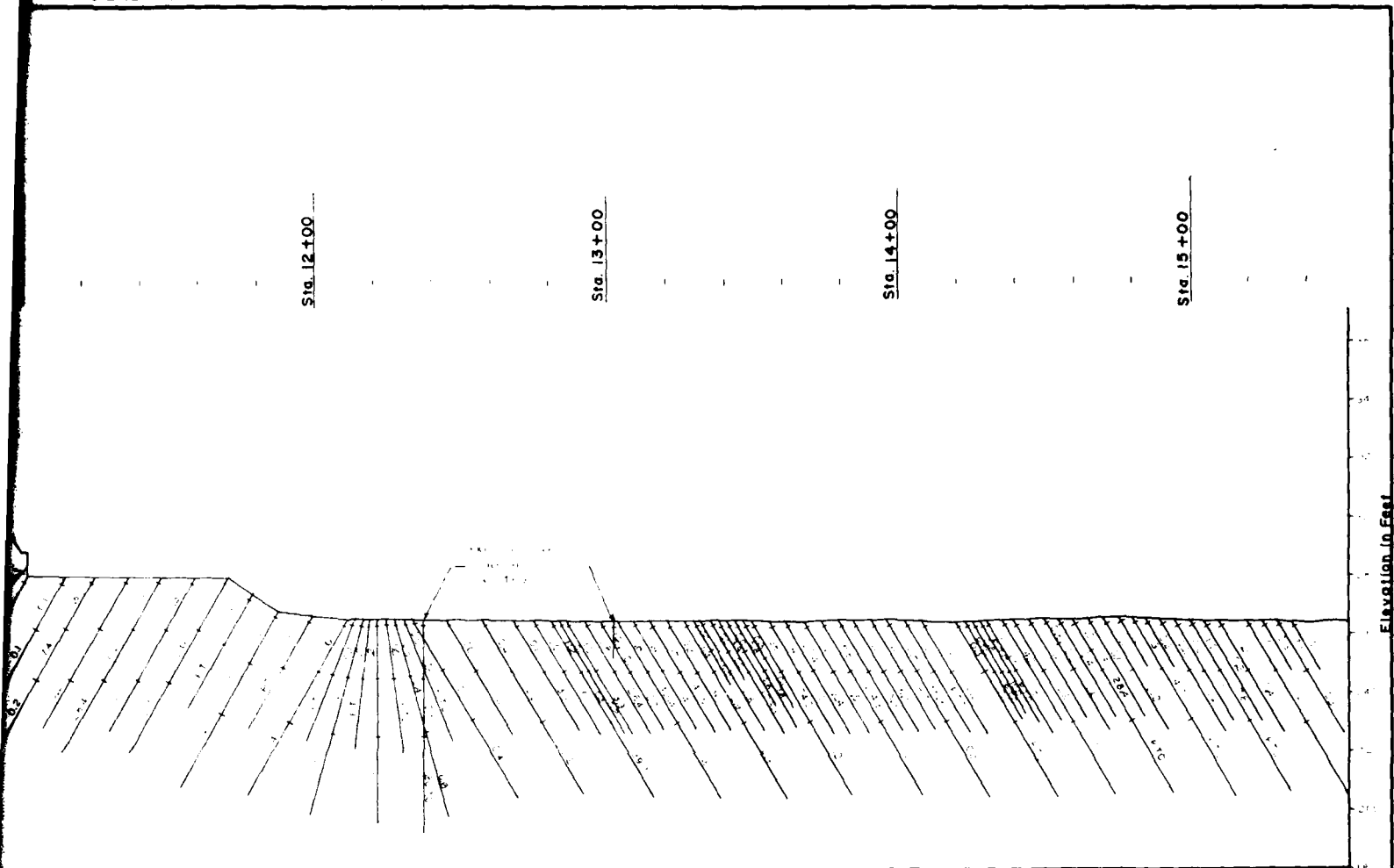
(LOOKING UPSTREAM)

Scale: 1" = 20'

20 10 0 10 20

**WORK SAFELY**

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**SECTION ALONG GROUT CURTAIN ON DAM AXIS**

(LOOKING UPSTREAM)

Scale: 1" = 20'

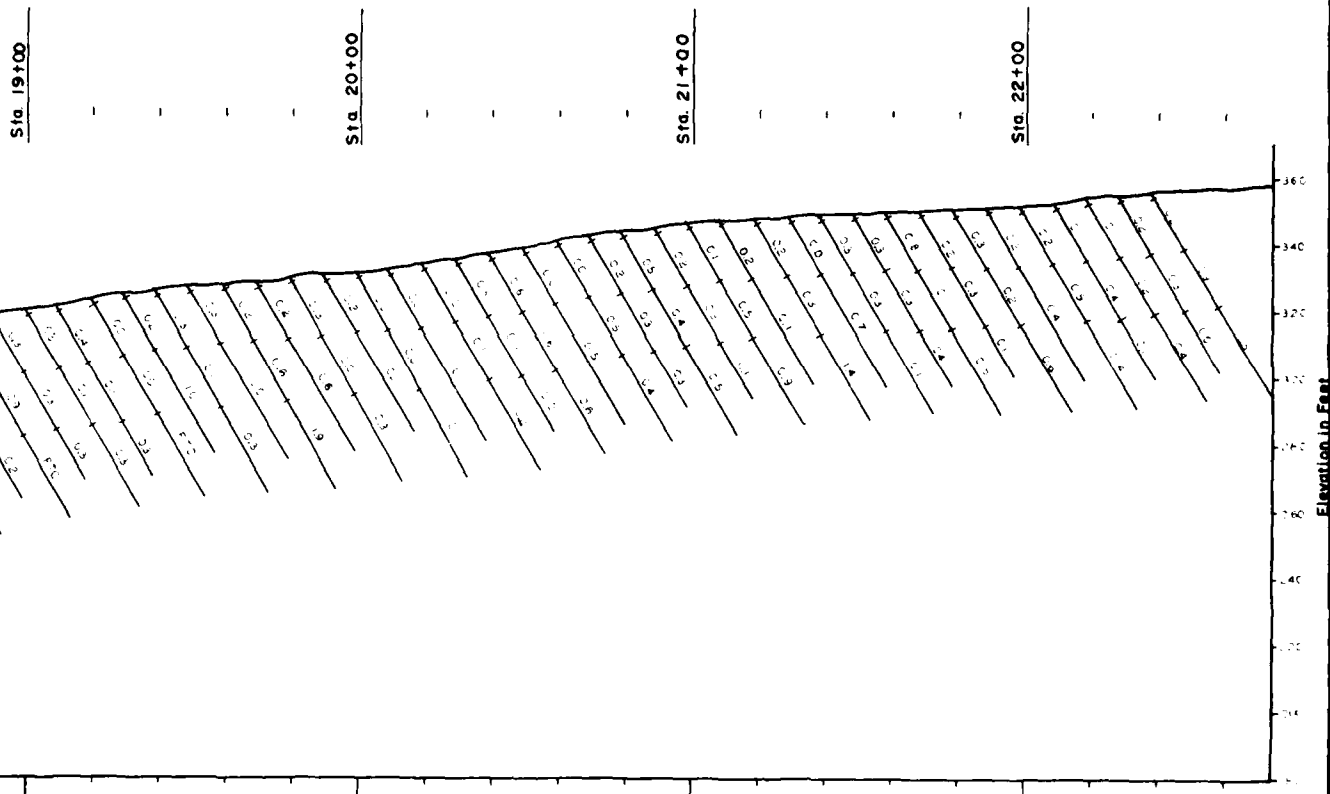
20 10 0 10 20

**NOTE**

Grout holes are shown with number of bags of cement used in each grout zone. Grout zones are between stops which are indicated by tick marks usually at depths of 2 ft., 20 ft., and 40 ft.

REVISION	DATE	DESCRIPTION	BY
DEPARTMENT OF THE ARMY LITTLE ROCK DISTRICT, CORPS OF ENGINEERS LITTLE ROCK, ARKANSAS			
DESIGNED BY	ARKANSAS RIVER AND TRIBUTARIES		ARKANSAS RIVER, ARKANSAS
RC	TOAD SUCK FERRY LOCK AND DAM		
DRAWN BY	RELOCATIONS		
CH	CONWAY WATER SUPPLY		
CHECKED BY	FOUNDATION TREATMENT		
CD	GROUTING		
SUBMITTED BY			APRIL 1983
ENGINEER	9687-621669		BY SERIAL NO. 80-8-0000
SHEET 23 OF 24			





**SECTION ALONG GROUT CURTAIN ON DAM AXIS**

(LOOKING UPSTREAM)

Scale: 1"=20'

20 10 0 10 20

**NOTE**

Grout holes are shown with number of bags of cement used in each grout zone. Grout zones are between stops which are indicated by tick marks, usually at depths of 2 ft, 20 ft, and 40 ft.

DESIGNED BY	RC	DEPARTMENT OF THE ARMY LITTLE ROCK DISTRICT CORPS OF ENGINEERS LITTLE ROCK, ARKANSAS
DRAWN BY	CH	ARKANSAS RIVER AND TRIBUTARIES
CHECKED BY	CD	TOAD SUCK FERRY LOCK AND DAM
SUBMITTED BY		RELOCATIONS CONWAY WATER SUPPLY FOUNDATION TREATMENT GROUTING
DATE		APRIL 1983
ENGINEER		9689-62/1670

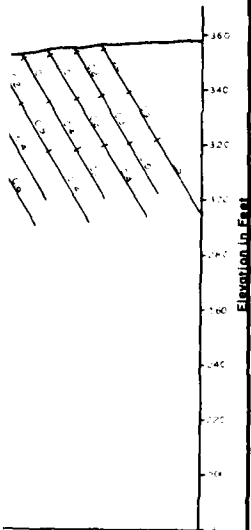
WORK SAFELY

END

DATE  
FILMED

8 - 83

DTIC



th number of bags  
grout zone. Grout  
ps which are indicated  
at depths of 2 ft, 20ft.

DESCRIPTION BY  
MENT OF THE ARMY  
TRICT, CORPS OF ENGINEERS  
E ROCK ARKANSAS  
RIBUTARIES ARKANSAS RIVER, ARKANSAS  
K FERRY LOCK AND DAM  
RELOCATIONS  
AY WATER SUPPLY  
DATION TREATMENT  
GROUTING  
APRIL 1983  
BY SERIAL NO. 80 9-000  
9689-627670  
24 24